

Assessment of the Potential Impact on Groundwater of the Proposed Expansion of the Hawaiian Memorial Park - April 2018

Prepared by: Tom Nance Water Resource Engineering



### Assessment of the Potential Impact on Groundwater of the Proposed Expansion of the Hawaiian Memorial Park

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#### Introduction

An expansion of the Hawaiian Memorial Park (HMP) Cemetery is proposed which will require a land use boundary amendment from Conservation to Urban for 53.45 acres of TMK 4-5-033:001. The Petition Area in question is shown on Figure 1. Of the 53.45-acre area, 28.2 acres would be for cemetery use. The remaining area would consist of internal roadways, open space, and a cultural reserve.

This report addresses the potential impact on groundwater resources should the land use boundary amendment be granted and the proposed project is implemented. The assessment addresses groundwater on a regional scale and also deals with a site specific issue regarding a dug well and perennial seep, the discharge from which has created a habitat for the damsel fly which must be preserved.

#### **Geologic Setting of the Petition Area**

All of HMP, including the Petition Area, is located within the caldera of the Koolau Mountain (labeled the Kailua Caldera on Figure 2). The caldera filling lavas which lie beneath HMP are a part of the Kailua Member of the Koolau volcanics. Its basalt flows are dense, massive, and relatively impermeable due to almost complete filling of interstices with secondary minerals resulting from hydrothermal alteration. Clinker beds, where they occur, have been cemented into hard and essentially impermeable breccia. Joints of intruded dikes are also filled with secondary minerals. In short, development of even a moderate capacity well anywhere in the Kailua volcanics beneath the HMP property would not be possible. This is in sharp contrast to the permeability most other basalts of the Koolau mountain.

Also of significance is the deep weathering of the Kailua volcanics across the HMP site. This has resulted in stiff silt and clay residual soils underlain by saprolite to depths exceeding 50 feet.

#### **Regional Groundwater Perspective**

The HMP site is at the south end of the area designated by the State Commission on Water Resource Management (CWRM) as the Koolaupoko Aquifer System. It is a 27-square mile area bounded by the Koolau Crest and the shoreline and extending from Oneawa Hills at the south end to the north ridge line of Waikane Valley. The CWRM has set the aquifer's sustainable yield at 30 million gallons per day (MGD) and has issued water use permits to 19 wells with a total permitted use of 10.312 MGD. As shown on Figure 3, total use by these wells has closely matched the combined permitted use amount.

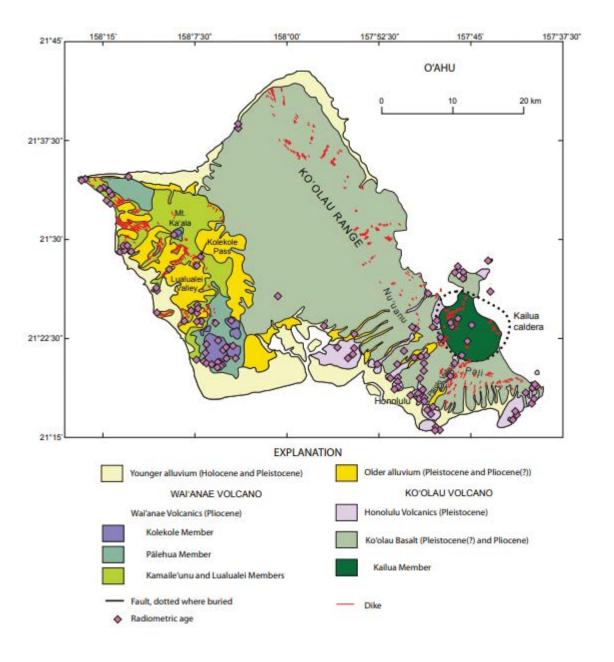
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**Project Vicinity Map (by HHF Planners)** 

Figure 1

Hawaiian Memorial Park Cemetery Expansion Project Kāne'ohe, O'ahu, Hawai'i



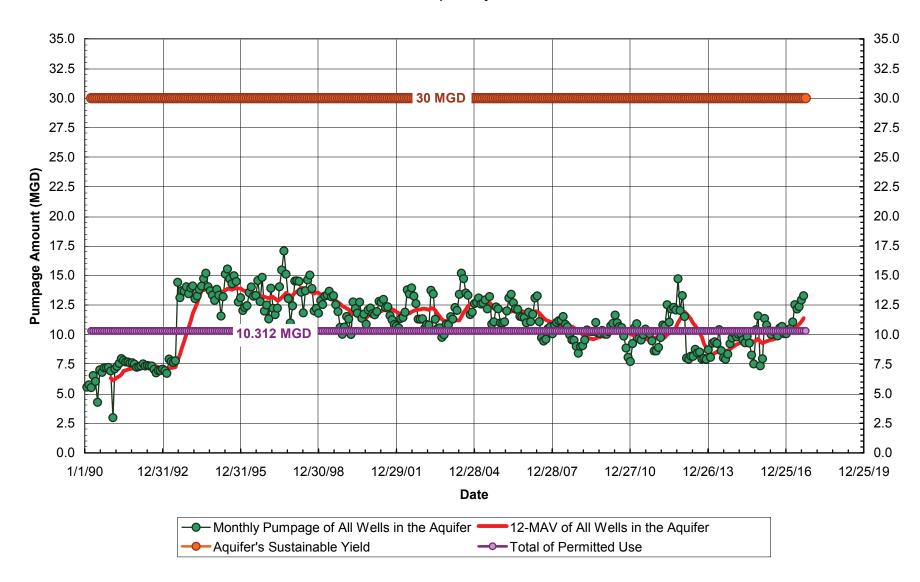
Source: Sherrod et al (2007 : p. 19)

Figure 2

Location of the Koolau Caldera

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Figure 3. Pumpage of Wells in the Koolaupoko Aquifer System in Comparison to the CWRM's Sustainable Yield of the Aquifer System and the Total of Permitted Use



Of the 19 wells in the aquifer with permitted use permits, nine are nominally upgradient of the HMP site. Their locations are shown on Figure 4 and information on them is presented in Table 1. Most notable is that all of these wells tap into high level groundwater standing between 200 and 570 feet above sea level, apparently all drawing from dike confined compartments in the Koolau's dike complex. Since the mid-1990s, total pumpage of all nine wells has been less than their combined permitted use (Figure 5). Based on the locations of these wells and the groundwater occurrence they draw from, nothing at the existing HMP or what is planned for its expansion in the Petition Area has or will have an impact on their ongoing uses.

There are also five wells which are nominally downgradient from HMP. Their locations are also shown on Figure 4 and information on their construction and hydraulic performance are presented in Table 2. All five are shallow irrigation wells of modest capacity within the Bay View Golf Course. They draw water exclusively from the overlying alluvium of clayey silt and gravel rather than from the volcanics at depth. Use of the wells does require a Water Use Permit from the CWRM, but apparently such a permit was never obtained. Their modest use was reported to the CWRM for the 29-month period from the July 1997 to November 1999 (Figure 6), but not since then. It is not known if these wells are still in use. However, the planned expansion of HMP in the Petition Area would have no impact on their viability if they are still in use.

#### Information and Analysis of the Dug Well and Seep in the Petition Area

There is a dug well and perennial seep in the Petition Area that is of concern. Figure 7 shows their locations about 300 feet northwest of the loop road in the Ocean View Garden. The well is 11.5 feet deep below the top of its square-shaped concrete rim. The opening of the concrete is 2.65 by 2.9 feet. The dug borehole below the concrete is substantially larger than this opening. Figure 8 is a schematic cross section of the well and Appendix A contains photos of it. As measured a number of times during the field investigation, the water level in the well was consistently above the ground level on the downstream side of the well. The well is not registered with the CWRM and no information about its installation or past use could be found. Based on old pipe laying nearby, it may at one time have been a modest source of supply.

A small but perennial seep emerges about four feet downslope from the well. Further down the waterway, the flowrate in the waterway continuously increases enroute to its ultimate discharge into the drain inlet at the upper end of Ohaha Place. Given the additions to the flowrate enroute downslope, it is more accurate to describe the seep as an area of discharge rather than a discharge from a single point.

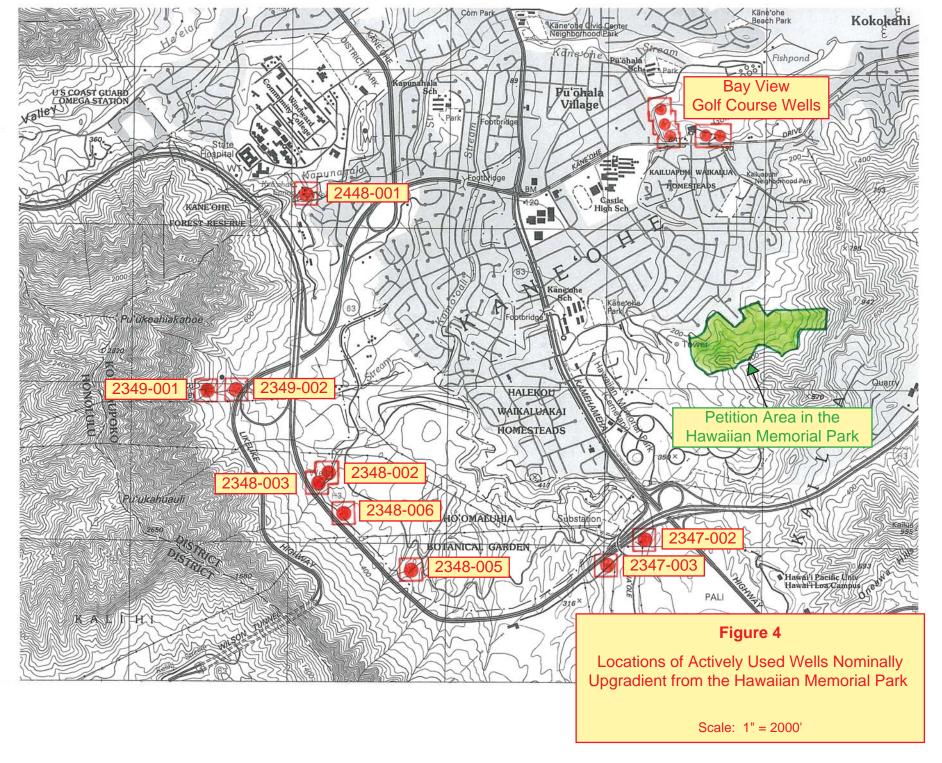


Table 1. Summary Information of Active Wells Nominally Upgradient of the Hawaiian Memorial Park

Well No.	Well Name	WUP (MGD)	Year Drilled	Ground Elevation (Ft. MSL)	Well Depth (Feet)	Elevation at Bottom (Ft. MSL)	SWL (Ft. MSL)	Hydraulic Performance (Feet @ GPM)	Installed Pump (GPM)
Wells of the Ho	nolulu Board of Water Su	oply							
2348-002	Kuou I-1	2.375	1955	274	418	-144	310	262 @ 820	
2348-003	Kuou I-2		1955	293	280	13	290	5.2 @ 1500	2100
2348-005	Kuou II	0.100	1986	342	550	-208	258	126 @ 994	700
2348-006	Kuou III	0.700	1984	324	566	-242	255	135 @ 609	500
2349-001	Luluku Tunnel	0.713	1948	570			570		
2349-002	Luluku	1.050	1984	412	460	-48	362	120 @ 739	700
Other Nominall	y Upgradient Wells								
2347-002	Koolau GC-1	0.150	1988	234	130	104	201	4.4 @ 300	350
2347-003	Koolau GC-2		1988	246	130	116	219	6 @ 400	350
2448-001	Hawaii State Hospital	0.088	1946	252	249	3	249		450

Figure 5. Pumpage of the Nine Wells Nominally Upgradient of the Hawaiian Memorial Park

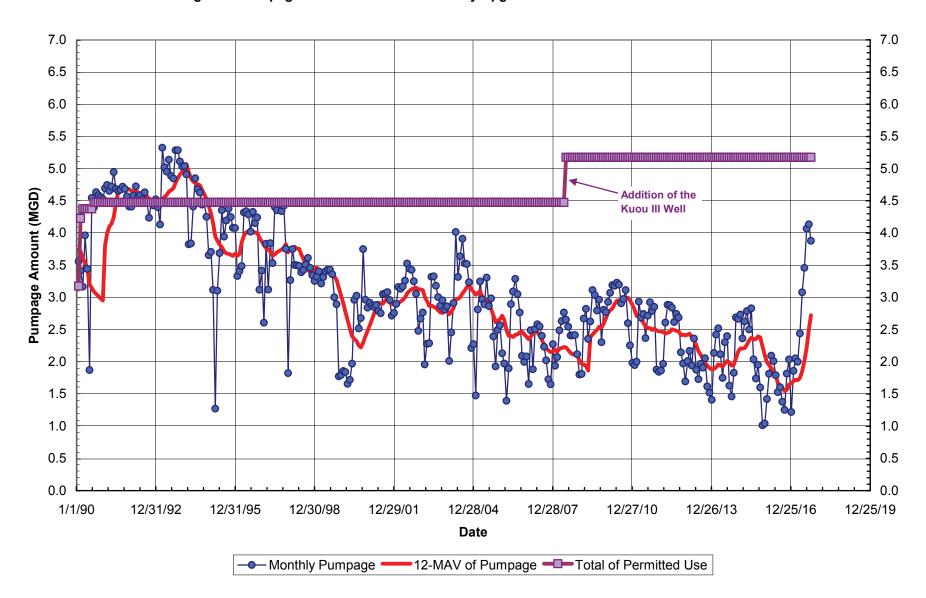
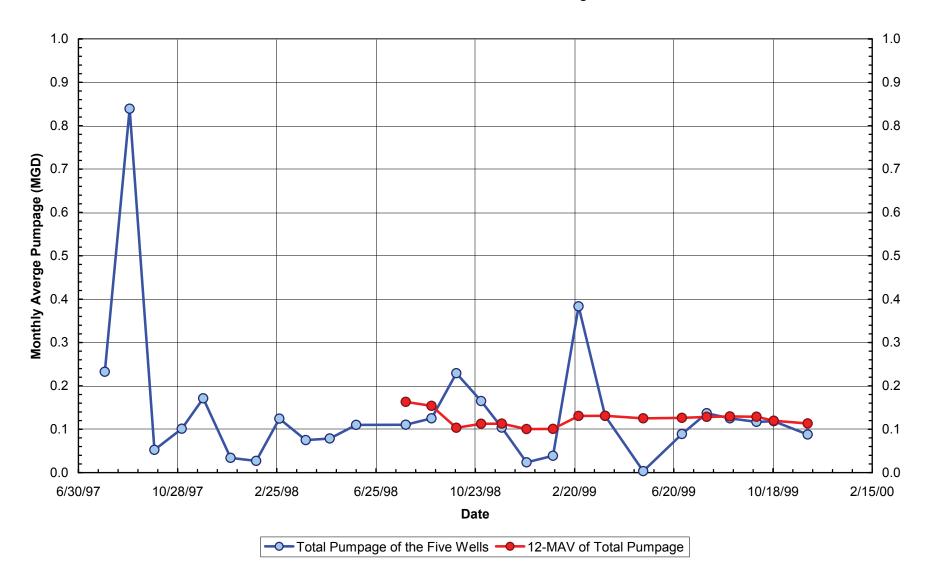
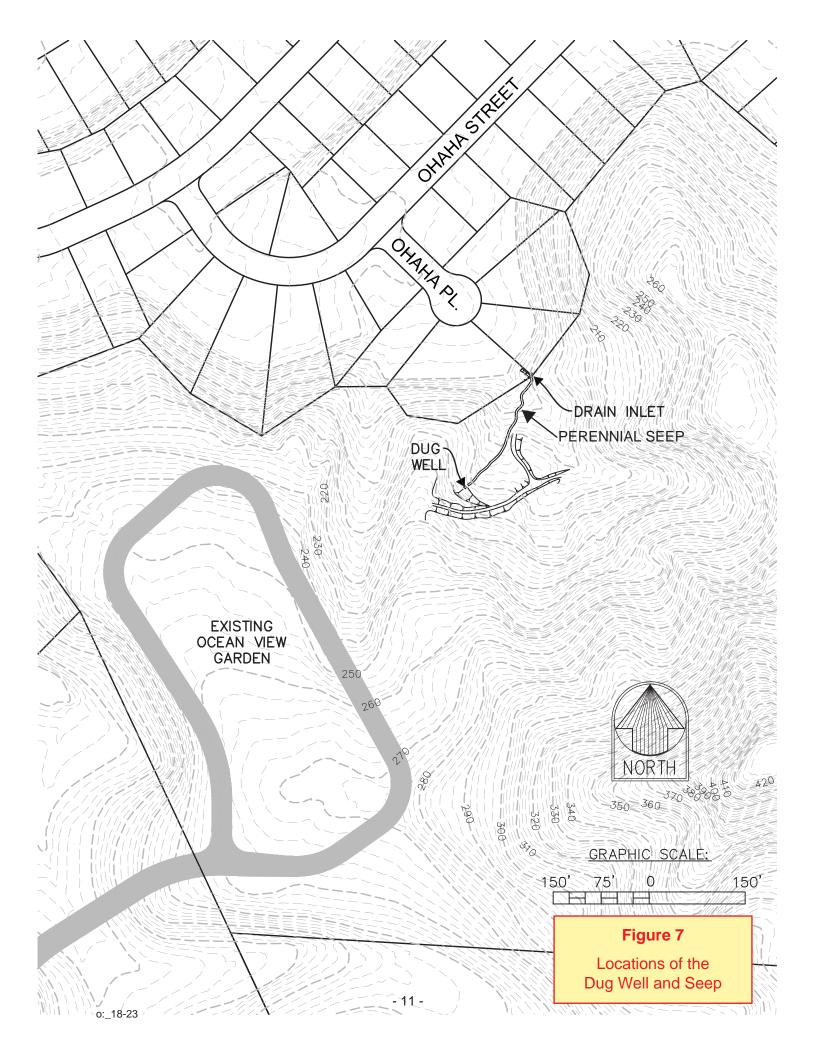


Table 2. Summary Information on the Five Bay View Golf Course Irrigation Wells

Well No.	Well Name	Year Drilled	Ground Elevation (Ft. MSL)	Well Depth (Feet)	Elevation at Bottom (Ft. MSL)	SWL (Ft. MSL)	Hydraulic Performance (Feet @ GPM)	Current Use
2447-002	Bay View 1	1995	13	50	-37	4.4	7.5 @ 50	Irrigation
2447-003	Bay View 2	1995	14	50	-36	5.1	5.8 @ 100	Irrigation
2447-004	Bay View 3	1995	15	50	-35	8.5	12 @ 60	Irrigation
2447-005	Bay View 4	1996	11	50	-39	8.4	7.4 @ 100	Irrigation
2447-006	Bay View 5	1996	22	60	-38	5.3	8.6 @ 100	Irrigation

Figure 6. Pumpage of the Bay View Golf Course Wells as Reported to the State Commission on Water Resource Management





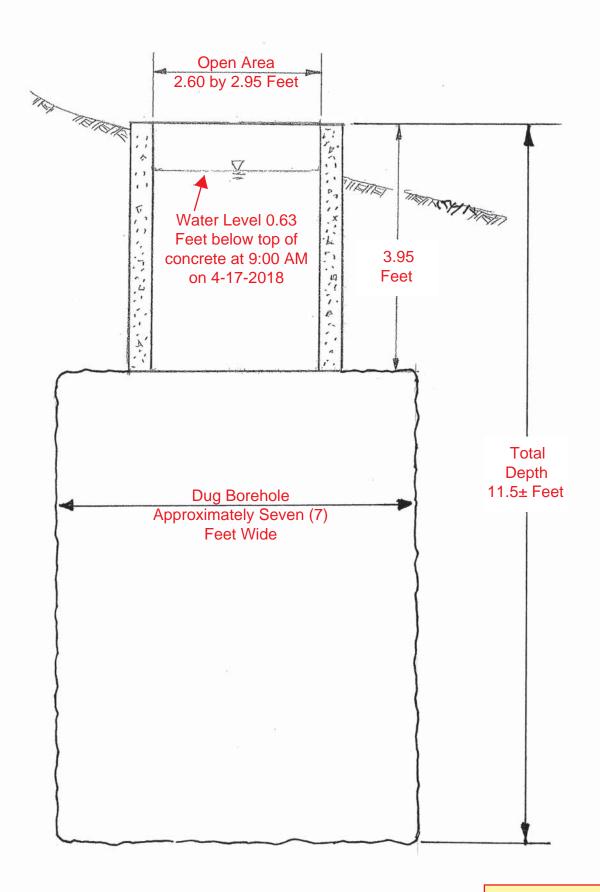


Figure 8
Schematic Cross Section of Dug Well

Implementation of the HMP expansion into the Petition Area would involve installation of retaining walls and fill of tens of feet in depth in the area upslope from the well and seep. Figures 9 and 10 illustrate these possibilities. On the assumption that supply to the dug well and seep is from a shallow perched water source that might be adversely impacted by footings for the retaining walls and/or compression by the weight of tens of feet of fill, two types of field investigation were undertaken: (1) drilling of four boreholes directly upslope of the well and seep; and (2) a siphon and pump test of the well to determine if subsurface leakage from the well is creating the seep that emerges just four feet downslope. Results of each of these investigations are described in the paragraphs following.

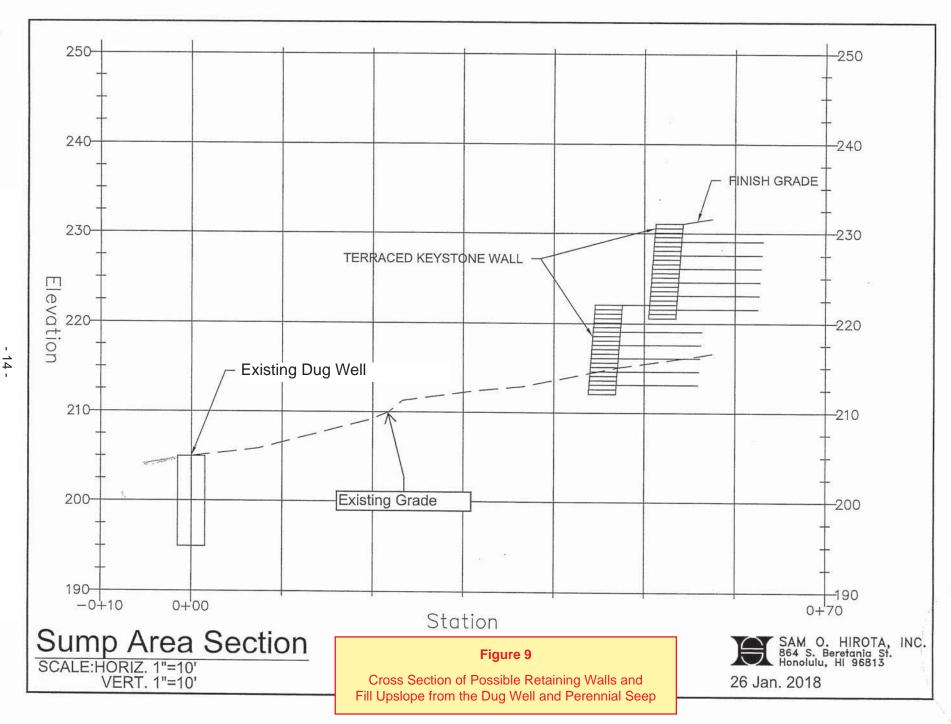
#### Results of the Four Boreholes Drilled Above the Well and Seep

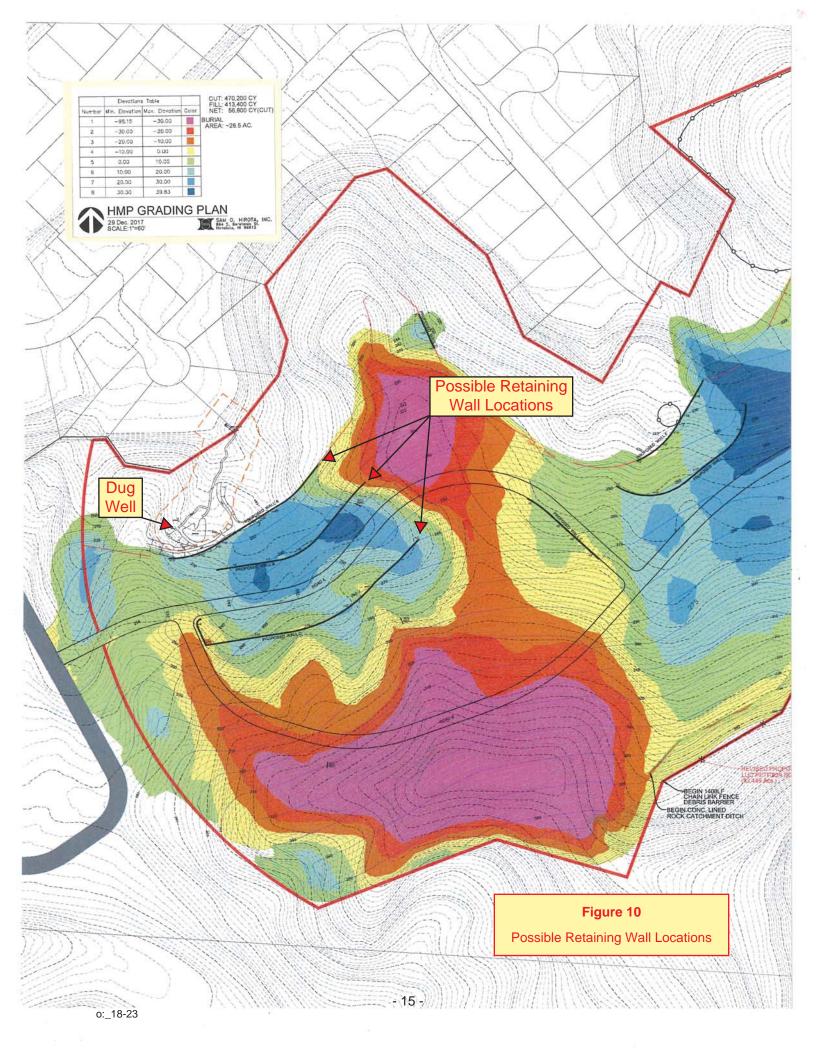
Figure 11 shows the approximate locations of the four boreholes drilled above the well and seep and Appendix B contains the logs of these boreholes prepared by Geolabs, Inc. Although an obvious perching member was not encountered in the borings, the water level response in all four boreholes was instructive. Water was not encountered in each borehole until each borehole had been drilled down to between 15 to 20 feet below ground. After reaching that depth, the water level in each borehole very slowly rose up (Steven Carr of Geolabs, personal communication). Table 3 prepared by Geolabs documents this slow filing in each of the boreholes. As the tabulation of approximate water levels in the boreholes and the well in Table 4 shows, the semi-confined groundwater residing in the poorly permeable residual soil has a relatively steep downslope gradient

#### Results of Siphon and Pump Testing the Dug Well

On April 17, 2018, testing of the dug well was undertaken with two basic objectives: (1) to confirm that the semi-confined groundwater occurrence found at the four Geolabs boreholes directly upslope also exists at the dug well; and (2) to confirm that the seep that emerges four feet downslope of the well is a result of subsurface leakage from the well. Both aspects of the groundwater occurrence were confirmed by the test.

The intention was to run the test by siphoning from the well (and discharging downslope to maintain the siphon) rather than by pumping. Siphoning was begun at about 9:30AM at about 30 GPM, but the siphon was lost in less than 10 minutes. An attempt to restart the siphon also failed, this time in less than five (5) minutes. Thereafter, the well was pumped with a small, 1/4 horsepower sump pump, first at 17 GPM and then at about 15 GPM. The several aspects to note from the test data depicted on Figures 12 and 13 are as follows:





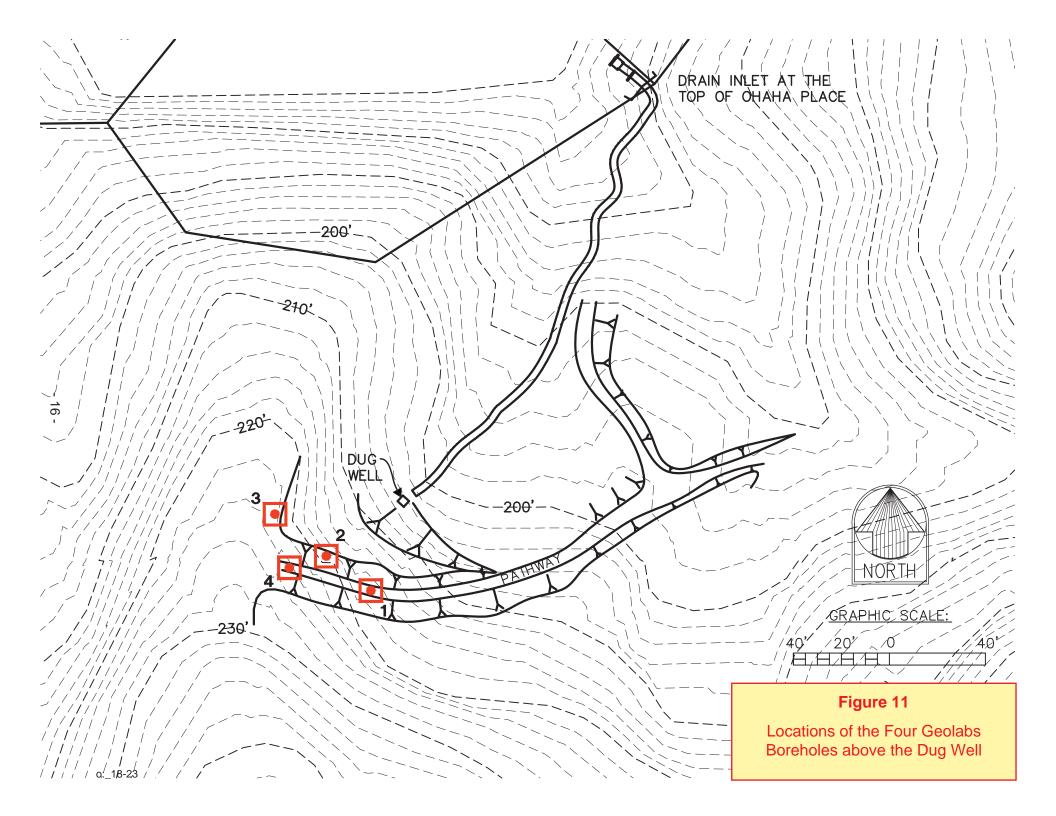


Table 3. Water Level Measurements in the Four Boreholes by Geolabs, Inc.

BORING	NO. 1 WATER LEVEL MEASUR	REMENTS
DATE/TIME	DEPTH TO WATER (FT.)	BOREHOLE DEPTH (FT.)
3/20/18 0945 hrs.	11.2	22
3/20/18 1030 hrs.	10.5	22
3/20/18 1120 hrs.	9.9	22
3/21/18 0800 hrs.	9.8	19
3/21/18 1130 hrs.	9.9	19
3/21/18 1435 hrs.	9.8	19
3/22/18 0755 hrs.	9.8	19
3/22/18 1330 hrs.	9.7	19
3/23/18 0745 hrs.	9.7	19

BORING	NO. 2 WATER LEVEL MEASUR	REMENTS
DATE/TIME	DEPTH TO WATER (FT.)	BOREHOLE DEPTH (FT.)
3/20/18 1450 hrs.	11.8	23
3/21/18 0805 hrs.	10.5	18.5
3/21/18 1135 hrs.	10.3	18.5
3/21/18 1440 hrs.	10.4	18.5
3/22/18 0750 hrs.	10.5	18.5
3/22/18 1115 hrs.	10.3	18.5
3/22/18 1325 hrs.	9.5	18.5
3/23/18 0750 hrs.	10.3	18.5

BORING	BORING NO. 3 WATER LEVEL MEASUREMENTS											
DATE/TIME	DEPTH TO WATER (FT.)	BOREHOLE DEPTH (FT.)										
3/21/18 1245 hrs.	Not Encountered	18.5										
3/21/18 1430 hrs.	Not Encountered	18.5										
3/22/18 0745 hrs.	15.2	18.5										
3/22/18 1110 hrs.	15.3	18.5										
3/22/18 1320 hrs.	14.6	18.5										
3/23/18 0755 hrs.	15.5	18.5										

BORING	NO. 4 WATER LEVEL MEASUR	REMENTS
DATE/TIME	DEPTH TO WATER (FT.)	BOREHOLE DEPTH (FT.)
3/22/18 1201 hrs.	15.1	22
3/22/18 1315 hrs.	13.3	22
3/23/18 0800 hrs.	13.5	20

Table 4. Elevations, Depths, and Water Levels in the Four Boreholes in Comparison to the Dug Well

Borehole Number	Approximate Ground Elevation (Ft. MSL)	Borehole Depth (Feet)	Approximate Elevation at Bottom (Ft. MSL)	Depth to Water (Feet)	Approximate Water Level (Ft. MSL)
1	217	22	195	10	207
2	218	23	195	10	208
3	222	19	203	15	207
4	224	19	205	13	211
Well	205	12	193	2	203

Figure 12. Water Level Response to the Siphon and Pump Test of the HMP Dug Well

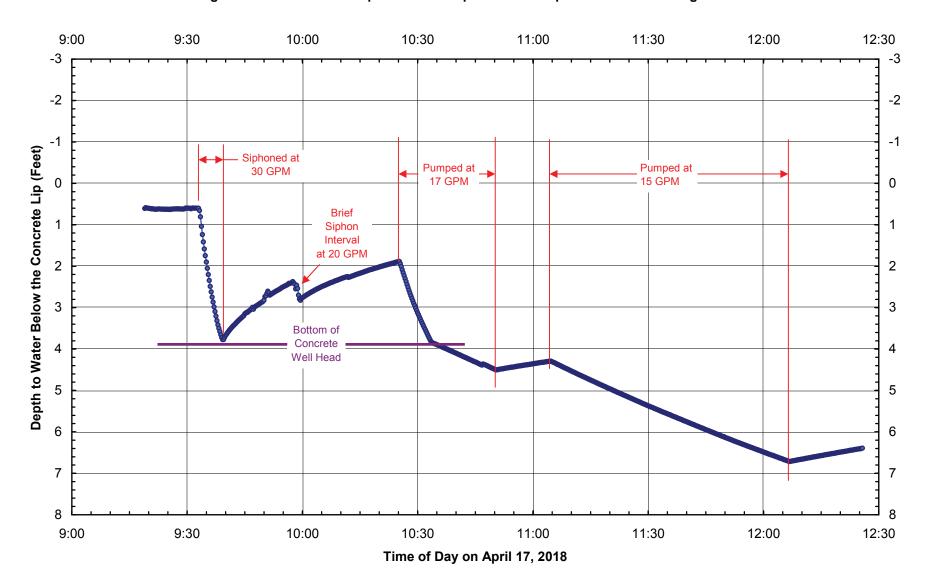
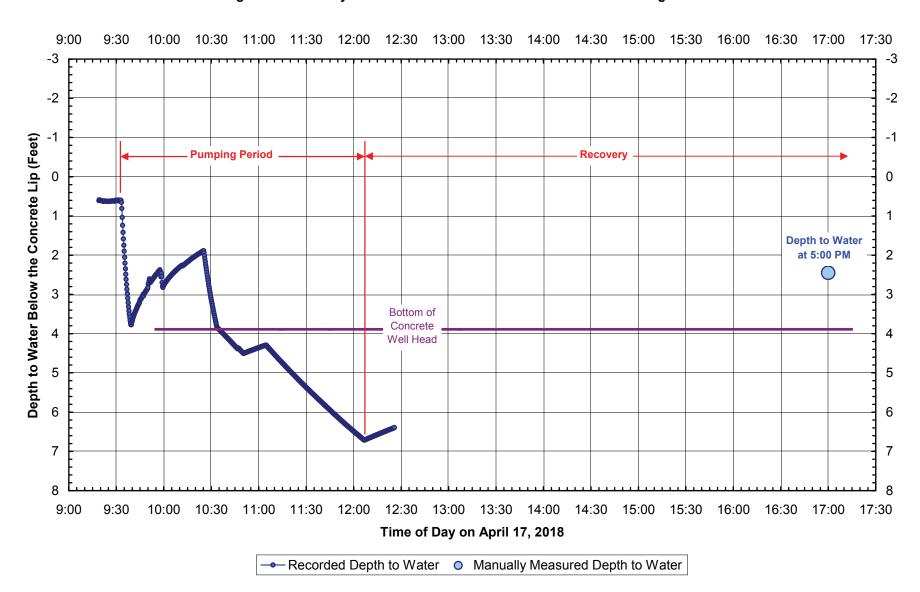


Figure 13. Manually Measured Recovered Water Level in the HMP Dug Well

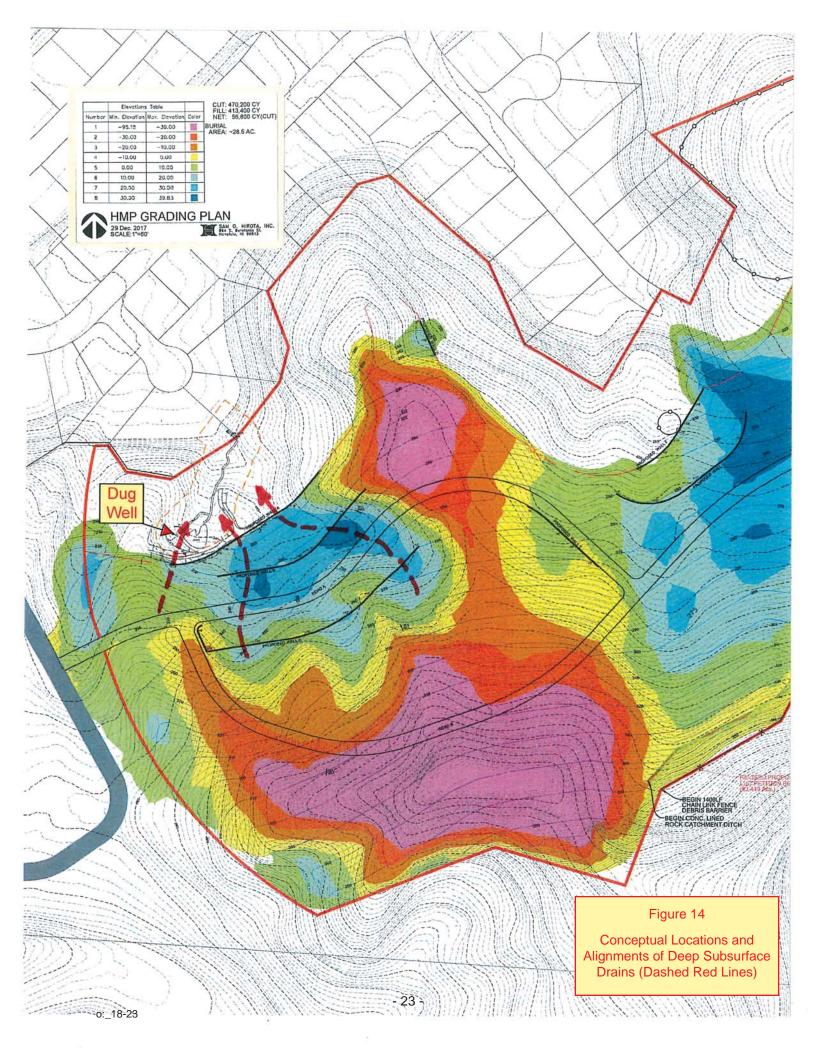


- When the water level in the well was drawn down about halfway down the concrete well
  head, the seep that emerges about four feet downslope had stopped flowing. Clearly, the
  seep is maintained by subsurface leakage from the well.
- Over the period of intermittent siphoning and then pumping, a total of 1615 gallons was removed from the well. Assuming the 7-foot wide borehole below the concrete is approximately round, 950 gallons was removed from storage in the well itself and the remaining 665 gallons flowed from the formation into the well. That inflow was at an average of about 4.3 GPM.
- The recovered water level was manually measured at 5:00PM (Figure 13). The water level had risen up inside the concrete well head, but not high enough to have started flow in the downstream seep. Average inflow to the well from the time pumping was stopped at 12:07PM until the 5:00PM measurement was approximately 3.1 GPM.
- The well's water level was checked at 9:30AM on the day following (April 18th). The water level had fully recovered (actually to a level 0.1-foot higher than at the start of the test the day before). The seep below the well was fully restored at that time.

#### **Summary of Findings, Conclusions, and Recommendations**

- 1. The entire Petition Area overlies on a geologic formation known as the Kailua series volcanics. These caldera-filling volcanics are virtually impermeable. As such, none of the proposed actions within the Petition Area have the potential to impact ongoing or possible future uses of groundwater drawn from the permeable Koolau volcanics of the Koolaupoko Aquifer System.
- With regard to the perennial groundwater seep which has created the habitat for the damsel fly, field observations, the four boreholes drilled by Geolabs, Inc., and the test of the dug well have established the following regarding this groundwater occurrence:
  - (a) The groundwater seep is maintained by the natural discharge of groundwater moving downslope through the poorly permeable residual soils overlying the unweathered Kailua volcanics at depth.
  - (b) In the vicinity of the dug well and the four Geolabs boreholes upslope from the wells, the groundwater is actually semi-confined. The groundwater movement is through soils at depths of 10 feet or more rather than through the surface soils.
  - (c) The upper end of the seep begins about four (4) feet downslope of the dug well. Based on results of the well test, flow in the upper one third to one half of the linear seep is maintained by subsurface leakage from the well.

- (d) Further downslope, flow in the seep increases continuously to its ultimate discharge into the Ohaha Place drainage system.
- 3. The proposed expansion into the Petition Area would include construction of a sequence of three (essentially parallel) retaining walls upslope of the dug well and perennial seep (Walls A, B, and C on Figure 10) and fill heights of 10 to 30 feet behind these walls (depths of fill are color coded on Figure 10). The concern is that the retaining walls and/or the fill behind them may intercept, impede, or reroute the groundwater flow that maintains the perennial seep and thereby diminish or destroy the damsel fly habitat. This potential impact is addressed in the following:
  - (a) Based on the groundwater occurrence established by the four Geolabs borings and the dug well, the footings of the proposed retaining walls would be too shallow to intercept the groundwater moving downslope. The walls and the fill behind them will have subsurface drains (Geolabs Inc., 2018: page 30 and Plate 6), but these will be too shallow to intercept the groundwater which maintains the downslope seep.
  - (b) Loading by the fill behind the retaining walls does have the potential to compress the soils below through which the groundwater is moving downslope. As such, this loading could reduce the permeability of these already poorly permeable soils, impeding or rerouting the downslope direction of the groundwater flow.
  - (c) To ensure that the quantity and direction of groundwater flow is maintained, at least two and possibly three deeper subsurface drains should be constructed. These would be aligned approximately perpendicular to the retaining walls and installed at depths to intercept and convey the flow of groundwater to the dug well seep. Their possible alignments are shown conceptually on Figure 14. Their exact locations, alignments, and depths would be determined with the drilling of additional boreholes in the project's design phase.



#### References

- Geolabs, Inc. 2018. Phase 1 Potential Rockfall and Slope Hazard Assessment, Hawaiian Memorial Park Cemetery Expansion. Consultant Report prepared for HHF Planners.
- Sherrod, D. R., J. M. Sinton, S. E. Watkins, and K. M. Brunt. 2007. Geologic Map of the State of Hawaii. U.S. Geological Survey Open-File Report 2007-1089, U.S. Department of the Interior, U.S. Geological Survey.
- Stearns, H. T. and K. N. Vaksvik. 1935. Geology and Ground-Water Resources of the Island of Oahu, Hawaii. Bulletin 1, Division of Hydrography, Territory of Hawaii.
- Sterns, H. T. 1939. Geologic Map and Guide of the Island of Oahu, Hawaii. Bulletin 2, Division of Hydrography, Territory of Hawaii.
- Stearns, H. T. 1940. Supplement to the Geology and Ground-Water Resources of the Island of Oahu, Hawaii. Bulletin 5, Division of Hydrography, Territory of Hawaii.

### Appendix

- A. Photos of the Dug Well and Seep Taken on March 30, 2018
- B. Logs of the Boreholes Drilled Above the Dug Well and Seep by Geolabs, Inc.
- C. Logs of the B-1 and B-2 Boreholes Drilled in Ocean View Garden by Geolabs, Inc.

### Appendix A

Photos of the Dug Well and Seep Taken on March 30, 2018

### View of the Concrete Top of the Well Note the Water Level in Relation to the Adjacent Ground Level



### View of the Top of the Well from the Other Side Note Tree Growth into the Well



## Relationship of the Well to the Emergent Seep Four Feet Downslope



## Flow from the Seep to the Adjacent Subdivision's Drain Inlet



### Appendix B

Logs of the Boreholes Drilled Above the Dug Well and Seep by Geolabs, Inc.

Geotechnical Engineering

# GROUNDWATER SPRING DISCHARGE Hawaiian Memorial Park

Log of Boring

		Field								Approximate Ground Surface	_
Drilling Notes	Φ _	Rec. Length/ Sample Length (inches)	RQD Length/ Sample Length (inches)		Pocket Pen. (tsf)	(feet)	Ф	Ö		Elevation (feet ): 218 * Latitude:21.39464 Longitude: -157.7887	
Drilling	Sample Quality	Rec. L Sampli (inche	RQD L Sampl (inche	Blows/ 6"	Pockel (tsf)	Depth (feet)	Sample	Graphic	nscs	Description	
	Good	10/18"		3/8/11		-	V	W	МН	Orangish brown <b>CLAYEY SILT</b> , stiff to very stiff, moist (residual soil)	
	Fair	23/24"		5/7/10/13	3	-					
	0	40/40"		0/40/40		5-			СН	Mottled orangish brown and gray SILT CLAY, very stiff, moist (residual soil)	
	Good Fair	16/18"		6/10/13 3/5/6/9		-	X		MH	Mottled orangish brown with some grace CLAYEY SILT, stiff to very stiff, moist (residual soil)	
	Good	15/18"		8/10/12	1	10-	X		SM	grades with gray silty clay seams loca grades with decomposed gravel Brown with trace gray SILTY SAND	lly
	Fair	22/24"		1/2/1/2	· ·	15-			>	(BASALTIC), loose to medium dense very moist to wet (saprolite)  grades with sandy silt	,
	Fair	23/24"		2/5/6/4		20 -	I		ML	Gray with some brown <b>CLAYEY SILT</b> with some fine sand, stiff, moist (residual soil)	
						25 - - - -	-			Boring terminated at 22 feet	
						30	-				_
Date/Time Sta			, 2018 10		Water L	evel:	Ţ	9.	1 ft.	03/22/2018 1330 HRS	
Date/Time Cor			-								
Logged By:		S. Latroni			Driller N		:			ngamath Plate	
Project Engine		Steven Ca	arr		Drill Rig: MINUTEMAN						
Total Depth:		22 feet			Drilling I					id Stem Auger	
Work Order:	7	7604-10			Driving	Ener	gy:	14	40 lb	. wt., 30 in. drop	

Geotechnical Engineering

### GROUNDWATER SPRING DISCHARGE Hawaiian Memorial Park

Log of Boring

ļ	#b. >											
			Field								Approximate Groun	
	Drilling Notes	ole ity	Rec. Length/ Sample Length (inches)	RQD Length/ Sample Length (inches)	/s	Pocket Pen. (tsf)	Depth (feet)	ole	hic	S	Elevation (feet ): Latitude:21.39 Longitude: -157.	451
	Orilli	Sample Quality	Rec. Sam (inch	RQD Sam (inch	Blows/ 6"	Pock (tsf)	Dept	Sample	Graphic	nscs	Description	on
		Good	10/18"		5/9/15		-	X		МН	Orangish brown with trace SILT, stiff to very stiff, mo soil)	gray <b>CLAYEY</b> bist (residual
		Fair	16/24"		5/6/5/7	7	-	1	$\mathcal{U}$		,	-
		Good	10/18"		5/8/13	3	5	X			grades with gray silty clay	seams locally
		Fair	24/24"		2/4/4/3	3	10 -			́СН ,	Gray with trace brown <b>FAT</b> moist (residual soil)  Brown with some gray <b>CLA</b>	-
		Good	16/18"		4/8/11		15-	X		CH	stiff, moist to very moist ( grades with gravel (basalt Mottled brown and gray SII stiff to very stiff, moist (re	residual soil) - ic) LTY CLAY, _
		Fair	24/24"		3/5/6/	6	20 -			SM	Prove CII TV CAND (PAC	- - - 
							25 -	-	-1 1:	SIVI	Brown SILTY SAND (BASA some decomposed grave dense, very moist to wet Boring terminated at 23 fe	el, medium (saprolite)
OT 3/23/18							30 -	-				- - - -
BORING LOG DRAFT 7604-10.GPJ GEOLABS.GDT 3/23/18							35-					- - -
-10.G	Date/Time Sta	rted: N	March 20	2018 11	:30	Water L		<b>y</b>	9	5 ft.	03/22/2018 1325 HRS	I
7604		ate/Time Started: March 20, 2018 11:30 ate/Time Completed:March 20, 2018 15:30						0.	J 11.	00,11,101010101010		
3AFT	Logged By:		S. Latroni			Driller N	lame	:	K	. Von	ngamath	- Plate
G DR	Project Engine	arr		Drill Rig		-			ГЕМАН	15		
G LO	Total Depth:		23 feet			Drilling		od:			d Stem Auger	1
MORIN	Work Order:				Driving					. wt., 30 in. drop	$\dashv$	
u (								~ .			· I	

Geotechnical Engineering

### GROUNDWATER SPRING DISCHARGE Hawaiian Memorial Park

Log of Boring

Pield   September   Septemb	ŀ	war ✓											
Belling of the property of the													
Good 10/18" 9/17/29 Fair 15/24" 6/6/6/9  Good 9/18" 5/10/10  Fair 14/24" 4/6/8/7  Good 16/18" 5/11/12		S		ogth	ر ngth								
Good 10/18" 9/17/29 Fair 15/24" 6/6/6/9  Good 9/18" 5/10/10  Fair 14/24" 4/6/8/7  Good 16/18" 5/11/12		Sot		Ler	ngtł Ler		Jen	eet)					
Good 10/18" 9/17/29 Fair 15/24" 6/6/6/9  Good 9/18" 5/10/10  Fair 14/24" 4/6/8/7  Good 16/18" 5/11/12		ng ľ	iple lity	Lei iple	Le iple	/S/	(et F	th (f	ple	ohic	တ္လ		
Good 10/18" 9/17/29 Fair 15/24" 6/6/6/9  Good 9/18" 5/10/10  Fair 14/24" 4/6/8/7  Good 16/18" 5/11/12		Drilli	Sarr Qua	Rec Sarr (incl	RQE Sam (inct	Blow 6"	Pocl (tsf)	Dep	San	Grap	OSC	Description	on
Fair 15/24" 6/6/6/9  Fair 14/24" 4/6/8/7  Good 16/18" 5/11/12  Good 16/18" 5/11/12  Good 16/18" 5/11/12  Grades with decomposed gravel gravel gravel gravel gray FAT CLAY, stiff, very moist (residual soil)  Boring terminated at 22 feet	ľ	<del>-</del>								$\overline{M}$	MH	Orangish brown CLAYEY S	SILT, stiff to
Good 9/18" 5/10/10  Fair 14/24" 4/6/8/7  Good 16/18" 5/11/12  Good 16/18" 5/11/12  Grades with decomposed gravel gravel are more moist (residual soil)  CH Brownish gray to gray FAT CLAY, stiff, very moist (residual soil)  Boring terminated at 22 feet			Good	10/18"		9/17/29			M	M		very stiff, moist (residual s	soil)
Good 9/18" 5/10/10  Fair 14/24" 4/6/8/7  Good 16/18" 5/11/12  Good 16/18" 5/11/12  Grades with decomposed gravel gravel are more moist (residual soil)  CH Brownish gray to gray FAT CLAY, stiff, very moist (residual soil)  Boring terminated at 22 feet			Fair	15/24"		6/6/6/9				M			
Fair 14/24" 4/6/8/7 4/6/8/7 4/6/8/7 5/11/12 5/11/12 Good 16/18" 5/11/12 Grades with decomposed gravel Brownish gray to gray FAT CLAY, stiff, very moist (residual soil)  Boring terminated at 22 feet								-	1	$\mathscr{U}$			
Fair 14/24" 4/6/8/7  Good 16/18" 5/11/12  Good 16/18" 5/11/12  Grades with decomposed gravel Brownish gray to gray FAT CLAY, stiff, very moist (residual soil)  Boring terminated at 22 feet  Boring terminated at 22 feet								5-	$\Box$	$\mathcal{W}$			-
Fair 14/24" 4/6/8/7  Good 16/18" 5/11/12  Good 16/18" 5/11/12  Grades with decomposed gravel Brownish gray to gray FAT CLAY, stiff, very moist (residual soil)  Boring terminated at 22 feet  Boring terminated at 22 feet			Good	9/18"		5/10/10		-	V	$\mathcal{W}$			
Fair 14/24" 4/6/8/7 Mottled orangish brown to yellowish brown CLAYEY SILT, stiff, moist to very moist (residual soil)  Good 16/18" 5/11/12 grades with decomposed gravel  CH Brownish gray to gray FAT CLAY, stiff, very moist (residual soil)  Boring terminated at 22 feet			0.000	0,10		G/ 1 G/ 1 G		-	Δ	$\mathcal{M}$			
Fair 14/24" 4/6/8/7 Mottled orangish brown to yellowish brown CLAYEY SILT, stiff, moist to very moist (residual soil)  Good 16/18" 5/11/12 grades with decomposed gravel  CH Brownish gray to gray FAT CLAY, stiff, very moist (residual soil)  Boring terminated at 22 feet								-	1	$\mathscr{U}$			
Fair 14/24" 4/6/8/7 Mottled orangish brown to yellowish brown CLAYEY SILT, stiff, moist to very moist (residual soil)  Good 16/18" 5/11/12 grades with decomposed gravel  CH Brownish gray to gray FAT CLAY, stiff, very moist (residual soil)  Boring terminated at 22 feet								10	]	$\mathcal{U}$	/		
Good 16/18"  5/11/12  grades with decomposed gravel  Brownish gray to gray FAT CLAY, stiff, very moist (residual soil)  Boring terminated at 22 feet								10-		11			
Good 16/18"  5/11/12  grades with decomposed gravel  Brownish gray to gray FAT CLAY, stiff, very moist (residual soil)  Boring terminated at 22 feet			Fair	14/24"		4/6/8/7		-		M	MLAMI		ellowish moist to
Good 16/18"  5/11/12  grades with decomposed gravel  Brownish gray to gray FAT CLAY, stiff, very moist (residual soil)  Boring terminated at 22 feet								/	4	<b>}</b> [		very moist (residual soil)	, 1110101 10
Good 16/18"  5/11/12  grades with decomposed gravel  Brownish gray to gray FAT CLAY, stiff, very moist (residual soil)  Boring terminated at 22 feet							١,	/ -	$ \cdot $	}			
Fair 17/24" grades with decomposed gravel  CH Brownish gray to gray FAT CLAY, stiff, very moist (residual soil)  Boring terminated at 22 feet								15-	M	1]/			-
Fair 17/24" 6/9/10/13 20 Brownish gray to gray FAT CLAY, stiff, very moist (residual soil) Boring terminated at 22 feet			Good	16/18"		5/11/12		\	$\overline{\mathbf{V}}$	N			
Fair 17/24" 6/9/10/13 20 Brownish gray to gray FAT CLAY, stiff, very moist (residual soil) Boring terminated at 22 feet										11		grades with decomposed (	rravol
Fair 17/24" 6/9/10/13 20 very moist (residual soil)  Boring terminated at 22 feet								> _			CH	, ,	
Boring terminated at 22 feet			<b>-</b> .	47/04!		0/0/10/1	$\backslash \backslash \backslash$	20 -					-
25-			Fair	17/24"		6/9/10/13	3 \						
25-					$ $ $\langle$ $\langle$		+	-				Boring terminated at 22 fee	at .
						<b>\</b>	+/	-	$\  \ $			Borning terminated at 22 10	
								-	1				
Date/Time Started: March 21, 2018 09:00 Date/Time Completed:March 21, 2018 14:50  Logged By: S. Latronic Driller Name: K. Vongamath Project Engineer: Steven Carr Drill Rig: MINUTEMAN Total Depth: 22 feet Drilling Method: 3" Solid Stem Auger Work Order: 7604-10 Driving Energy: 140 lb. wt., 30 in. drop						$\setminus$		25 -	1				-
Date/Time Started: March 21, 2018 09:00 Date/Time Completed:March 21, 2018 14:50  Logged By: S. Latronic Driller Name: K. Vongamath Project Engineer: Steven Carr Drill Rig: MINUTEMAN Total Depth: 22 feet Drilling Method: 3" Solid Stem Auger Work Order: 7604-10 Driving Energy: 140 lb. wt., 30 in. drop													
Date/Time Started: March 21, 2018 09:00 Date/Time Completed:March 21, 2018 14:50 Logged By: S. Latronic Driller Name: K. Vongamath Project Engineer: Steven Carr Total Depth: 22 feet Drilling Method: 3" Solid Stem Auger Work Order: 7604-10  Date/Time Started: March 21, 2018 09:00 Water Level: ▼ 14.6 ft. 03/22/2018 1320 HRS Plate  Plate Plate  Plate  Plate  Project Engineer: Steven Carr Drilling Method: 3" Solid Stem Auger  Driving Energy: 140 lb. wt., 30 in. drop						,							
Date/Time Started: March 21, 2018 09:00 Date/Time Completed:March 21, 2018 14:50 Logged By: S. Latronic Driller Name: K. Vongamath Project Engineer: Steven Carr Total Depth: 22 feet Drilling Method: 3" Solid Stem Auger Work Order: 7604-10  Date/Time Started: March 21, 2018 09:00 Water Level: ▼ 14.6 ft. 03/22/2018 1320 HRS  Plate Plate Plate Project Engineer: Steven Carr Drill Rig: MINUTEMAN Drilling Method: 3" Solid Stem Auger Work Order: 7604-10 Driving Energy: 140 lb. wt., 30 in. drop								-	1				
Date/Time Started: March 21, 2018 09:00 Date/Time Completed:March 21, 2018 14:50 Logged By: S. Latronic Driller Name: K. Vongamath Project Engineer: Steven Carr Total Depth: 22 feet Drilling Method: 3" Solid Stem Auger Work Order: 7604-10  Date/Time Started: March 21, 2018 09:00 Date/Time Started: March 21, 2018 09:00 Driller Name: K. Vongamath Plate Plate  Project Engineer: Steven Carr Drilling Method: 3" Solid Stem Auger Driving Energy: 140 lb. wt., 30 in. drop	118				,			30 -					-
Date/Time Started: March 21, 2018 09:00 Date/Time Completed:March 21, 2018 14:50 Logged By: S. Latronic Driller Name: K. Vongamath Project Engineer: Steven Carr Total Depth: 22 feet Drilling Method: 3" Solid Stem Auger Work Order: 7604-10  Date/Time Started: March 21, 2018 09:00 Water Level: ▼ 14.6 ft. 03/22/2018 1320 HRS  Plate  Plate Plate  Plate Drilling Method: 3" Solid Stem Auger University of the project Stew Auger  Driving Energy: 140 lb. wt., 30 in. drop	3/23							-					
Date/Time Started: March 21, 2018 09:00 Date/Time Completed:March 21, 2018 14:50 Logged By: S. Latronic Driller Name: K. Vongamath Project Engineer: Steven Carr Total Depth: 22 feet Drilling Method: 3" Solid Stem Auger Work Order: 7604-10  Date/Time Started: March 21, 2018 09:00 Driller Name: K. Vongamath Plate Drilling Method: 3" Solid Stem Auger Driving Energy: 140 lb. wt., 30 in. drop	S.GD1							-	$\mid \mid$				
Date/Time Started: March 21, 2018 09:00 Date/Time Completed:March 21, 2018 14:50 Logged By: S. Latronic Driller Name: K. Vongamath Project Engineer: Steven Carr Total Depth: 22 feet Drilling Method: 3" Solid Stem Auger Work Order: 7604-10  Date/Time Started: March 21, 2018 09:00 Water Level: ▼ 14.6 ft. 03/22/2018 1320 HRS  Plate Plate Plate Plate Drilling Method: 3" Solid Stem Auger Driving Energy: 140 lb. wt., 30 in. drop	<b>JLAB</b>							-	$\mid \mid$				
Date/Time Started: March 21, 2018 09:00 Date/Time Completed:March 21, 2018 14:50  Logged By: S. Latronic Driller Name: K. Vongamath Project Engineer: Steven Carr Drill Rig: MINUTEMAN  Total Depth: 22 feet Drilling Method: 3" Solid Stem Auger Work Order: 7604-10 Driving Energy: 140 lb. wt., 30 in. drop	J GEC												
Date/Time Completed:March 21, 2018 09.00  Logged By: S. Latronic Driller Name: K. Vongamath Project Engineer: Steven Carr Total Depth: 22 feet Drilling Method: 3" Solid Stem Auger Work Order: 7604-10  Date/Time Completed:March 21, 2018 09.00  Driller Name: K. Vongamath Plate  Project Engineer: Steven Carr Drilling Method: 3" Solid Stem Auger Driving Energy: 140 lb. wt., 30 in. drop	10.GP	Dato/Timo Sto	rtod: N	March 21	2010 00	1:00	Water		. •	1	1 E f+	03/22/2018 1220 LIDS	
Logged By: S. Latronic Driller Name: K. Vongamath Project Engineer: Steven Carr Drill Rig: MINUTEMAN Total Depth: 22 feet Drilling Method: 3" Solid Stem Auger Work Order: 7604-10 Driving Energy: 140 lb. wt., 30 in. drop	7604-						vvalei L	evel	. 🛂	11	4.0 II	. 03/22/2010 1320 1113	
Project Engineer: Steven Carr Drill Rig: MINUTEMAN Total Depth: 22 feet Drilling Method: 3" Solid Stem Auger Work Order: 7604-10 Driving Energy: 140 lb. wt., 30 in. drop	3AFT		•				Driller N	lame	:	K	. Vor	ngamath	Plate
Total Depth: 22 feet Drilling Method: 3" Solid Stem Auger Work Order: 7604-10 Driving Energy: 140 lb. wt., 30 in. drop	OG DF												
Work Order: 7604-10 Driving Energy: 140 lb. wt., 30 in. drop	NG LC							od:					
	BORI	Work Order:	-	7604-10			Driving	Ener	gy:	1	40 lb	. wt., 30 in. drop	

Geotechnical Engineering

### GROUNDWATER SPRING DISCHARGE Hawaiian Memorial Park

Log of Boring

	<u> </u>											_
		Field					П			Approximate Ground		
(0		t f	, ath			1				Elevation (feet ):		
] set		gth/ eng	gth, enç		en.	ef (				Latitude:21.39 Longitude: -157.7		
Ž	<u>o</u> >	le L	en le L		٠.	(fe	<u>e</u>	.≌		Zongilado. 107.		
Orilling Notes	Sample Quality	Rec. Length/ Sample Length (inches)	RQD Length/ Sample Length (inches)	Blows/ 6"	Pocket Pen. (tsf)	Depth (feet)	Sample	Graphic	nscs	Description	าท	
مَ ا	йŌ	R. W.F.	R S F	6 B	<u> </u>	ے	Š	ō arar	_ ⊃ MH	•		
	Good	16/18"		11/13/26	2	-		W	IVIII	Orangish brown with trace brown <b>CLAYEY SILT</b> , stiff	to very stiff.	-
	Good	10/10		11/13/20	5	-	X	₩		moist (residual soil)	to 101, 0 til,	-
	Fair	19/24"		8/8/10/9	)	-		₩				-
						-	<b>₩</b>	W				-
						5-	$\Box$	W		grades with trace gray silty	, clay seams	-
	Good	8/18"		8/9/12		-		₩		locally	Clay Scarris	-
	aoou	0/10		0/3/12		-	X	W		,		-
						-	$\prod$	W				-
						-	1	W	/			-
						10-	1	W				-
	Fair	13/24"		3/4/5/7		-		₩				-
	I all	10/24		0/4/3/1		-		XV.	$/ \setminus$	grades with decomposed of	aravol	-
					1	¥ /		$\mathcal{U}$		grades with decomposed (	graver	-
						/ ;	Y	<u> </u>	СH	Brownish gray to gray <b>FAT</b>	CI AV stiff	
						15-			/	moist to very moist (resid		-
	Good	17/18"		4/7/8		/				,	,	-
	accu	17710		( (		_	M					-
					// /_							-
						<b>/</b> /~						-
			/			20 -	1					-
	Fair	24/24"		3/4/4/7	\ \	-				grades with brown clayey :	silt seams	-
		,		0,7,1,1,1	+>	1 -	Y			\ locally	ont coarrie	7
				\ \ \ \	+/	-	$\vdash$			Boring terminated at 23 fe	et	
						-	1					-
						25 -	1					-
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Date/Time Sta		I.				35-	Ш					
Date/Time Sta			, 2018 08		Water L	.evel	<b>T</b>	13	3.3 ft	. 03/22/2018 1315 HRS		
Date/Time Co			-	1:00	Driller N							
Logged By:										ngamath	Plate	
Project Engine		arr		Drill Rig: MINUTEMAN								
Logged By: Project Engine Total Depth: Work Order:	2		Drilling Method: 3" Solid Stem Auger									
Work Order:	7			Driving	Ener	gy:	14	40 lb.	. wt., 30 in. drop			

### Appendix C

Logs of the B-1 and B-2 Boreholes Drilled in Ocean View Garden by Geolabs, Inc.



Geotechnical Engineering

PHASE I POTENTIAL ROCKFALL AND SLOPE HAZARD ASSESSMENT HAWAIIAN MEMORIAL PARK CEMETERY EXPANSION TMK: 4-5-033: 001 KANEOHE, OAHU, HAWAII Log of Boring

	2.203												
Labo	Laboratory Field												
Other Tests	Moisture Content (%)	Density f)	Core Recovery (%)	RQD (%)	Penetration Resistance (blows/foot)	Pocket Pen. (tsf)	Depth (feet)	Sample	Graphic	SS	Approximate Ground Surface Elevation (feet ): 269 *		
Oth	Mois	Dry [ (pcf)	Cor	RQI	Pen Res (blo	Poc (tsf)	Dep	San	Gra	nscs	Description		
	50 54	62			12 5	4.0	-	X		MH MH	Orangish brown <b>CLAYEY SILT</b> with a little grave (basaltic), very stiff, moist (fill)  Mottled orangish brown <b>CLAYEY SILT</b> with som sand, very stiff, moist (residual soil)	H	
Direct Shear	56	62			9	4.0	5 <del>-</del>	X			Mottled orangish brown with some dark gray CLAYEY SILT with some sand and traces of decomposed gravel, stiff to very stiff, moist (saprolite)	-	
LL=72 PI=22	62				6		10 -						
TXCU					7	4.0	- - 15 - -	X			grades with yellowish brown mottling locally	- - - -	
	49				17		20 -				grades more clayey locally	- - -	
	53	70			24	4.0	25 - -	X				- - -	
LL=79 PI=30  Date Star Date Com Logged B Total Dep Work Ord	59				11		30					- - - -	
							35-						
Date Star	Date Started: October 12, 2017							l: <u>▼</u>	N	lot E	ncountered		
Date Con	Date Completed: October 12, 2017										Plate		
Logged B							45C TRUCK (Energy Transfer Ratio = 78%)						
Total Dep		Drilling Method: 4" Solid Stem Auger  A						1					
Work Ord			Driving Energy: 140 lb. wt., 30 in. drop										



Geotechnical Engineering

PHASE I POTENTIAL ROCKFALL AND SLOPE HAZARD ASSESSMENT HAWAIIAN MEMORIAL PARK CEMETERY EXPANSION TMK: 4-5-033: 001 KANEOHE, OAHU, HAWAII Log of Boring

- W	<i>V</i>											
Lab	Laboratory Field											
Direct Tests	G Moisture Content (%)	Dry Density (pcf)	Core Recovery (%)	RQD (%)	Penetration Resistance (blows/foot)	N Pocket Pen. യ (tsf)	Depth (feet)	Sample	Graphic	nscs	(Continued from previous plat	e)
Shear  LL=66	55 51	69	OIL	ш_	18	2.3	40 -			MH	grades with highly weathered basalt locally	corestones
Pl=33							50		XX		grades to very moist  Boring terminated at 46.5 feet  * Elevations based on available Gra Ocean View Gardens.	ding Plan for
Date Star Date Con Logged E Total Dep Work Ord	rted:	Octo	ber 12	, 2017		<b>V</b> ater I	65     		<u> </u>	Not E	ncountered	
Date Con								Plate				
Logged E		Drill Rig: CME-45C TRUCK (Energy Transfer Ratio = 78%) Drilling Method: 4" Solid Stem Auger A - 1.						A - 1.2				
Work Ord	Work Order: 7604-00									140 lk	o. wt., 30 in. drop	



Geotechnical Engineering

PHASE I POTENTIAL ROCKFALL AND SLOPE HAZARD ASSESSMENT HAWAIIAN MEMORIAL PARK CEMETERY EXPANSION TMK: 4-5-033: 001 KANEOHE, OAHU, HAWAII Log of Boring

Laboratory Field							<u> </u>						
			Density f)	Core Recovery (%)			Pocket Pen. (tsf)	(teet)	Φ	ic		Approximate Ground Surface Elevation (feet ): 263 *	
	Other Tests	Moisture Content (%)	Dry De (pcf)	Core	RQD (%)	Penetration Resistance (blows/foot)	Pocke (tsf)	Depth (feet)	Sample	Graphic	nscs	Description	
		34	82			40	4.5	-	V		МН	Brown <b>CLAYEY SILT</b> with some sand and traces of gravel (basaltic), very stiff to hard, moist (fill)	
	LL=66	34				30		-					-
	PI=29	32	86			34	4.5	5 <del>-</del>					-
		37	00			40	4.5	-	X				_
						-		-			MH	Mottled orangish brown <b>CLAYEY SILT</b> , very stiff to hard, moist (residual soil)	-
	LL=65 PI=8	35	77			68	4.5	10 -	X		MH	Mottled grayish brown with some orange CLAYEY SILT with some sand and a little decomposed gravel, hard, moist (saprolite)	
		55				6		15 – -			МН	Mottled orangish brown <b>CLAYEY SILT</b> with some sand, stiff to very stiff, moist (saprolite)	 ; 
	Direct Shear	54	50			16	3.5	20 -	X			grades more sandy locally	-
	LL=81 PI=21	65				5		25 - - -					-
	Direct Shear	71	57			13	2.3	30 -	X				-
GEOLAI								35-				grades more clayey	-
04-00.GF	Date Started: October 12, 2017						Water L		l: <u>¥</u>	١	Not E	incountered Plate	
	Date Completed: October 12, 2017  Logged By: S. Latronic						Drill Rig		45C TRUCK (Energy Transfer Ratio = 78%)				
	Total Depth: 46.5 feet						Drilling Method: 4" Solid Stem Auger  A -						
L	Work Order: 7604-00 Driving Energy: 140 lb. wt., 30 in. drop												



Geotechnical Engineering

PHASE I POTENTIAL ROCKFALL AND SLOPE HAZARD ASSESSMENT HAWAIIAN MEMORIAL PARK CEMETERY EXPANSION TMK: 4-5-033: 001 KANEOHE, OAHU, HAWAII Log of Boring

Labo	ield											
S	(9)	\ \	(%)		ا ا	۸.	t)					
Test	ure ent (%	ensit	very (	(%)	tratio	et Pe	ee) ι	<u>le</u>	Jic	(0	(Continued from previous plat	e)
Other Tests	Moisture Content (%)	Dry Density (pcf)	Core Recovery (%)	RQD (%)	Penetration Resistance (blows/foot)	Pocket Pen. (tsf)	Depth (feet)	Sample	Graphic	nscs	Description	
	50				17		-			MH	Mottled yellowish brown and gray <b>CL</b> with a little gravel (basaltic) and rer structure, very stiff, moist (saprolite	nnant rock
	44	77			26	3.5	40 -	X				- - -
	23				19		- 45 -				grades with highly weathered basalt locally	corestones - - -
							-		11/		grades more silty	
							_	-			Boring terminated at 46.5 feet	-
							-					-
							50 -					_
							_					-
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							55 -					-
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05.65 05.05 05 05.05 05 05.05 05 05 05 05 05 05 05 05 05 05 05 05							_					=
EOLAE							_	$\left\{ \ \ \right\}$				-
Date Star Date Com Logged B Total Dep Work Ord							70 <b>-</b>	<u> </u>			<u> </u>	
Date Star Date Com			ber 12			Vater I	_eve	l: 🔽	_ \	Not E	ncountered	Plate
E Logged B			atronic	, 2017		Drill Rig	45C TRUCK (Energy Transfer Ratio = 78%)	rialt				
Total Dep		Drilling Method: 4" Solid Stem Auger A - 2.2										
Work Ord		Driving Energy: 140 lb. wt., 30 in. drop										