

APPENDIX L

Traffic Impact Analysis Report



WAIKAPU COUNTRY TOWN TRANSPORTATION IMPACT ANALYSIS REPORT - FINAL

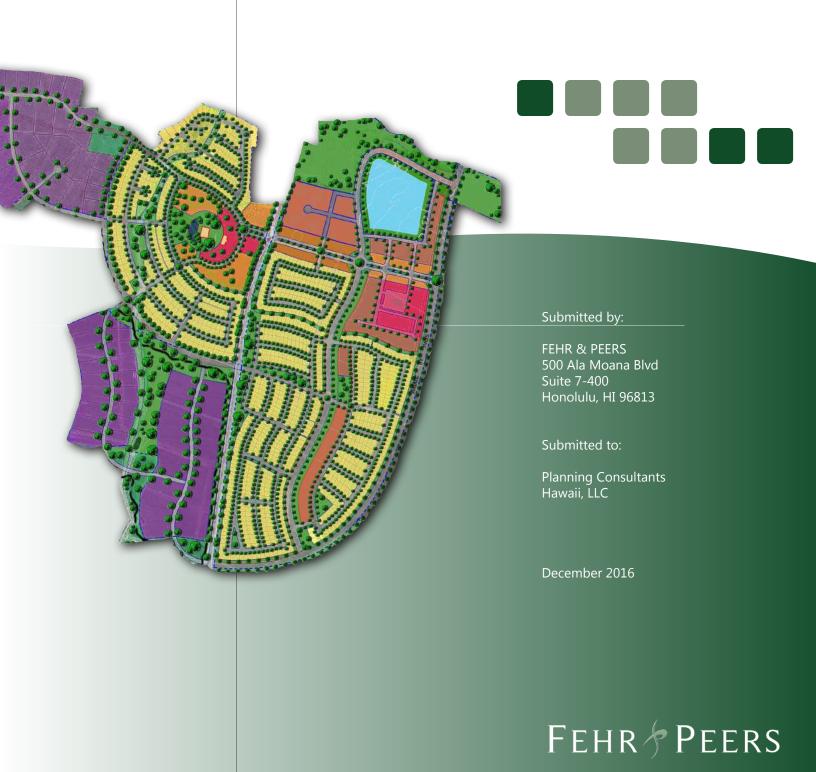


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1. EXECUTIVE SUMMARY

This report presents the results of the Transportation Impact Analysis (TIAR) for the Waikapu Country Town Project (the Project).

The Project. The Project is a mixed use neighborhood development on mostly undeveloped land south of Waiko Road in the Waikapu community in Central Maui. It is located on both the mauka and makai side of Honoapiilani Highway (Highway 30).

The Project will be developed in two phases: 2017 through 2021 is the first phase, and the second phase will be from 2022 through 2026. Figure A in this Executive Summary depicts the proposed land use plan and street network for the Project, and more detail is provided in Figures 2 and 10 in the report.

Two Phases. The first phase is to be developed as a "Village Center" on the mauka side of Honoapiilani Highway and will contain approximately 170,000 square feet of commercial and employment uses, as well as 731 residential units, an elementary school and 27 acres of park and open space. Phase 2 will include: 848 residential units and approximately 6 acres of park and open space. Primary access would be provided via Honoapiilani Highway and Waiale Road, via the planned southward extension of Waiale Road known as the Waiale Bypass. Much of the right-of-way necessary to construct the Waiale Bypass lies within the Project site.

Project Site Plan. The proposed site plan provides an extensive internal roadway system which will provide community residents and visitors multiple options for accessing neighborhoods, employment centers, commercial areas, and institutional uses. The Project embodies Country Town Design principles that include a country sense of place with a mix of uses, and fosters walkability and connectivity through pedestrian/bicycle routing, with bridges and approximately 8 miles of hiking, biking, and walking trails. These characteristics promote the use of non-motorized modes, especially for short commutes, and help to reduce external vehicle trip generation.

Study Methodology. The study first forecasts traffic volumes based without the development of the Project, and then forecasts volumes with the development of each phase of the Project. It documents estimated traffic movements at the analyzed intersections and determines volume-to-capacity (V/C) ratios, average delay times and the resulting level of service (LOS) ratings. This study recommends specific mitigation measures to address locations where undesirable levels of service are projected. The project site plan and study area are depicted in Figure A in this Executive Summary.

Vehicle Trip Generation. The first phase of the Project is estimated to generate approximately 13,100 week day daily trips including approximately 700 trips during the weekday morning peak hour and 1,000 trips during the weekday afternoon peak hour. At the end of the second phase, the Project would

generate a total of approximately 19,000 weekday trips including approximately 1,200 trips in the weekday AM peak hour and 1,500 trips in the weekday PM peak hour.

Intersection Analysis. The traffic impact analysis was evaluated pursuant to guidelines established by the County of Maui and the Hawaii Department of Transportation-Highways Division-Planning Branch. Weekday a.m. and p.m. peak hour capacity analysis was conducted for eight (8) existing and six (6) future intersections in the vicinity of the Project site. Under the current baseline 2013 conditions, seven (7) of the eight (8) existing intersections are operating at the desired LOS of D or better during the weekday peak hours. The existing intersection LOS analysis is presented in Table 3 of the report.

Future Conditions without Project. The future intersection operating conditions will be significantly affected by regional growth and development in the study area before project implementation. By 2022 and 2026 the Project area will have experienced significant residential and commercial growth and due to the development of neighboring projects including Waiale, Maui Lani Development, Kehalani Development, Puunani residences, and other developments as outlined in Table 4. Future regional development will be accompanied by roadway network changes will improve mobility options for residents and visitors, as well as expand roadway capacity at various locations within the study area. Nevertheless, with this growth, five (5) of the 14 study intersections are projected to operate at an undesirable LOS E or F during one or both peak hours in each future year.

Project Traffic Impact. The traffic analysis addressed the completion of the first phase (2022) and the second phase (2026) with the Project. Following development of both the first phase and second phase of the Project, six (6) of the fourteen (14) intersections studied (Intersection 1-4 and 7-8) would operate at LOS (E) or (F) in either the AM and/or PM peak hour. As noted above, all but one of these six intersections (Intersection 8) are projected to operate at undesirable levels without the addition of project traffic. Eight (8) of the study intersections (Intersections 5-6 and 9-14) are projected to operate at acceptable LOS with buildout of the project and will not require mitigation strategies. See Tables 6 and 7.

Mitigation Strategies. Mitigation strategies were developed to identify recommended improvements at the intersections with projected overall intersection levels of service, LOS (E) or LOS (F) in the years 2022 and 2026. Each of the identified project-related and cumulative impacts would be fully mitigated (achieving LOS D or better for intersection operations) with recommended improvements as described in Chapter 5 and Appendix F of the TIAR. In some cases, certain individual turning movements or approaches would continue to operate at LOS (E) or (F), even with overall intersection mitigation. However, further mitigation measures to address specific turning movement or approach operations are not recommended because they do not meet typical traffic engineering guidelines or would result in atypical improvements (i.e., triple left-turn lanes) that could have significant right-of-way impacts or change community character. The estimated share of traffic mitigation cost shown on Table 8 was calculated for proposed mitigations under Year 2026 with project conditions.

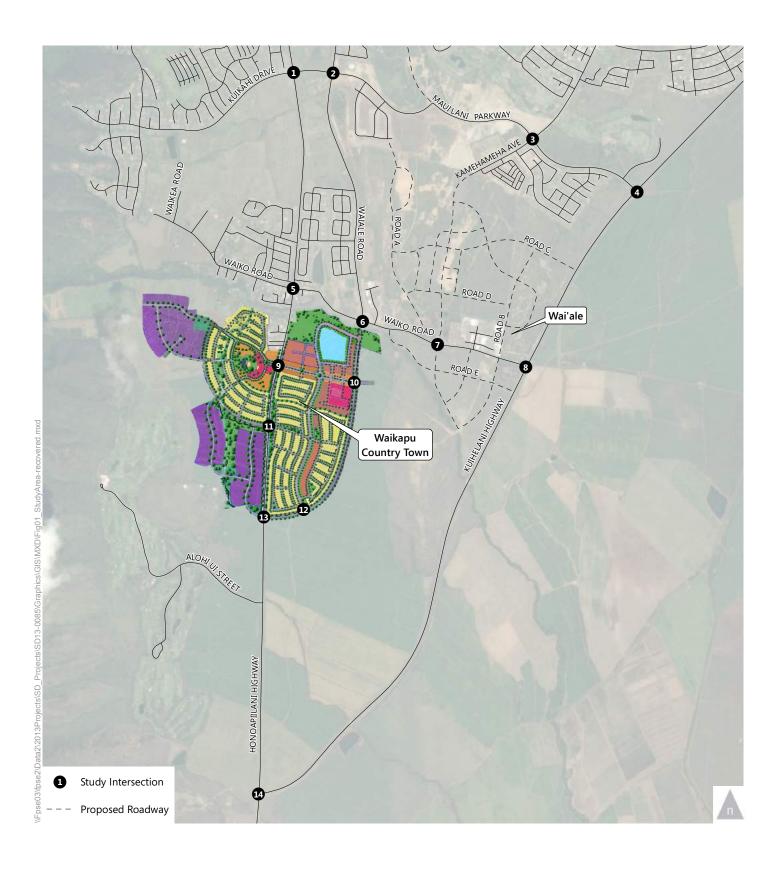




Figure A

2. INTRODUCTION

This transportation impact analysis report (TIAR) presents the results of the study conducted by Fehr & Peers for the proposed Waikapu Country Town Project (hereafter "WCT" or "Project") located in the area of south Waikapu in Central Maui, which is approximately two miles south of Wailuku. The purpose of this analysis is to identify the impacts of the proposed project on the surrounding transportation system. The TIAR includes a description of the assumptions and methods used to conduct the study, as well as a discussion of the results. This TIAR was conducted in accordance with the requirements of the affected government agencies.

PROJECT DESCRIPTION

The project would construct a new mixed-use neighborhood on approximately 500 acres of mostly undeveloped land south of Waiko Road on both the mauka and makai side of Honoapiilani Highway (Highway 30). The proposed development site lies within the County's adopted urban growth boundary and is part of larger property that totals approximately 1,562 acres. The area outside of the proposed WCT site will remain in agricultural use within the State's Agricultural District. **Figure 1** illustrates the study area of the proposed project.

WCT will be built in two phases through 2026 and the proposed land use plan and street network for the project is illustrated on **Figure 2**. The "village center" type development on the mauka side of Honoapiilani Highway is proposed to be constructed in the first phase, 2017 through 2021. Phase 1 also includes the development of residential parcels directly north and northwest of the "village center," as well as the northern half of the project site on the makai side of Honoapiilani Highway. Phase 1 is programmed as follows:

- 332 single-family dwelling units;
- 15 rural residential units;
- 216 mixed-use multi-family dwelling units;
- 41 "ohana" units;
- 127 country town mixed-use residential units;
- 58,475 square feet of country town mixed-use commercial;
- 111,122 square feet of new commercial and employment;
- an elementary school (12 acres); and
- 26.66 acres of parks and open space.

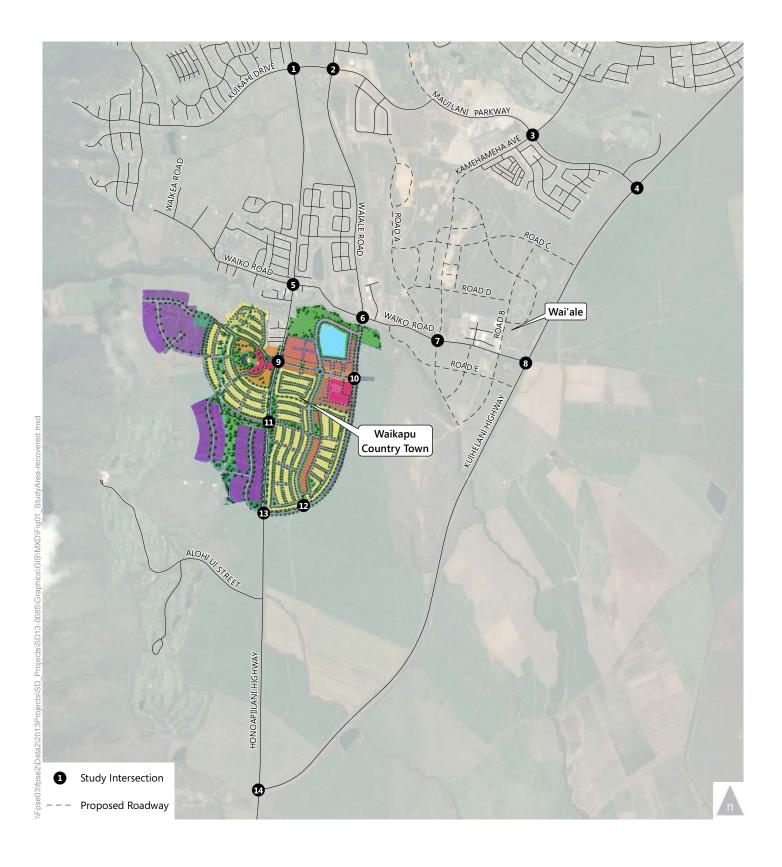




Figure 1 Study Area and Analyzed Intersections





Figure 2
Conceptual Site Plan

Additionally, it is assumed that the 29,250 square feet of existing commercial uses located in the same area as the "village center" will remain.

Phase 2 of the development program, 2022-2026, will construct the remainder of the project and includes:

- 638 single-family dwelling units;
- 65 rural residential units;
- 40 multi-family dwelling units;
- 105 "ohana" units; and
- 5.78 acres of parks and open space.

Primary access would be provided via Honoapiilani Highway and Waiale Road via the planned southward extension of Waiale Road, known as the Waiale Bypass.

PROJECT STUDY AREA

The study analyzed the potential project-related traffic impacts under typical weekday AM and PM peak hour traffic conditions at partial buildout in 2022 and at full buildout in 2026. The transportation analysis evaluated the operations at eight existing and six future intersections (a total of 14 study intersections) in the vicinity of the proposed project. The analyzed intersections are listed below and are shown in **Figure 1**:

- 1. Honoapiilani Highway (Highway 30)/Kuikahi Drive
- 2. Waiale Road/Kuikahi Drive
- 3. S. Kamehameha Avenue/Maui Lani Parkway
- 4. Kuihelani Highway (Highway 380)/Maui Lani Parkway
- 5. Honoapiilani Highway (Highway 30)/Waiko Road
- 6. Waiale Road/Waiko Road
- 7. S. Kamehameha Avenue/Waiko Road*
- 8. Kuihelani Highway (Highway 380)/Waiko Road
- 9. Honoapiilani Highway (Highway 30)/Main Street*
- 10. Waiale Road/Main Street*
- 11. Honoapiilani Highway/East-West Residential Street*
- 12. North-South Residential Street/ Waiale Road*
- 13. Honoapiilani Highway (Highway 30)/Waiale Road*
- 14. Honoapiilani Highway (Highway 30)/Kuihelani Highway (Highway 380)

 *Future intersection

INTERSECTION ANALYSIS SCENARIOS

The operations of the study intersections were evaluated during the weekday morning and evening peak hours for the following scenarios:

- <u>Scenario 1: Existing (2013) Conditions</u> The analysis of existing traffic conditions was based on 2013 counts collected for analyzed peak hours. The existing conditions analysis includes a description of key area streets and highways, and an assessment of traffic volumes and intersection operating conditions.
- Scenario 2: Year 2022 No Project Conditions Future Year 2022 volumes were projected using the Maui Travel Demand Forecasting Model (TDFM). Traffic from approved but not yet constructed (and possibly pending) developments in the area were also be added to this scenario. Although the anticipated completion year of the first phase of the WCT development is 2021, the Phase 1 traffic impact analysis was conducted for 2022 to be consistent with the planned completion of large background projects in the area, such as the Waiale development and the Waiale Bypass, and to provide a conservative analysis.
- <u>Scenario 3: Year 2022 with Partial Development Conditions</u> Traffic projections from Scenario 2 plus traffic estimates from the first phase of project development.
- <u>Scenario 4: Year 2026 No Project Conditions</u> Future volumes in the anticipated year of project buildout and full occupancy were projected using the Maui TDFM. Traffic from approved and pending developments in the area not included in Scenario 2 is added in this scenario.
- Scenario 5: Year 2026 with Project Conditions Traffic projections from Scenario 4 plus traffic estimates anticipated from project buildout and full occupancy.

TRAFFIC ANALYSIS METHODS

The analysis of roadway operations performed for this study is based on procedures presented in the *Highway Capacity Manual* (HCM), published by the Transportation Research Board in 2000. Although the 2010 *HCM* was available at the time this report was published; not many jurisdictions have yet adopted the 2010 HCM, as many LOS software programs are still fine tuning versions incorporating updated 2010 methods. Differences in analysis results for intersection level of service (LOS) evaluation have been found to be negligible between the 2000 and 2010 HCM and are not expected to change the conclusions of this report.

The operations of roadway facilities are described with the term level of service. LOS is a qualitative description of traffic flow based on such factors as speed, travel time, delay, and freedom to maneuver. Six

levels are defined from LOS A, with the least congested operating conditions, to LOS F, with the most congested operating conditions. LOS E represents "at-capacity" operations. Operations are designated as LOS F when volumes exceed capacity, resulting in stop-and-go conditions. The methodologies for signalized and unsignalized intersections are described below.

SIGNALIZED INTERSECTIONS

The method described in Chapter 16 of the 2000 *Highway Capacity Manual* was used to prepare the LOS calculations for the signalized study intersections. This LOS method analyzes a signalized intersection's operation based on average control delay per vehicle. Control delay includes the initial deceleration delay, queue move-up time, stopped delay, and final acceleration delay. The average control delay for signalized intersections is calculated using Synchro analysis software and is correlated to a LOS designation as shown in **Table 1**.

TABLE 1 – SIGNALIZED INTERSECTION LEVEL OF SERVICE DEFINITIONS

| Level of Service | Description | Average Control Delay Per Vehicle (Seconds) | |
|---|--|--|--|
| А | Operations with very low delay occurring with favorable progression and/or short cycle lengths. | ≤ 10.0 | |
| В | Operations with low delay occurring with good progression and/or short cycle lengths. | 10.1 to 20.0 | |
| С | Operations with average delays resulting from fair progression and/or longer cycle lengths. Individual cycle failures begin to appear. | 20.1 to 35.0 | |
| D | Operations with longer delays due to a combination of unfavorable progression, long cycle lengths, and high V/C ratios. Many vehicles stop and individual cycle failures are noticeable. | 35.1 to 55.0 | |
| E | Operations with high delay values indicating poor progression, long cycle lengths, and high V/C ratios. Individual cycle failures are frequent occurrences. | 55.1 to 80.0 | |
| F | Operations with delays unacceptable to most drivers occurring due to over-saturation, poor progression, or very long cycle lengths. | > 80.0 | |
| Source: <i>Highway Capacity Manual</i> , Transportation Research Board, 2000. | | | |

UNSIGNALIZED INTERSECTIONS

The operations of the unsignalized intersections were evaluated using the method contained in Chapter 17 of the 2000 *Highway Capacity Manual*. LOS ratings for stop-sign-controlled intersections are based on the average control delay expressed in seconds per vehicle. At two-way or side-street-controlled intersections, the average control delay is calculated for each stopped movement, not for the intersection as a whole. For approaches composed of a single lane, the control delay is computed as the average of all movements in that lane. For approaches with multiple lanes, the control delay is computed for each movement; the movement with the worst (i.e., longest) delay is presented. The average control delay for unsignalized intersections is calculated using Synchro analysis software and is correlated to a LOS designation as shown in **Table 2**.

TABLE 2 – UNSIGNALIZED INTERSECTION LEVEL OF SERVICE DEFINITIONS

| Level of Service Description | | Average Control Delay Per Vehicle (Seconds) | |
|---|---------------------------|--|--|
| А | Little or no delay. | ≤ 10.0 | |
| В | Short traffic delay. | 10.1 to 15.0 | |
| С | C Average traffic delays. | | |
| D | D Long traffic delays. | | |
| E Very long traffic delays. 35.1 to 50.0 | | | |
| F Extreme traffic delays with intersection capacity exceeded. > 50.0 | | | |
| Source: Highway Capacity Manual, Transportation Research Board, 2000. | | | |

SIGNIFICANT IMPACT CRITERIA

The analysis of future conditions compares baseline scenarios with Phase 1 of the project and full buildout year of the project to determine whether the project traffic is expected to result in a significant impact on the surrounding roadways. Based on previous studies conducted for the County of Maui, the minimum acceptable operating standard for a signalized intersection is LOS D for the overall intersection. Additionally, the Hawaii Department of Transportation (HDOT) strives to universally maintain LOS D conditions and in their *HDOT Best Practices for Traffic Impact Report* (June 2012) defines a significant impact when the operations of an intersection, turning movement, or roadway segment changes from LOS D or better to LOS E or F. Also when evaluating intersection approach LOS at any location, other

factors should be considered in the analysis, such as traffic volumes, volume-to-capacity (V/C) ratios (should ideally be less than 1.00), and secondary impacts to pedestrian, bicycle, and transit travel.

Each of the identified significant impacts could be further categorized as either a cumulative impact or a project-related impact. If the addition of project traffic is expected to degrade acceptable service levels (LOS D or better) to unacceptable service levels (LOS E or F) then the project is considered to have a project-specific impact. Whereas, if the LOS for any roadway element is LOS E or F without the project and the project adds traffic to this location, causing the delay to increase by 5% or more, then this would be characterized as a cumulative impact.

For unsignalized intersections, the project is determined to have a significant cumulative impact when it adds traffic to a study location that includes a controlled approach that operates at an unacceptable level (i.e., LOS E or F). If the addition of project traffic causes an unsignalized intersection to degrade from LOS D or better to LOS E or F, then the impact is considered project-specific.

The County of Maui does not publish impact criteria for pedestrian, bicycle, and transit impacts. However, these impacts are generally evaluated based on whether a proposed project would: 1) conflict with existing or planned pedestrian, bicycle, or transit facilities, or 2) create walking, bicycling, or transit use demand without providing adequate and appropriate facilities for non-motorized mobility. The existing amenities for pedestrians, bicycles, and transit users were inventoried to evaluate the quality of the facilities in place today. Planning documents affecting future non-motorized transportation in the study area, including the draft Federal-Aid Highways 2035 Transportation Plan for the District of Maui, the Central Maui Pedestrian and Bicycle Master Plan for 2030, and the Bike Plan Hawaii, were reviewed to assess the compatibility of the project with planned future conditions for non-automobile modes.

REPORT ORGANIZATION

The remainder of this report is divided into six chapters, including this Introduction. The existing transportation system serving the project site and the current operating conditions of the key intersections are described in **Chapter 2** Existing Conditions. **Chapter 3** summarizes the methodologies used to forecast future cumulative and project traffic volumes and the resultant forecasts. **Chapter 4** presents an assessment of future traffic impacts at intersections in the surrounding area and identifies mitigation measures to address both cumulative and project-specific impacts. **Chapter 5** contains an assessment of the potential effect of the project on future transit, bicycle, and pedestrian facilities and discusses the project's site access and circulation. Finally, **Chapter 6** summarizes the conclusions of the study.

3. EXISTING CONDITIONS

A comprehensive data collection effort was undertaken to identify existing transportation conditions in the vicinity of the proposed project. The assessment of existing conditions relevant to this study includes an inventory of the street and highway system, traffic volumes on these facilities, and operating conditions at key intersections. Existing public transit service and bicycle and pedestrian facilities are also described.

EXISTING TRANSPORTATION FACILITIES

This section describes the significant roadway facilities in the study area, as well as the existing transit, bicycle, and pedestrian facilities.

EXISTING STREET SYSTEM

Primary regional access to the area is provided by Honoapiilani Highway, which traverses directly through the middle of the project site, and by Kuihelani Highway, which is located east of the project site. The key roadways providing access to the site are described below. **Figure 1** illustrates the proposed project location and the surrounding roadway system.

Honoapiilani Highway (Highway 30) provides regional access around the western side of Maui and links West Maui with Central Maui. The roadway is initially classified as a principal arterial in downtown Wailuku and as it extends south to Waikapu and Maalaea. As the roadway runs through Lahaina in West Maui, it transitions into a minor arterial. Through the regions of Kapalua and Honolua, it is classified as a collector roadway, and ends in Honokohau Bay, where it becomes Kahekili Highway. In the project area, this undivided arterial runs north-south and provides two travel lanes (one in each direction) with separate lanes for left and right turns at many intersections. Parking is not permitted on most segments of Honoapiilani Highway, and sidewalks are not provided. The posted speed limit ranges between 30 to 45 miles per hour (mph).

Kuihelani Highway (Highway 380) is a north-south, four-lane divided arterial with a posted speed limit of 45 or 55 mph in the study area. The roadway begins at its intersection with Puunene Avenue and Dairy Road in Kahului and extends southward until it terminates at its intersection with Honoapiilani Highway north of Maalaea Harbor.

Waiale Road is a north-south, undivided collector road that starts as an extension of Lower Main Street and terminates at Waiko Road. The roadway provides two travel lanes (one in each direction) and serves

as the only access road for residents of the Waikapu Gardens neighborhood located between Kuikahi Drive and Waiko Road. The posted speed limit is 20 mph.

Kuikahi Drive is an east-west, undivided collector road with two travel lanes (one in each direction). West of its intersection of Honoapiilani Highway, Kuikahi Drive passes through the Wailuku Heights Development until it terminates at a cul-de-sac. Approximately 1,000 feet east of its intersection with Honoapiilani Highway, the roadway terminates at its intersection with Waiale Road and Maui Lani Parkway. The posted speed limit is 20 to 30 mph in the study area.

Kamehameha Avenue is a north-south collector road with two travel lanes (one in each direction). Kamehameha Avenue begins at its intersection of Hana Highway and extends southward through the Maui Lani development until it terminates just south of Pomakai Elementary School. In the project study area, sidewalks are provided along most segments and the posted speed limit is 20 mph.

Maui Lani Parkway is an east-west, divided collector road with two travel lanes (one in each direction) and a raised median. Maui Lani Parkway begins as the east leg of where Kuikahi Drive intersects with Waiale Road and extends eastward until it terminates at its intersection with Kuihelani Highway. The posted speed limit is 20 mph.

Waiko Road is an east-west, undivided collector road with two travel lanes (one in each direction). Waiko Road begins in a residential neighborhood west of Honoapiilani Highway and traverses through mostly residential and industrial uses until it terminates when it intersects Kuihelani Parkway. In the project area, Waiko Road is a narrow, winding 20 to 30 mph road with no sidewalks provided and limited street parking opportunities.

EXISTING TRANSIT FACILITIES

The Maui Bus service, operated by Roberts Hawaii, provides public transit service around the island with 13 bus routes. Each route operates seven days a week, including holidays.

The Lahaina Islander Route (#20) is the only Maui Bus that serves the Waikapu area, which provides hourly service between the Wharf Cinema Center in Lahaina, Maia'aea Harbor Village, and Waikapu, before it originates and terminates at the Queen Ka'ahumanu Center in Kahului. In the study area, this route operates along Honoapiilani Highway with a bus stop approximately 2,000 feet north of the project site at the intersection of Honoapiilani Highway and Waiko Road.

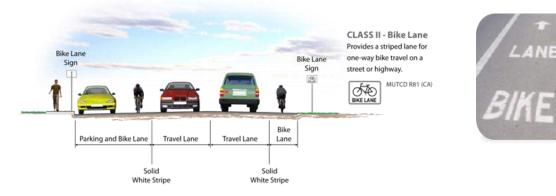
EXISTING BICYCLE FACILITIES

Bicycle facilities generally consist of three types of facilities, which are outlined below:

<u>Bike or Shared Use Paths</u> provide a completely separate right-of-way and is designated for the
exclusive use of bicycles and pedestrians with vehicle and pedestrian cross-flow minimized.
Generally, the recommended pavement width for a two-directional shared use path is ten (10)
feet.



• <u>Bike Lanes</u> provide a restricted right-of-way and is designated for the use of bicycles with a striped lane on a street or highway. Bicycle lanes are generally five (5) feet wide. Adjacent vehicle parking and vehicle/pedestrian cross-flow are permitted.



• <u>Bike Route or Signed Shared Roadways</u> provide for a right-of-way designated by signs or pavement markings for shared use with pedestrians or motor vehicles.



In 2003, the HDOT released the *Bike Plan Hawaii* to provide a blueprint for integrating bicycle facilities into the State's transportation system and enhancing the bicycle environment for its residents and visitors. *Bike Plan Hawaii* is the most current document that presents a comprehensive existing bicycle facility inventory for Maui. The *Bike Plan Hawaii* (2003) reported the island of Maui has 37.8 miles of bicycle facilities that are signed shared roads, 21.6 miles of bicycle lanes, and one mile of shared use path.

In March 2012 the State of Hawaii's Department of Health, Healthy Hawaii Initiative prepared a bicycle and pedestrian master plan for Central Maui, entitled *Central Maui Pedestrian & Bicycle Master Plan for 2030*. The report documents existing pedestrian and bicycle facilities within the region, current gaps in these facilities, and a detailed capital improvements program to significantly increase walking and bicycling. The Plan's major recommendations include:

- Initiating a comprehensive signage and striping program;
- Establishing a "bicycle" district within Kahului that emphasizes separating pedestrians and bicyclists from traffic by installing separated cycle/pedestrian tracks along Papa and Wakea Avenues and calming traffic along residential streets;
- Establishing "pedestrian" districts that emphasizes mixed-use development, wide sidewalks and pedestrian amenities within the core commercial districts of Wailuku and Kahului;
- Establishing a pedestrian/bicycle esplanade along the Kahului Beach Road; and
- Installing a separated pedestrian and bike path along the Waiale Road and Waiale Bypass to link Wailuku, Maui Lani, and Waikapu.

The Plan is being used by the County's Department of Public Works for its pedestrian and bicycle planning. Under existing conditions, the WCT site comprises of mostly vacant parcels and so there are no bicycle facilities. However, in the vicinity of the project site and in the greater study area, there are limited existing bicycle facilities. Honoapiilani Highway is a signed shared road facility that provides access between Waiale Road and Fleming Beach Park. In the study area, striped bicycle lanes have been identified along some north and south segments of Honoapiilani Highway. Waiale Road provides a bicycle facility that provides a ½-mile designated bicycle lane from the start of Waiale Road to the Maui Correctional Center. Maui Lani Parkway provides a ½-mile bicycle lane from Kamehameha Avenue and Kuihelani Highway.

EXISTING PEDESTRIAN FACILITIES

Pedestrian facilities consist of sidewalks, crosswalks, and pedestrian signals at signalized intersections. Pedestrian facilities do not currently exist within the WCT site and existing pedestrian facilities are limited in the major roadways that serve the project study area. For example, sidewalks are not provided on either side of Honoapiilani Highway, Kuihelani Highway, Waiko Road, and Waiale Road, while sidewalks are provided only on one side of Kuikahi Drive and most portions of Maui Lani Parkway.

Pedestrian facilities at the existing study intersections are described below. Five of the eight existing study intersections are marked with high visibility crosswalks on at least two of the legs.

- Intersection 1: Honoapiilani Highway (Highway 30) & Kuikahi Drive
 - o Signalized with marked crosswalks and pedestrian signals on all four legs
- Intersection 2: Waiale Road & Kuikahi Drive
 - Signalized with marked crosswalks and pedestrian signals on all four legs
- Intersection 3: S. Kamehameha Avenue/Maui Lani Parkway
 - o All-way stop-controlled with marked crosswalks on three legs
- Intersection 4: Kuihelani Parkway (Highway 380) & Maui Lani Parkway
 - Signalized with no marked crosswalks and pedestrian signals at all four legs
- Intersection 5: Honoapiilani Highway (Highway 30) & Waiko Road
 - o Signalized with marked crosswalks and pedestrian signals on three legs
- Intersection 6: Waiale Road & Waiko Road
 - Side-street stop-controlled with no marked crosswalks on all legs
- Intersection 8: Kuihelani Highway (Highway 380) & Waiko Road
 - Signalized with marked crosswalks and pedestrian signals on two legs
- Intersection 14: Honoapiilani Highway (Highway 30) & Kuihelani Highway (Highway 380)
 - O Signalized with no marked crosswalks and pedestrian signals at all four legs

EXISTING INTERSECTION VOLUMES AND LANE CONFIGURATIONS

The operations of the eight existing study intersections were evaluated during weekday morning (6:00 to 9:00 AM) and evening (3:00 to 6:00 PM) peak-period conditions. Traffic counts were collected during the weekday AM and PM peak periods at the study intersections in September 2013, when local schools were in session. Existing lane configurations and signal controls were obtained through field observations.

Figure 3 presents the existing AM and PM peak-hour turning movement volumes, corresponding lane configurations and traffic control devices. Traffic count data sheets are provided in **Appendix A**.

EXISTING INTERSECTION LEVELS OF SERVICE

Existing peak-hour volumes and lane configurations were used to calculate levels of service for each of the study intersections. The results of the existing LOS analysis are presented in **Table 3** and the corresponding LOS calculation sheets are included in **Appendix B**.

TABLE 3 – EXISTING INTERSECTION LEVEL OF SERVICE

| | Intersection | Traffic | Peak | Delay | LOS ^{2,3} |
|-----|--|----------------------|-------|------------------------|--------------------|
| | intersection | Control | Hour | (sec/veh) ¹ | LO3 /- |
| 1. | Honoapiilani Highway (Highway 30) / Kuikahi Drive | Signalized | AM | 25.2 | С |
| | | 9 | PM | 23.3 | С |
| 2. | Waiale Road / Kuikahi Drive | Signalized | AM | 26.4 | C |
| | Trailaic Read / Railain 2.11.6 | 0.9.10.1200 | PM | 24.7 | С |
| 3. | S. Kamehameha Avenue / Maui Lani Parkway | AWSC | AM | 48.3 | E |
| ٥. | 5. Ramenamena / Wenae / Waar Lam ranknay | 7.11.50 | PM | 54.4 | F |
| 4. | Kuihelani Highway / Mauilani Parkway | Signalized | AM | 21.4 | С |
| ₹. | Kullielalli i ligilway / Waulialli i arkway | Signanzed | PM | 21.9 | C |
| 5. | Honoapiilani Highway (Highway 30) / Waiko Road | Signalized | AM | 13.3 | В |
| Э. | Horioapiliani Highway (Highway 50) / Walko Koau | Signalized | PM | 11.9 | В |
| _ | Maiala Dand (Mailea Dand | CCCC | AM | 12.4 | В |
| 6. | Waiale Road / Waiko Road | SSSC | PM | 10.9 | В |
| _ | C. Kanada anda A. ana (NA/all a BandA | N1 / A | AM | D | |
| 7. | S. Kamehameha Avenue / Waiko Road ⁴ | N/A | PM | Does no | t exist |
| 0 | W 11 1 1 1 1 200 1 1 D 1 | C: I: I | AM | 14.5 | В |
| 8. | Kuihelani Highway (Highway 380) / Waiko Road | Signalized | PM | 11.2 | В |
| | | N1/A | AM | 5 | |
| 9. | Honoapiilani Highway (Highway 30) / Main Street ⁴ | N/A | PM | Does no | t exist |
| 10 | W L. D L. (14.) . G (4 | N 1/ A | AM | | |
| 10. | Waiale Road / Main Street ⁴ | N/A | PM | Does no | t exist |
| | | | AM | _ | |
| 11. | Honoapiilani Highway / East-West Residential Street ⁴ | N/A | PM | Does no | t exist |
| | | | AM | | |
| 12. | North-South Residential Street / Waiale Road ⁴ | SSSC | PM | Does no | t exist |
| | | | AM | | |
| 13. | Honoapiilani Highway (Highway 30) / Waiale Road ⁴ | N/A | PM | Does no | t exist |
| 14 | Honoapiilani Highway (Highway 30) / Kuihelani Highway | | AM | 15.2 | В |
| 17. | (Highway 380) | Signalized | PM | 12.4 | В |
| | (ga) 555/ | | 1 171 | 16, 1 | |

Source: Fehr & Peers, 2014.

Notes:

AWSC = All-way stop-controlled intersection

SSSC = Side-street stop-controlled intersection

^{**} Indicated oversaturated conditions. Delay cannot be calculated

¹ Whole intersection weighted average stopped delay expressed in seconds per vehicle for signalized and all-way stop-controlled intersections. The vehicular delay for the worst movement is reported for side street stop-controlled intersections.

²LOS calculations performed using the *2000 Highway Capacity Manual (HCM)* method.

³ Undesirable LOS highlighted in **bold.**

⁴ Future intersection

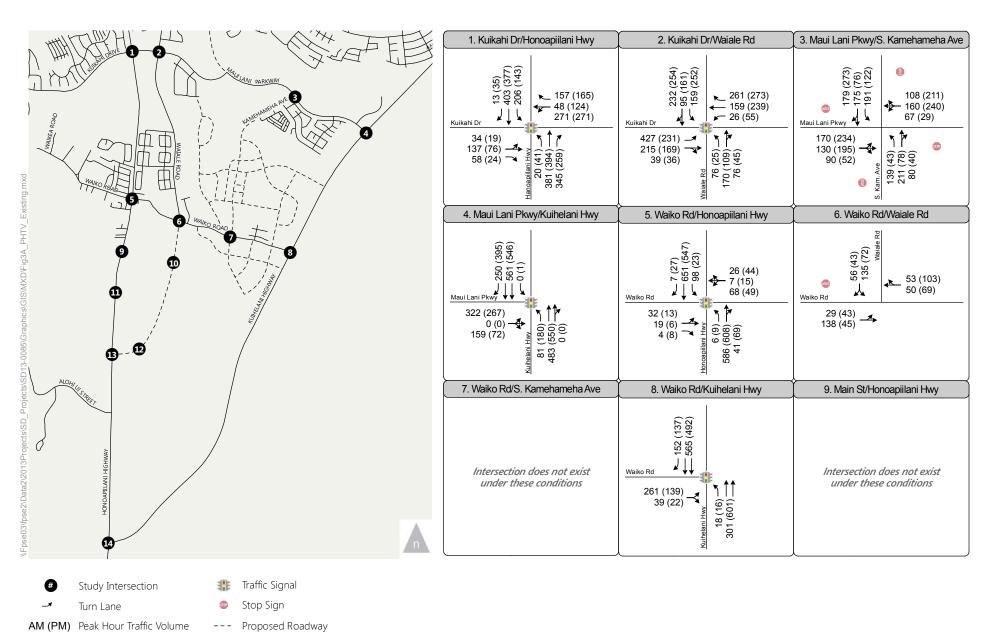
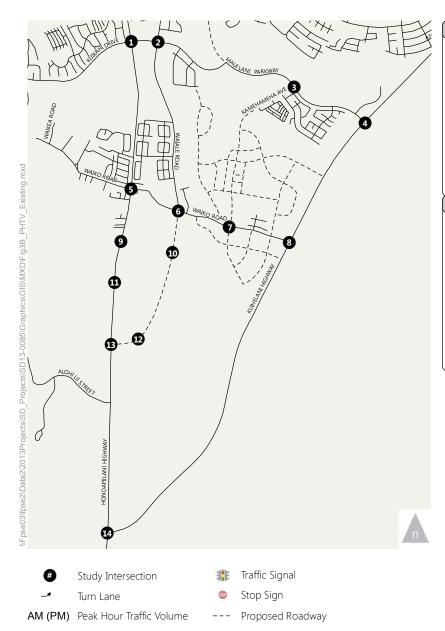




Figure 3A

Peak Hour Traffic Volumes and Lane Configurations -Existing (2013) Conditions



| 10. Main St/Waiale Rd | 11. E-W Residential St/Honoapiilani Hwy | 12. Waiale Rd/N-S Residential St | |
|---|--|---|--|
| Intersection does not exist under these conditions | Intersection does not exist under these conditions | Intersection does not exist under these conditions | |
| 13. Waiale Rd/Honoapiilani Hwy | 14. Kuihelani Hwy/Honoapiilani Hwy | | |
| Intersection does not exist under these conditions | Column C | | |



Figure 3B

Peak Hour Traffic Volumes and Lane Configurations -Existing (2013) Conditions The results of the LOS calculations indicate that all of the existing study intersections operate at an overall acceptable service level (LOS D or better), with the exception of the following location:

- <u>Intersection 3: S. Kamehameha Avenue & Maui Lani Parkway</u> (LOS E AM peak hour and LOS F PM peak hour)
 - The all-way stop-control and high eastbound and westbound volumes traversing through a shared left/through/right configuration contribute to the relatively high eastbound and westbound approach delays and overall poor operating peak levels of service at this intersection.

4. FUTURE TRAFFIC PROJECTIONS

To evaluate the potential impact of traffic generated by the proposed project on the surrounding street system, it was necessary to develop estimates of future traffic conditions in the area both with and without the project. Future traffic conditions without the proposed project reflect traffic increases due to general regional growth and development, as well as traffic increases generated by other specific developments near the project site. These conditions are referred to as the cumulative base condition (i.e., no project conditions). The sum of the cumulative base and project-generated traffic represents the cumulative plus project conditions. Development of these future traffic scenarios is described in this chapter.

CUMULATIVE BASE TRAFFIC PROJECTIONS

The cumulative base traffic projections include two elements: 1) model forecasts of future traffic volumes that take into account the expected changes in traffic over the existing traffic volumes caused by traffic generated by specific cumulative projects located in the study area and overall regional growth; and 2) by roadway network changes and street system improvements.

Although the anticipated completion year of the first phase of the WCT development is 2021, the analysis used 2022 for the horizon year for Phase 1 to be consistent with the planned completion of large background projects in the area, such as the Waiale development and the Waiale Bypass, providing a more conservative cumulative forecast against which to assess potential project impacts.

AREAWIDE TRAFFIC GROWTH AND CUMULATIVE DEVELOPMENT PROJECTS

Information was obtained from the County of Maui on approved, planned, and proposed development projects throughout Central Maui. This information was used to estimate future traffic volumes for the study area, since the growth and changes in traffic caused by anticipated projects in the Kahului, Wailuku and Waikapu areas could affect conditions on the streets around WCT. **Table 4** is a compiled list of future cumulative projects in the Central Maui vicinity. **Appendix C** provides a more detailed list with available project descriptions for residential projects that the County is monitoring, as well as maps of other residential and non-residential development projects in Central Maui that have come to the attention of the Department of Planning.

TABLE 4 - CENTRAL MAUI FUTURE CUMULATIVE PROJECT LIST 1,2

| Project Name | | | | |
|--------------|-----------------------------------|---|---|--|
| • | `Aina o Kane Condos | • | Kehalani (C-9) | |
| • | Alternative Care Services, Inc. | • | Kehalani Commercial Center | |
| • | Central Maui Regional Park | • | Maui Beach Hotel Addition | |
| • | Central Maui Senior Housing | • | Maui Lani Church | |
| • | Civil Defense Center | • | Maui Lani Homes 1 | |
| • | Consolidated Baseyards | • | Maui Lani Lot 4 | |
| • | Habitat For Humanity Condos | • | Maui Lani Lot 7B | |
| • | Hale Ho`omalu Mental Health Kokua | • | Maui Lani MF7 Condos | |
| • | Hale Mua | • | Maui Lani Parkway Commercial | |
| • | Hale Kapili Project | • | Maui Lani The Parkways | |
| • | Ka Lima O Maui Affordable Housing | • | Maui Lani Village | |
| • | Kahawai Condos | • | MEO B.E.S.T. House | |
| • | Kahului Harbor Improvements | • | Mission Street Affordable Apts. | |
| • | Kahului Town Center Redevelopment | • | Na Leo Pulama O Maui Hawaiian School Hale Hou | |
| • | Kehalani (C-12) | • | Pi`ihana Project District 2 | |
| • | Kehalani (C-13) | • | Pu`unani Residences | |
| • | Kehalani (C-14) | • | Valley Isle Fellowship Condos | |
| • | Kehalani (C-18) | • | Wai`ale | |
| • | Kehalani (C-19) | • | Wai'ale Affordable Homes | |
| • | Kehalani (C-3) | • | Waiehu Mauka Affordable Townhomes | |
| • | Kehalani (C-6) | • | Waikapu Gardens II | |
| • | Kehalani (C-7) | • | Waikapu Light Industrial Park | |
| • | Kehalani (C-8) | • | Waikapu Rural Village | |

Notes:

¹The list above of development projects in Central Maui were pulled from multiple sources, including: conversations with County staff, a residential project list for Central Maui provided by the County of Maui in December 2013, available and relevant environmental assessments or impact studies available on the State's website for Maui, and the 2011 Central Maui Development Project maps and Development Project GIS layer available on the County website.

²During the related project review process, the socioeconomic and land use data in the interim year and long-term year No Build models was consistent with the future cumulative projects listed above.

By 2022 and by 2026, the WCT study area will have experienced significant residential growth and development of new commercial, industrial, business, and institutional land uses, primarily because of the following projects:

- <u>Waiale</u>, located along Waiko Road, south of the Maui Lani development, east of Waiale Road, and directly west of Kuihelani Highway, is assumed to be completed by 2022. The planned mixed-use community will include 2,550 single-family and multi-family dwellings, commercial and light industrial land uses, as well as a middle school.
- <u>Maui Lani Development</u> is partially complete and assumed to be fully completed by 2026. This
 master planned community along Mauilani Parkway between Waiale Road and Kuihelani
 Highway, comprises of a mixture of residential subdivisions that total approximately 1,000 singlefamily and multi-family households and commercial uses. Specifically, the development includes
 the Maui Lani Village Center, which will be about 540,000 square feet or 79 lots available for
 commercial, business, or medical office uses.
- <u>Kehalani Development</u> is partially complete and assumed to be fully completed by 2026. This master planned community of 2,400 homes is located north of Kuikahi Drive, south of Iao Valley Road, east of the West Maui Mountains, and primarily west of Honoapiilani Highway.²
- <u>Puunani Residences</u> is located on the southwest quadrant of the intersection of Honoapiilani Highway & Kuikahi Drive. It is assumed that 20% and 40% of the project would be completed by both 2022 and 2026, respectively. Kuikahi Drive and Honoapiilani Highway are planned to provide access to the 600-home neighborhood.

Traffic generated by the above related projects and other developments were projected using the Maui Travel Demand Forecasting Model (TDFM)³ and the trip generation methodology. The TDFM assigns land use and socioeconomic data provided by the County of Maui in 2007 to Traffic Analysis Zones (TAZs). These attributes were further used to generate and assign traffic across the roadway network for the base and horizon years, respectively.

¹ The TIAR for the Waiale development analyzed the project with Base Year 2022 conditions (Austin, Tsutsumi, and Associates, Inc., 2011).

² Source: http://www.kehalani.org/

³ The base 2007 model, the interim horizon 2020 No Build model, and the long-term horizon 2035 No Build model were obtained from HDOT. The socioeconomic and land use data supplied by Maui County in 2007 was used to calibrate the TDFM.

BASELINE STREET SYSTEM IMPROVEMENTS

Discussions were held with County and State agency staff regarding the roadway improvements in or near the study area planned for completion by 2022. These improvements, whether the result of local capital improvement programs or in connection with planned or approved projects, would result in dramatically improved mobility options for residents and visitors as well as capacity changes at various locations throughout the study area as discussed below.

Based on the information received from agency staff, the review of planning documents related to the nearby projects, and the review of the roadway network changes between the base and horizon year models, the proposed transportation system changes that are projected to occur between 2007 and 2022 are included in the cumulative base traffic network of each horizon year No Build model.⁴ The improvements are listed in detail below. The study area for transportation analysis purposes is generally bounded by Kuikahi Drive/Maui Lani Parkway to the north, Honoapi`ilani Highway to the west, Kuihelani Highway to the east, and the intersection of Honoapi`ilani Highway and Kuihelani Highway to the south. The street system improvements denoted with an asterisk (*) are outside of the WCT study area:

- Hana Highway Widening * The 2020 and 2035 roadway networks of the TDFM includes the widening of Hana Highway from a four-lane to a six-lane divided highway from Kaahumanu Avenue to the vicinity of the also proposed Kahului Airport Access Road.
- Honoapiilani Highway Widening * The 2020 and 2035 roadway networks of the TDFM includes
 the widening of Honoapiilani Highway between Lahainaluna Road and Aholo Road in West Maui
 from being a two-lane roadway to a four-lane roadway.
- <u>Kahului Airport Access Road * This four-lane bypass will be constructed from Puunene Avenue</u>
 to Hana Highway. The purpose of this road is to provide an alternative route to congested
 existing routes (i.e., Dairy Road) to Kahului Airport. This roadway improvement project is assumed
 in the 2020 and 2035 roadway networks of the TDFM.
- <u>Kamehameha Avenue Extension</u> To support the Waiale development and related traffic, it is assumed that Kamehameha Avenue will extend southward from its existing terminus near its intersection with Maui Lani Parkway to intersect Waiko Road and eventually to intersect with the Waiale project site Road B.

-

⁴ Per HDOT, No Build scenarios are considered baseline conditions, which includes socioeconomic forecasts but without implementing projects, such as major roadway improvements and some private developments. At the time the model files were obtained, HDOT was currently working on the build scenario that modeled future projects. Because some of the roadway improvements listed in the TIAR were absent from both the 2020 No Build model and 2035 No Build model roadway networks, the roadway network for each model horizon year was updated to ensure these future facility improvements are appropriately modeled.

- <u>Intersection 7: Kamehameha Avenue & Waiko Road</u> This future side street stop-controlled, four-legged intersection will consist of one left-turn lane and one shared through/right-turn lane on all approaches. This intersection is assumed to be constructed under cumulative base conditions, as it would provide access to portions of the Waiale mixed-use community.
- <u>Lahaina Bypass</u> * This two-lane highway will be located in West Maui and will extend between Launiupoko south of Lahaina and Honokowai to the north. This roadway improvement project was added to the 2020 and 2035 roadway networks of the TDFM.
- Maui Lani Parkway Extension To support the Maui Lani developments and related traffic, it is
 assumed that Maui Lani Parkway will extend and connect Waiinu Street and Kuikahi Drive. It is
 assumed that the extension will provide one lane in each direction.
- <u>Puunene Avenue Widening *</u> The 2020 and 2035 roadway networks of the TDFM includes the widening of Puunene Avenue from two to four lanes from Wakea Avenue to Kuihelani Highway.
- Roadway Detailing for Waiale To support the Waiale project and related traffic, the construction
 of the following roadways are assumed within the Waiale project site: Road A, Kamehameha
 Avenue extension, Road C, and Road B. These roadways are assumed to be constructed under
 cumulative base conditions, as it would provide access to various areas of the Waiale mixed-use
 community.
- <u>Waiale Bypass</u> Waiale Road would extend from its existing terminus at Waiko Road to intersect
 Honoapiilani Highway approximately one mile south of Honoapiilani Highway/ Waiko Road. It is
 assumed that the bypass would be constructed as a two-way, two-lane roadway and left-turn
 pockets will be provided at key intersections, including the two future study intersections
 (discussed below).
- Intersection 6: Waiale Road & Waiko Road This intersection will become a four-legged intersection under cumulative base conditions and the fourth (south) leg will be constructed as part of the Waiale Bypass. It is assumed that the reconfigured intersection will consist of one left-turn lane and one shared through/right-turn lane at the eastbound and southbound approaches, while the northbound and westbound approaches are assumed to consist of one left-turn lane, one through lane, and one right-turn lane. This existing, unsignalized intersection is assumed to become signalized as part of the construction of the Waiale Bypass.
- <u>Intersection 13: Honoapi`ilani Highway & Waiale Road</u> This future intersection will consist of a northbound approach that provides one through lane and one free right-turn lane, a southbound approach that provide one through lane and one left-turn lane, and a westbound approach with

one left-turn lane and one right-turn lane. This intersection is assumed to be signalized and constructed as part of the Waiale Bypass project under cumulative base conditions.

Cumulative Base Traffic Projection Methodology

Related projects were checked against the model growth between the base year (2007) and each of the horizon years (2020 and 2035) to see if the land use and socioeconomic attributes included the known related projects, such as those listed in **Table 4**. Since the horizon year models obtained from HDOT were No Build scenarios,⁵ some of the major projects planned in the vicinity of the WCT study area were noticeably absent in the TDFM's projections; therefore, in order to appropriately model these future projects, the respective land use and socioeconomic attributes were adjusted for the corresponding horizon year the related projects are anticipated to be completed by. The changes in land use and socioeconomic assumptions between the updated 2020 and 2035 model were then used to interpolate the land use and socioeconomic data for the scaled 2022 and 2026 models, which were used to forecast cumulative base traffic volumes for 2022 and 2026, respectively.

After the land use and socioeconomic data adjustments were completed, trips generated by the related projects were estimated and assigned by the model to the future roadway system based on their locations and anticipated distribution patterns. The geographic distribution of traffic generated by new development depends on several factors, such as the type and density of the proposed land uses, the geographic distribution of the population from which employees and/or patrons may be drawn, the geographic distribution of activity centers (employment, commercial, and other) to which residents of proposed residential projects may be drawn, and the location of those developments in relation to the surrounding future street system.

Between 2013⁶ and 2026, the TDFM anticipates an aggregate, island-wide growth of approximately 17,000 households and about 24,000 employees for Maui. Additionally, after land use and socioeconomic data adjustments were completed for the 2026 model, the TDFM projected an approximate 20% increase in demand over existing conditions along Honoapiilani Highwy between Kuikahi Drive and Kuihelani Highway. The TDFM also projected an approximate 30% increase in demand along Kuihelani Highway over existing conditions between Maui Lani Parkway and Honoapiilani Highway. 7

⁵ Ibid.

⁶ The Base Year (2007) for the TDFM was adjusted to include known socioeconomic changes up to 2013 (See Appendix C for specific projects). Therefore, the updated Base Year TDFM used in this analysis reflects land use and employment updates between 2007 and 2013.

⁷ The overall percentage increase in traffic demand was based on averaging the calculated percentage increase in each of the PM peak hour roadway segment volumes between the updated base year and 2026 horizon year models.

CUMULATIVE BASE TRAFFIC VOLUMES

The resulting cumulative base traffic volumes and the anticipated lane configurations, representing future conditions without the project for year 2022 and 2026, are presented in **Figure 4** and **Figure 5**, respectively. These future projections take into account the estimated overall growth in the surrounding area without the addition of traffic generated by the proposed Waikapu Country Town Project. To analyze level of service, post-processed model volumes for the 2022 cumulative base and the 2026 cumulative base were loaded into Synchro 8.0.

PROJECT TRAFFIC PROJECTIONS

Development of future traffic projections related to the amount of traffic added to the roadway system by WCT is estimated using a three-step process: (1) project trip generation, (2) trip distribution, and (3) trip assignment. The first step estimates the amount of project-generated traffic will be added to the roadway network. The second step estimates the direction of travel to and from the project site. The new trips are assigned to specific street segments and intersection turning movements during the third step. This process is described in more detail in the following sections.

PROJECT STREET SYSTEM IMPROVEMENTS

Based on feedback from agency staff and review of the proposed street network, the proposed transportation system changes described previously are anticipated to occur between 2013 and 2022/2026 and are therefore included in the cumulative base traffic network. Additional improvements will be made as part of the proposed project and are listed below:

• <u>Intersection 9: Honoapiilani Highway & Main Street</u> – This future intersection will be constructed as part of the Year 2022 Conditions (Phase 1) of the proposed project. The intersection is assumed to be configured with northbound and southbound approaches that provide one left-turn lane, one through lane, and one right-turn lane and eastbound and westbound approaches that provide one left-turn lane and one shared through/right-turn lane.

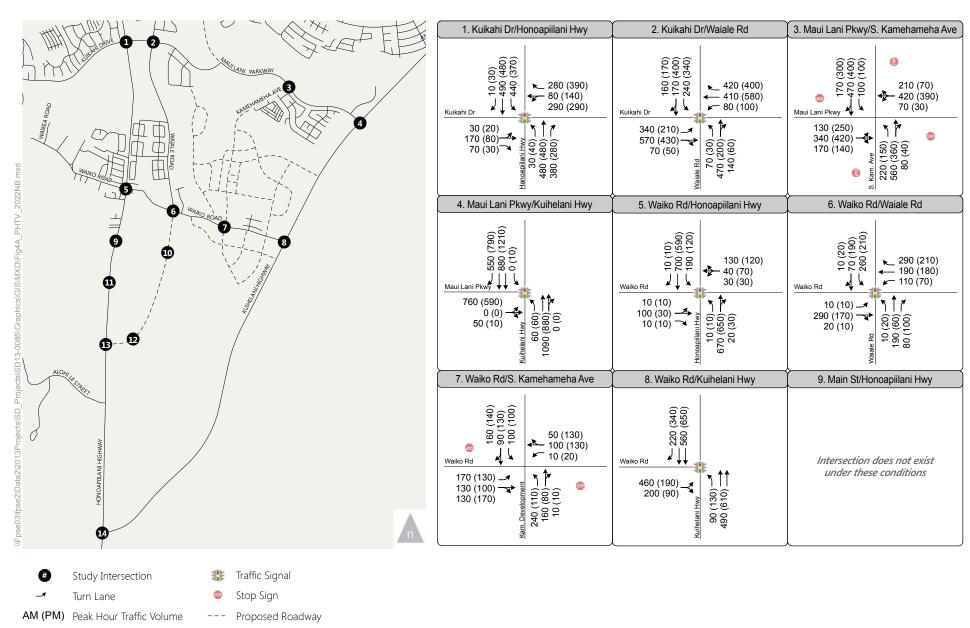
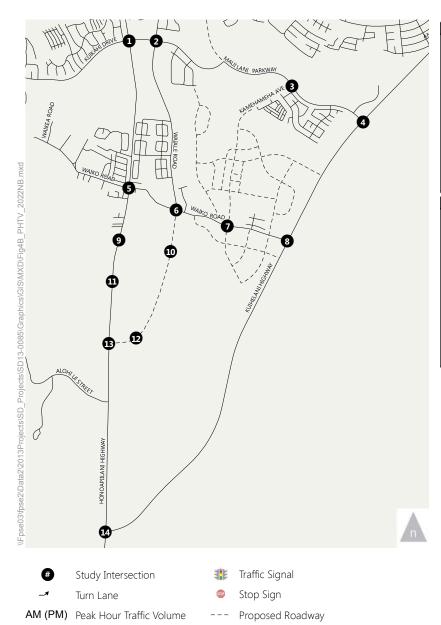




Figure 4A

Peak Hour Traffic Volumes and Lane Configurations -Year 2022 No Project Conditions



| 10. Main St/Waiale Rd | 11. E-W Residential St/Honoapiilani Hwy | 12. Waiale Rd/N-S Residential St |
|---|--|---|
| Intersection does not exist under these conditions | Intersection does not exist under these conditions | Intersection does not exist under these conditions |
| 13. Waiale Rd/Honoapiilani Hwy | 14. Kuihelani Hwy/Honoapiilani Hwy | |
| Honoapillani Hwy 740 (900) 280 (100) 280 (100) Maine Bd 740 (200) 740 (200) 740 (200) 740 (200) | Multiplication of the property | |



Figure 4B

Peak Hour Traffic Volumes and Lane Configurations -Year 2022 No Project Conditions

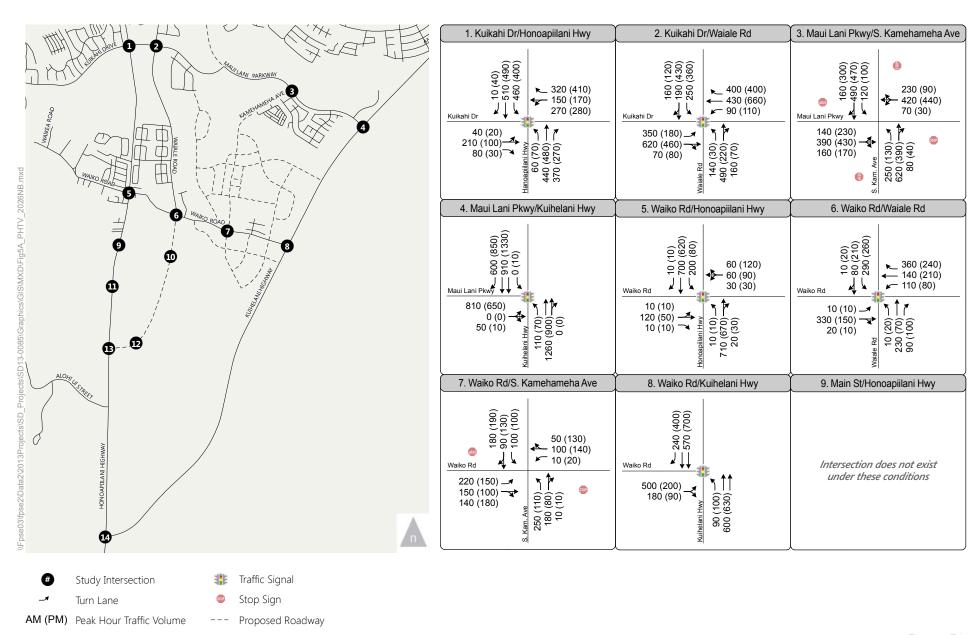
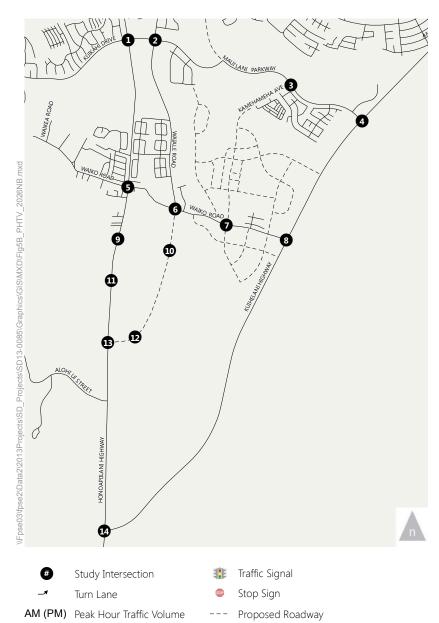




Figure 5A

Peak Hour Traffic Volumes and Lane Configurations -Year 2026 No Project Conditions



| 10. Main St/Waiale Rd | 11. E-W Residential St/Honoapiilani Hwy | 12. Waiale Rd/N-S Residential St |
|--|---|---|
| Intersection does not exist under these conditions | Intersection does not exist under these conditions | Intersection does not exist under these conditions |
| 13. Waiale Rd/Honoapiilani Hwy | 14. Kuihelani Hwy/Honoapiilani Hwy | |
| Honospillani Hwy 790 (930) 340 (110) Maiale Bd Maiale Bd Maiale Bd Maiale Bd | Minimal Heave 10 (10) 10 (10) | |



Figure 5B

Peak Hour Traffic Volumes and Lane Configurations -Year 2026 No Project Conditions Additionally, the intersection is proposed to be signalized.8 If the intersection was side-street stop-controlled under future conditions, the side-street approaches would operate at undesirable LOS and drivers at the side streets would experience significantly long delays due to the heavy projected through volumes along the Honoapiilani Highway.

- Intersection 10: Waiale Road & Main Street This future intersection will be constructed as part of the Year 2022 Project Conditions (Phase 1). It is assumed to be configured as a four-legged, single-lane roundabout, where vehicles must yield for a gap in the circulating flow before entering the circle. The east leg of the intersection is assumed to provide access to consolidated County and public facilities, light industrial uses, a regional park, fire station, and emergency management center.9
- Intersection 11: Honoapiilani Highway & East-West Residential Street This future intersection will be constructed as part of the proposed project. The intersection is assumed to be configured as a four-legged intersection with northbound and southbound approaches that provide one leftturn lane, one through lane, and one right-turn lane and eastbound and westbound approaches that provide one left-turn lane and one shared through/right-turn lane.

Additionally, it should be noted that the intersection is proposed to be signalized under full buildout conditions of the project.8 If the intersection was side-street stop-controlled under future conditions, the side-street approaches would operate at undesirable LOS and drivers at the side streets would experience significantly long delays due to the heavy projected through volumes along the Honoapiilani Highway.

Intersection 12: Waiale Road & North-South Residential Street - This future intersection will be constructed as part of the Year 2026 with Project Conditions (Phase 2). It is assumed to be configured as a three-legged, side-street stop-controlled intersection with an eastbound approach that provides a shared through/left-turn lane, a westbound approach that provides a

⁸ Prior to the installation of a traffic signal, it is recommended that a full warrant analysis be conducted based on field-measured traffic data and a thorough study of traffic and roadway conditions by an experienced engineer. Furthermore, the decision to install a signal should not be based solely on the warrants because the installation of signals can lead to certain types of collisions. The responsible state or local agency should undertake regular monitoring of actual traffic conditions and collision data and conduct a timely re-evaluation of the full set of warrants to prioritize and program intersections for signalization.

⁹ Based on consultations with the County, approximately 100 acres will be dedicated to consolidated facilities for water, parks, environmental management, and public works departments. The primary access to these uses is planned to be via Kuihelani Highway, however, some vehicles and maintenance trucks will likely access these uses via the Waiale Bypass. This analysis assumes that such mauka access will be via the east leg of Intersection 10: Waiale Road & Main Street. Additionally, the fire station, emergency management center, and regional park access will be through the east leg of Waiale Road & Main Street. Based on the best available data, traffic projections for theses uses have been estimated and applied to the intersection analysis.

shared through/right-turn lane, and a stop-controlled southbound approach that provides a shared left-turn/right-turn lane.

• Intersection 13: Honoapiilani Highway & Waiale Road – This signalized intersection will be a three-legged intersection under cumulative base conditions. The fourth (west) leg will be constructed as part of the Year 2026 Conditions (Phase 2) of the proposed project, resulting in a northbound approach that provides one left-turn lane, one through lane, and one free right-turn lane, a southbound approach that provides one left-turn lane, one through lane, and one right-turn lane, and eastbound and westbound approaches that provide one left-turn lane and one shared through/right-turn lane.

PROJECT TRIP GENERATION ESTIMATES

Vehicle trip rates presented in *Trip Generation 9th Edition* (Institute of Transportation Engineers, 2012) were used to estimate number of trips to and from the proposed project. The trip generation rates used in this study and the estimated new numbers of trips generated by the proposed project in 2026 are summarized in **Table 5**.

Project trip generation estimates are commonly developed using Institute of Transportation Engineers (ITE) rates. However, ITE rates are typically obtained from isolated, suburban developments generally not sensitive to the trip-making characteristics of mixed-use developments such as WCT. In fact, few methodologies are available to estimate the unique trip generation characteristics of mixed-use and infill developments. One of the most commonly used methods is to use trip generation rates or equations from *Trip Generation* and apply reductions from the mixed-use internalization spreadsheet from *Trip Generation Handbook*, 2nd Edition (ITE, 2004). This method has some shortcomings in that it is based on a limited sample of six mixed-use sites in Florida, it is limited to three land use types (residential, retail, and office), and it does not take into account the influence of nearby land uses.

More comprehensive analyses of mixed-use and infill trip generation were developed and presented in the following research studies: *Traffic Generated by Mixed-Use Developments – A Six-Region Study Using Consistent Built Environmental Measures* (Reid Ewing et al., September 2008) and *National Cooperative Highway Research Program Report 684: Enhancing Internal Trip Capture Estimation for Mixed-Use Developments* (Bochner et al., March 2011). The two studies examined over 260 mixed-use development sites throughout the U.S. and, using different approaches, developed new quantification methods. Fehr & Peers has reviewed the two methods, including the basis, capabilities, and appropriate uses of each, to produce a new method (MXD+) that combines the strengths of the two individual advances to best practice. MXD+ recognizes that traffic generation by mixed-use and other forms of sustainable development relate closely to the density, diversity, design, destination accessibility, transit proximity, and scale of development. MXD+ improves the accuracy of impact estimation and trip internalization and

gives planners a tool to rationally balance land use mix and to incorporate urban design, context compatibility, and transit orientation to create lower-impact development.

Accordingly, the MXD+ process was used to estimate more appropriate internalization and non-motorized trip reductions to apply to the ITE-based automobile trip generation for WCT. The MXD reductions for full buildout of WCT ranged from 22% to 27% during the peak hours and 15% for daily. Using the MXD+ process to inform and refine the internalization and non-motorized trip reduction estimate used for the project trip generation, it was determined that the application of a 15% daily reduction and a 25% AM and PM peak hour reduction were appropriate to account for the infill and mixed-use nature of the land use plan where vehicle trips would be linked (i.e. residential-school-retail interplay) and/or replaced with walk and bicycle trips to nearby land uses. The MXD+ model inputs and results are provided in **Appendix D**.

As shown in **Table 5**, by 2026 and completion of both Phase 1 and Phase 2 of WCT, the project full buildout is estimated to generate approximately 19,000 daily trips, including about 1,200 AM peak hour trips (409 inbound and 746 outbound) and about 1,500 PM peak hour trips (852 inbound and 633 outbound).

The MXD+ process was also used to estimate more appropriate internalization and non-motorized trip reductions to apply to the ITE-based automobile trip generation for just WCT Phase 1. The MXD reductions for partial buildout of WCT ranged from 26% to 35% during the peak hours and 17% for daily. The variation in reductions related to internal capture and non-motorized trips between the full buildout reductions are because a smaller portion of the makai and mauka side of the WCT project will be developed and less residential units will be constructed by Phase 1. Using the MXD+ process to inform and refine the internalization and non-motorized trip reduction estimate to be used for the Year 2022 project trip generation, it was determined that the application of a 15% daily reduction and a 25% AM and PM peak hour reduction would still be the appropriate, conservative approach.

With the application of the reductions to the WCT Phase 1 trip estimates, the partial buildout of the project is expected to generate approximately 13,100 daily trips, including about 700 trips during the AM peak hour (306 inbound and 427 outbound) and about 1,000 trips during the PM peak hour (552 inbound and 460 outbound). These WCT Phase 1 trip estimates were then used to conduct the traffic analysis for the Year 2022 with Partial Development Conditions. **Appendix E** provides the vehicle trip generation estimates for Phase 1 and **Appendix D** provides the corresponding MXD+ model inputs and outputs.

TABLE 5 – TRIP GENERATION RATE AND ESTIMATES

| SUMMARY OF RATES | | | | | | | | | | | |
|--|------|-----------------------|-------|-----|-----------|-------|--------------|-----|-------|--|--|
| Land Use | ITE# | Rate | Daily | AN | /I Peak H | our | PM Peak Hour | | | | |
| Land Ose | 116# | nate | Daily | In | Out | Total | In | Out | Total | | |
| Single-Family Housing | 210 | per Dwelling Unit | [a] | 25% | 75% | [a] | 63% | 37% | [a] | | |
| Apartments | 220 | per Dwelling Unit | [a] | 20% | 80% | [a] | 65% | 35% | [a] | | |
| Retail | 820 | per 1,000 square feet | [a] | 62% | 38% | [a] | 48% | 52% | [a] | | |
| Parks | 412 | per acre | 2.28 | 61% | 39% | 0.02 | 61% | 39% | 0.09 | | |
| Elementary School | 520 | per student | 1.29 | 55% | 45% | 0.45 | 49% | 51% | 0.15 | | |
| Quality Restaurant | 931 | per 1,000 square feet | 89.95 | 82% | 18% | 0.81 | 67% | 33% | 7.49 | | |
| Source: ITE Trip Generation Manual, 9th Edition, 2012. | | | | | | | | | | | |

VEHICLE TRIP ESTIMATES

| Land Use | ITE# | Quantity | Unit | Daily | AN | 1 Peak H | our | PM Peak Hour | | |
|--|-------------------|-------------|----------------------------|--------|------|----------|-------|--------------|------|-------|
| Land Ose | 116# | Quantity | Onit | Daily | In | Out | Total | In | Out | Total |
| | | Phase 1 | & 2 (2017-202 ₎ | 6) | | | | | | |
| Single-Family Housing | 210 | 1,050 | DU^1 | 9,136 | 186 | 559 | 745 | 549 | 323 | 872 |
| Apartments [b] | 220 | 529 | DU^1 | 3,329 | 53 | 210 | 263 | 201 | 108 | 309 |
| Retail [c] | 820 | 169.597 | KSF ² | 9,573 | 133 | 82 | 215 | 410 | 444 | 854 |
| Parks | 412 | 32.440 | Acres | 74 | 1 | 0 | 1 | 2 | 1 | 3 |
| Elementary School [d] | 520 | 750 | Students | 968 | 186 | 152 | 338 | 55 | 58 | 113 |
| Internal Capture or Non-motorized Trips (15% | 6 Daily; 25% AM c | and PM) [e] | | -3,462 | -140 | -251 | -391 | -304 | -234 | -538 |
| Pass-by Reduction (10% Daily and AM; 20% P | PM) [f] | | | -813 | -10 | -6 | -16 | -61 | -67 | -128 |
| Total Net New External Vehicle Trips (Phase 1 & 2) | | | | 18,805 | 409 | 746 | 1,155 | 852 | 633 | 1,485 |

Source: Fehr & Peers, 2014; Waikapu Country Town Conceptual Land Use Plan by Planning Consultants Hawaii, LLC. (October 2014)

Notes:

- [a] Fitted curve equations were used to derive AM peak hour, PM peak hour, and daily trip generation.
- [b] The country town mixed-use residential units and the multi-family residential units were all analyzed as apartments for conservative trip generation analysis purposes.
- [c] Does not include the 29,250 square feet of existing commercial uses located in the same area as the "village center," which will remain.
- [d] Elementary school student body assumed based on information provided in the latest Waikapu Country Town Land Use Plan dated March 3, 2014 and further consultation with the Planning Consultants Hawaii, LLC and Hawaii Department of Education, Facilities.
- [e] Reductions related to internal trip capture and non-motorized trips are due to residential-school-retail interplay. An estimated 15% reduction of daily trips and 25% reductions of the AM and PM peak hour trips were made to account for the mixed-use nature of the site, where vehicle trips can be linked and/or replaced with non-motorized trips. The MXD process was used to confirm and refine the initial reduction estimate. The MXD+ estimates peak hour internalization at 22% to 27%.
- [f] Based on the ITE Trip Generation Handbook, 2nd Edition, 2004, the estimated pass-by trip credit (assuming all WCT commercial space is for retail) is about 33%. However, because some space is expected to be service-oriented or small office, and to provide a more conservative analysis it is estimated that the pass-by credit is 10% and 20% of the net daily and net AM and PM peak hour retail trips, respectively.

¹ Dwelling Unit = DU

² 1,000 square feet = ksf

Figure 6 illustrates the net new 2022 Phase 1 project-generated traffic volumes for the AM and PM peak hours at each of the study intersections. **Figure 7** illustrates the net new 2026 project-generated traffic volumes with Phase 1 and Phase 2 project-generated traffic volumes for the AM and PM peak hours at each of the study intersections. The project trips shown on these figures reflect the inclusion of pass-by trips at some of the project intersections.

PROJECT TRIP DISTRIBUTION AND ASSIGNMENT

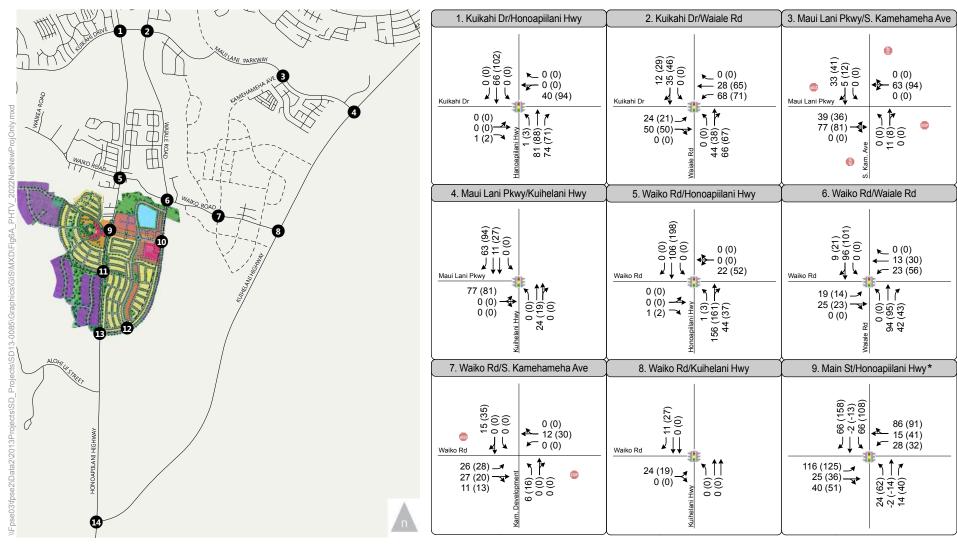
The trip distribution pattern was informed by a select zone analysis of the project site using the TDFM. Based on the model data and other refinements (i.e., adjustments based locations of complementary land uses), the following overall trip distribution pattern was estimated for the project-generated traffic:

- 2% to/from the west for employment based trips
- 25% to/from the south for household based trips and 30% to/from the south for employment based trips
- 65% to/from the north for household based trips and 58% to/from the north for employment based trips
- 100% to/from the north for school-related external trips
- 10% to/from nearby developments or mixed-use communities for both household and employment based trips

Based on the trip distribution pattern discussed above, the estimated project trips were assigned to the future roadway network that will be in place by 2022 and 2026, the horizon years in which buildout of Phases 1 and 2 of WCT are planned to be completed, respectively. As discussed, this analysis assumes that the Waiale Bypass would be in place to serve project-related and other traffic.

CUMULATIVE PLUS PROJECT TRAFFIC PROJECTIONS

The project-generated traffic volumes were added to the cumulative base traffic projections to develop the cumulative plus project traffic forecasts for 2022 and 2026. **Figure 8** illustrates the anticipated lane configurations and projected Year 2022 with Partial Development AM and PM peak hour traffic volumes at each of the study intersections. **Figure 9** illustrates the anticipated lane configurations and the Year 2026 with Project AM and PM peak hour traffic volumes at each of the study intersections. At a few locations, differences in the future roadway network with Phase 1 and with Phase 2 of the project will result in slightly different trip assignments.



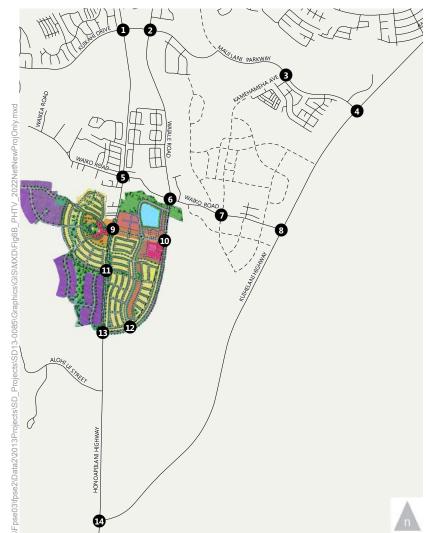


Note: Under Phase 1, only the northern portion of both the mauka and makai sides of the project site are developed. Therefore, the negative volumes reported at some movements indicate that the traffic shifts caused by pass-by trips were greater than forecasted project volumes traversing through these movements.

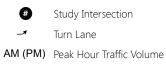
Figure 6A

Peak Hour Traffic Volumes and Lane Configurations -Net New Project Only, Phase 1 (2022)





| 10. Main St/Waiale Rd * | 11. E-W Residential St/Honoapiilani Hwy | 12. Waiale Rd/N-S Residential St |
|--|--|---|
| Meine Rd V(0) 0 (0) V(0) 0 (| Intersection does not exist under these conditions | Intersection does not exist under these conditions |
| 13. Waiale Rd/Honoapiilani Hwy | 14. Kuihelani Hwy/Honoapiilani Hwy | |
| Maiale Bd (68) A (68) A (70 (0) (0) (0) (0) (0) (0) (0) (0) (0) (0 | Mennoapullani Hwa 0 (0) 0 (0 | |



Includes Pass-by Trips

Traffic SignalStop Sign

Proposed Roadway

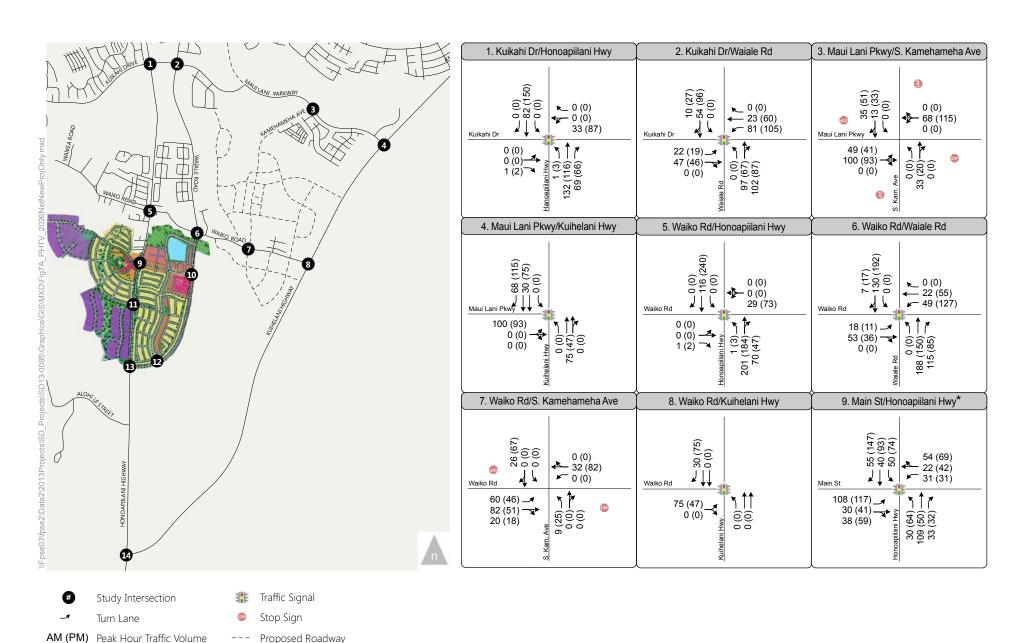
➤ Roundabout

Note: Under Phase 1, only the northern portion of both the mauka and makai sides of the project site are developed. Therefore, the negative volumes reported at some movements indicate that the traffic shifts caused by pass-by trips were greater than forecasted project volumes traversing through these movements.

Figure 6B

Peak Hour Traffic Volumes and Lane Configurations -Net New Project Only, Phase 1 (2022)







Includes Pass-by Trips

Figure 7A

Peak Hour Traffic Volumes and Lane Configurations -Net New Project Only, Phase 1 & 2 (2026)

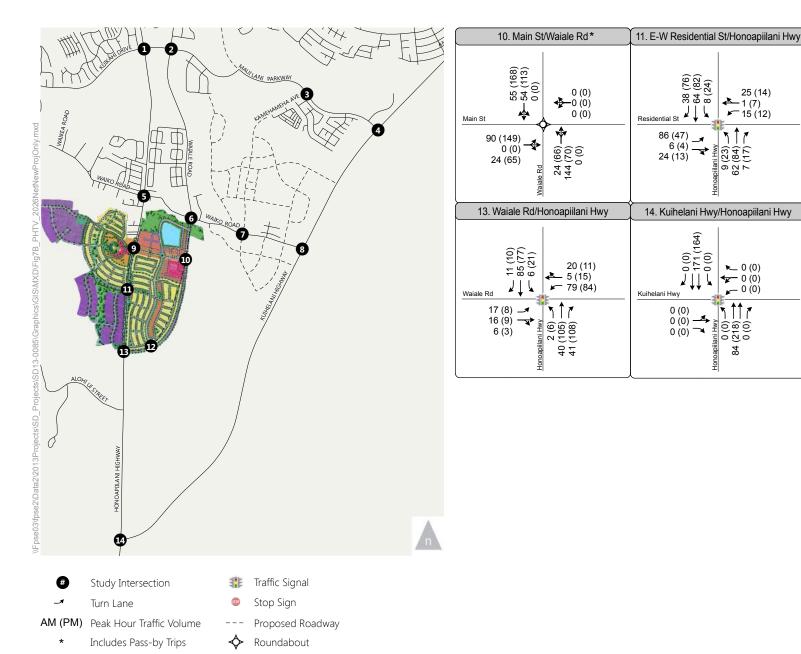




Figure 7B

12. Waiale Rd/N-S Residential St

51 (126)

28 (66)

77 (43) 133 (74)

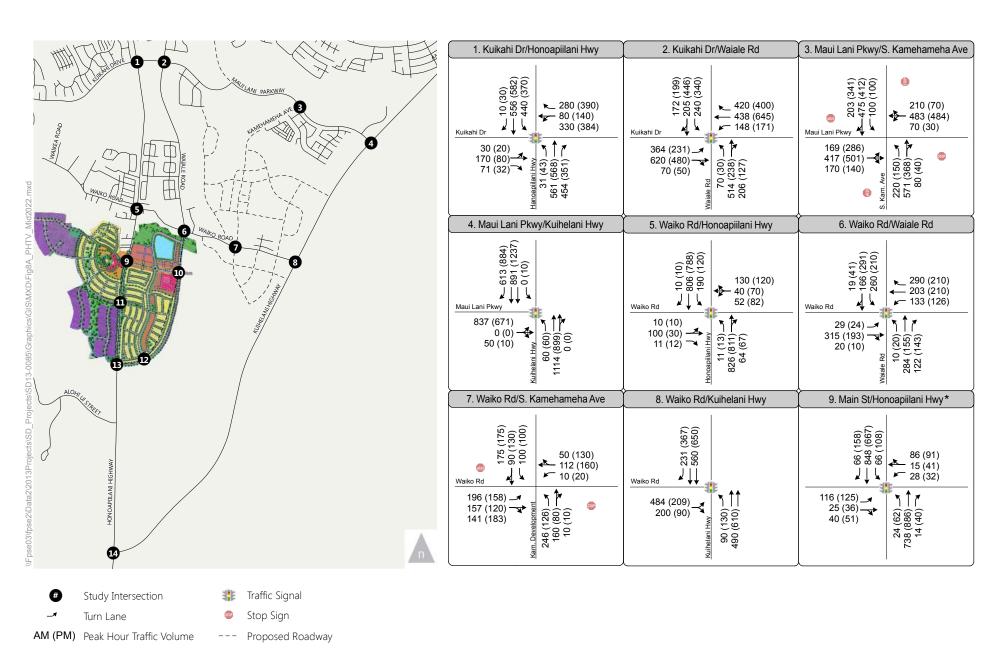
28 (74) 34 (62)

25 (14) 1 (7)

► 15 (12)

C 0 (0) 0 (0)

Peak Hour Traffic Volumes and Lane Configurations -Net New Project Only, Phase 1 & 2 (2026)



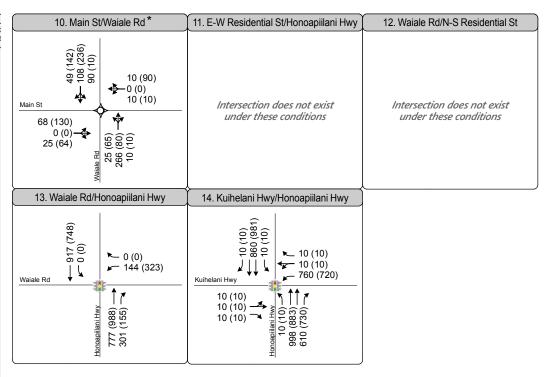


Includes Pass-by Trips

Figure 8A

Peak Hour Traffic Volumes and Lane Configurations -Year 2022 with Partial Development - Phase 1 Conditions



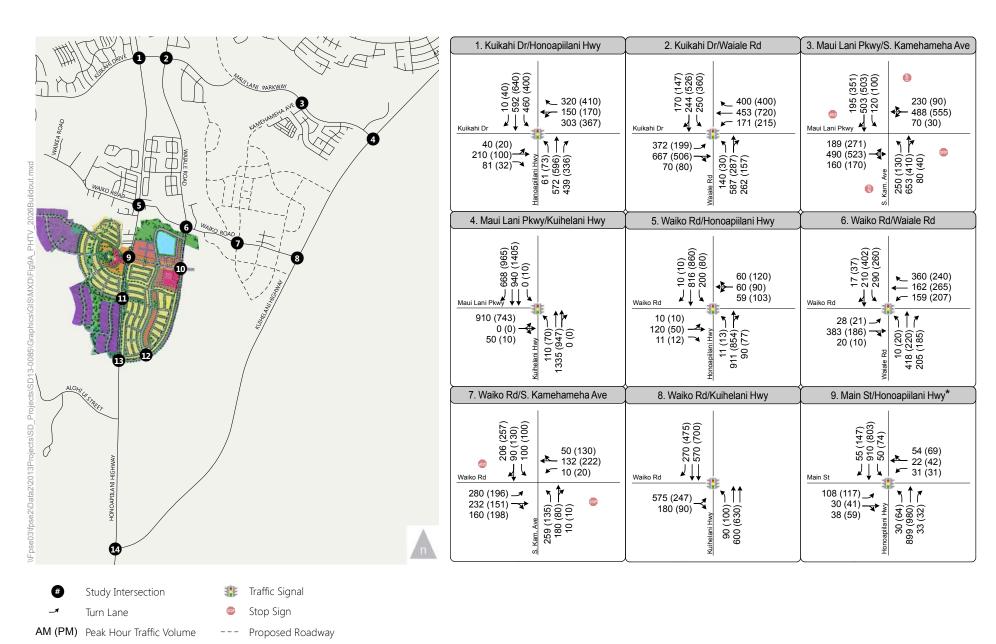






Peak Hour Traffic Volumes and Lane Configurations -Year 2022 with Partial Development - Phase 1 Conditions



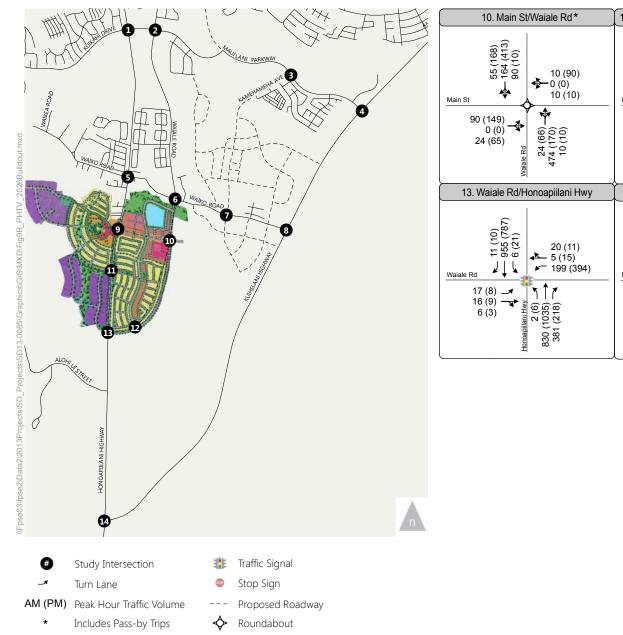




Includes Pass-by Trips

Figure 9A

Peak Hour Traffic Volumes and Lane Configurations -Year 2026 with Project Conditions - Phase 1 & 2 Conditions



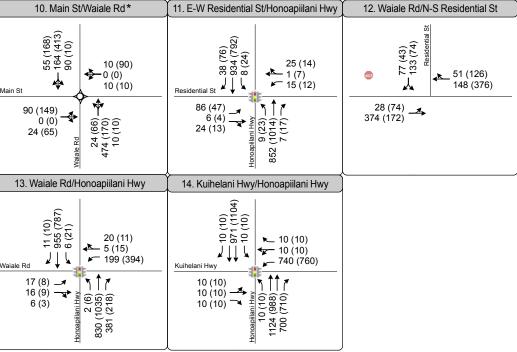


Figure 9B

Peak Hour Traffic Volumes and Lane Configurations -Year 2026 with Project Conditions - Phase 1 & 2 Conditions



5. INTERSECTION ANALYSIS

This chapter presents an analysis of the potential impacts on the roadway system due to projected increases in traffic, including traffic generated by WCT, under partial and full buildout. The analysis compares the projected levels of service at each study intersection under cumulative conditions for 2022 and 2026 both with and without the proposed project to determine potential project impacts.

YEAR 2022 NO PROJECT TRAFFIC CONDITIONS

This section presents an analysis of potential future traffic conditions projected for the Year 2022. The Year 2022 No Project or cumulative base traffic volumes projected in Chapter 3 were analyzed using the methodologies described in Chapter 1 to forecast cumulative base peak hour LOS at the study intersections. The first few columns in **Table 6** summarize the results of this analysis and the corresponding LOS calculation sheets are included in **Appendix B**.

The results of the LOS calculations indicate that all of the future study intersections operate at an overall acceptable service level (LOS D or better) in 2022, with the exception of the following locations:

- Intersection 1: Honoapiilani Highway (Highway 30) & Kuikahi Drive (LOS E AM peak hour)
- Intersection 2: Waiale Road & Kuikahi Drive (LOS E AM peak hour)
- <u>Intersection 3: S. Kamehameha Avenue & Maui Lani Parkway</u> (LOS F AM peak hour and PM peak hour)
- <u>Intersection 4: Kuihelani Highway (Highway 380) & Maui Lani Parkway</u> (LOS E AM peak hour and PM peak hour)
- <u>Intersection 7: S. Kamehameha Avenue & Waiko Road</u> (LOS F AM peak hour and PM peak hour)

The remaining five study intersections are expected to continue operating at an overall desirable LOS (LOS D or better) during both peak hours.

YEAR 2022 WITH PARTIAL DEVELOPMENT TRAFFIC CONDITIONS

The Year 2022 with Partial Development or cumulative plus project Phase 1 peak hour traffic volumes illustrated in **Figure 8**, were analyzed to determine 2022 operating conditions with the addition of project-related Phase 1 traffic. The results of the Year 2022 with Partial Development analysis is presented in **Table 6** and the corresponding LOS calculation sheets are included in **Appendix B**.

TABLE 6 – YEAR 2022 LEVELS OF SERVICE – WAIKAPU COUNTRY TOWN PARTIAL DEVELOPMENT (PHASE 1)

| | | | | Year 2022 N | o Proiect | Year 2022 with Partia | al Development | | | | Mitigated t | o: | |
|--------------|---|--------------------|--------------|-------------------|--------------------|-----------------------|----------------------|---------------------|----------------------|--|---------------------|-------------------------------|--------------------|
| Intersection | | Traffic Control | Peak Hour | Conditions | | | (Phase 1) Conditions | | Mitigation Required? | Pre-Project or Better Conditions (≤ LOS D) | | LOS D or Better Conditions | |
| | | | | Del/Veh¹ | LOS ^{2,3} | Del/Veh ¹ | LOS ^{2,3} | | | Del/Veh¹ | LOS ^{2,3} | Del/Veh¹ | LOS ^{2,3} |
| 1 | Honoapiilani Highway / Kuikahi Drive | Signal | AM | 67.3 | E | 92.5 | F | 25.2 | YES | 43.2 | D | Same as Pre | e-Project |
| Δ. | Honoapiliani Highway / Kulkani Drive | Signal | PM | 38.6 | D | 66.1 | E | 27.5 | YES | 35.2 | D | Mitigation | |
| 2. | Waiale Road / Kuikahi Drive | Signal | AM | 73.5 | E | 108.2 | F | 34.7 | YES | 61.9 | E | 39.8 | D |
| ۷. | Walale Road / Rulkarii Drive | Signal | PM | 48.6 | D | 73.6 | E | 25.0 | YES | 34.8 | С | 31.3 | C |
| 3. | S. Kamehameha Avenue / Maui Lani | AWSC | AM | > 180 | F | > 180 | F | ** | YES | 131.5 | F | 30.5 | C |
| | Parkway ⁶ | AVVJC | PM | > 180 | F | > 180 | F | ** | YES | 133.1 | F | 36.0 | D |
| 4. | Kuihelani Highway / Maui Lani Parkway | Signal | AM | 78.0 | E | 101.6 | F | 23.6 | YES | 22.7 | С | Same as Pre | e-Project |
| 4. | Kumelani ingriway / Wadi Lani Farkway | Signal | PM | 57.9 | E | 79.9 | E | 22.0 | YES | 26.4 | С | Mitigat | tion |
| 5. | Honoapiilani Highway / Waiko Road | Signal | AM | 18.6 | В | 34.5 | С | 15.9 | NO | | No Mitigation Red | quirod | |
| ٦. | Honoapillarii Fiigriway / Walko Koad | Signal | PM | 17.5 | В | 29.8 | С | 12.3 | NO | | No wingation net | quired | |
| 6. | Waiale Road / Waiko Road ^{4,9} | Signal | AM | 8.1 | Α | 8.8 | Α | 0.7 | NO | | No Mitigation Rec | aguirad | |
| 0. | Waldle Road / Walko Road / | Signal | PM | 7.3 | Α | 7.5 | Α | 0.2 | NO | | · · | | |
| 7 | S. Kamehameha Avenue / Waiko Road ^{6,7} | SSSC | AM | > 180 | F | > 180 | F | ** | YES | 8.1 | Α | Same as Pre | e-Project |
| 7. | 5. Ramenamena Avenue / Walko Road | 3330 | PM | 169.9 | F | > 180 | F | ** | YES | 7.4 | Α | Mitigat | tion |
| 0 | Kuihelani Highway / Waiko Road | Cianal | AM | 38.7 | D | 43.2 | D | 4.5 | NO | | No Mitigation Box | quirad | |
| 8. | Kullielatii Highway / Walko Koau | Signal | PM | 17.9 | В | 18.6 | В | 0.7 | NO | | No Mitigation Red | quireu | |
| 0 | Honoapiilani Highway / Main Street ^{5,8} | Cianal | AM | Only built wi | th project | 9.0 | Α | 9.0 | NO | | No Mitigation Red | quirad | |
| 9. | Horioapiliani Highway / Main Street- | Signal | AM | Only built wil | in project | 10.4 | В | 10.4 | NO | | No Miligation Rec | quireu | |
| 10 | Maiala Band / Main Chungt | Danis dalaas d | AM | ئىن بائىندا يىلىن | ula | 6.6 | Α | 6.6 | NO | | Na Mitimatian Day | and and | |
| 10. | . Waiale Road / Main Street ⁵ | Roundabout | PM | Only built wi | in project | 7.1 | Α | 7.1 | NO | | No Mitigation Red | quirea | |
| 11. | . Honoapiilani Highway / East-West | NI/A | AM | | | | 0 | مممولات بالدارية | 2 - f | | | | |
| | Residential Street | N/A | PM | | | | On | ly built with Phase | 2 of project | | | | |
| 12. | North-South Residential Street / Waiale | N/A | AM | | | | On | ly built with Phase | 2 of project | | | | |
| | Road | IN/A | PM | | | | Oli | iy bullt with Fhase | 2 of project | | | | |
| 13. | . Honoapiilani Highway / Waiale Road ⁹ | Signal | AM | 5.9 | Α | 7.4 | Α | 1.5 | NO | | No Mitigation Red | quirod | |
| 13. | . Honoapiliani riighway / Walale Koaus | Signal | PM | 12.9 | В | 17.9 | В | 5.0 | NO | | ino minganon Rec | ₁ uneu | |
| 1.4 | Hanasaillasi Hiskoon / Wolkslasi U. F | Ciamal. | AM | 22.2 | С | 23.1 | С | 0.9 | NO | | NI - Mitimatia - Da | and the al | |
| 14. | . Honoapiilani Highway / Kuihelani Highway | Signal | PM | 20.3 | С | 22.2 | С | 1.9 | NO | No Mitigation Required | | quirea | |

Source: Fehr & Peers, 2014

Notes:

AWSC = All-way stop-controlled intersection

SSSC = Side-street stop-controlled intersection

^{**} Indicated oversaturated conditions. Delay cannot be calculated.

¹Whole intersection weighted average stopped delay expressed in seconds per vehicle for signalized and all-way stop-controlled intersections. The vehicular delay for the worst movement is reported for side street stop-controlled intersections.

² LOS calculations performed using the 2000 Highway Capacity Manual (HCM) method.

³ Unacceptable LOS highlighted in **bold.**

⁴ With the construction of the Waiale Bypass under future conditions, the intersection will include a fourth (south) leg and is assumed to be signalized.

⁵ Intersection provides access to the project site.

⁶ The proposed mitigation measure at this location is signalization and the delay and LOS displayed under this condition is based on the average control delay for the intersection as a whole.

⁷ Intersection is or is assumed to be controlled by stop signs on the minor approach(es).

⁸ The project intersection is assumed to be signalized in 2022.

⁹ Intersection assumed to be signalized as part of the Waiale Bypass project.

As shown in Table 6, the proposed project would contribute to cumulative impacts (LOS E or F conditions) during one or both peak hours at five study intersections:

- Intersection 1: Honoapiilani Highway (Highway 30) & Kuikahi Drive (LOS F AM peak hour)
- Intersection 2: Waiale Road & Kuikahi Drive (LOS F AM peak hour and LOS E PM peak hour)
- <u>Intersection 3: S. Kamehameha Avenue & Maui Lani Parkway</u> (LOS F AM peak hour and PM peak hour)
- <u>Intersection 4: Kuihelani Highway (Highway 380) & Maui Lani Parkway</u> (LOS F AM peak hour and LOS E PM peak hour)
- <u>Intersection 7: S. Kamehameha Avenue & Waiko Road</u> (LOS F AM peak hour and PM peak hour)

In addition, a project-specific impact has been identified at Intersection 1: Honoapiilani Highway & Kuikahi Drive during the PM peak hour, where the addition of project-generated traffic would cause the overall intersection operations to degrade from LOS D to LOS E.

YEAR 2026 NO PROJECT TRAFFIC CONDITIONS

This section presents an analysis of potential future traffic conditions projected for the Year 2026. The Year 2026 No Project or cumulative base traffic volumes projected in Chapter 3 were analyzed using the methodologies described in Chapter 1 to forecast cumulative base peak hour LOS at the study intersections. The first few columns in **Table 7** summarize the results of this analysis and the corresponding LOS calculation sheets are included in **Appendix B**.

The results of the LOS calculations indicate that all of the future study intersections operate at an overall acceptable service level (LOS D or better) in 2026, with the exception of the following locations:

- <u>Intersection 1: Honoapiilani Highway (Highway 30) & Kuikahi Drive</u> (LOS E AM peak hour)
- <u>Intersection 2: Waiale Road & Kuikahi Drive</u> (LOS F AM peak hour and LOS E PM peak hour)
- <u>Intersection 3: S. Kamehameha Avenue & Maui Lani Parkway</u> (LOS F AM peak hour and PM peak hour)
- <u>Intersection 4: Kuihelani Highway (Highway 380) & Maui Lani Parkway</u> (LOS F AM peak hour and LOS E PM peak hour)
- <u>Intersection 7: S. Kamehameha Avenue & Waiko Road</u> (LOS F AM peak hour and PM peak hour)

The remaining five study intersections are expected to continue operating at an overall desirable LOS (LOS D or better) during both peak hours.

TABLE 7 – YEAR 2026 LEVELS OF SERVICE - WAIKAPU COUNTRY TOWN FULL DEVELOPMENT (PHASE 1 & 2)

| | | | | Year 2026 N | o Project | Year 2026 with | Phase 1&2 | | | | Mitigated to | : | |
|-----|---|--------------------|--------------|----------------------|--------------------|----------------------|--------------------|-----------------|----------------------|----------------------------|------------------------|----------------------|--------------------|
| | Intersection | Traffic Control | Peak Hour | Conditi | | Conditi | | Delay Change | Mitigation Required? | Pre-Project or Bett LOS | | LOS D or Condit | |
| | | | | Del/Veh ¹ | LOS ^{2,3} | Del/Veh ¹ | LOS ^{2,3} | | | Del/Veh ¹ | LOS ^{2,3} | Del/Veh ¹ | LOS ^{2,3} |
| -1 | Harris Charles and Mark Day | 6' | AM | 75.3 | E | 111.1 | F | 35.8 | YES | 50.3 | D | Same as Pro | e-Project |
| 1. | Honoapiilani Highway / Kuikahi Drive | Signal | PM | 46.3 | D | 77.0 | E | 30.7 | YES | 37.7 | D | Mitigation | |
| 2 | Waiale Road / Kuikahi Drive | Cianal | AM | 87.8 | F | 149.2 | F | 61.4 | YES | 81.8 | F | 46.6 | D |
| 2. | Walale Road / Kulkani Drive | Signal | PM | 55.3 | E | 99.4 | F | 44.1 | YES | 41.5 | D | 33.3 | С |
| 3. | S. Kamehameha Avenue / Maui Lani | AWSC | AM | > 180 | F | > 180 | F | ** | YES | > 180 | F | 30.2 | C |
| | Parkway ⁶ | AVVSC | PM | > 180 | F | > 180 | F | ** | YES | 167.9 | F | 19.4 | В |
| 4. | Kuihelani Highway / Maui Lani | Signal | AM | 105.0 | F | 139.5 | F | 34.5 | YES | 27.2 | C | Same as Pro | e-Project |
| | Parkway | Signal | PM | 75.9 | E | 100.1 | F | 24.2 | YES | 31.2 | С | Mitiga | tion |
| 5. | Honoapiilani Highway / Waiko Road | Signal | AM | 18.6 | В | 46.9 | D | 28.3 | NO | | No Mitigation Requ | iirad | |
| ٥. | Tionoapiliarii Tiigriway / Walko Koad | Signal | PM | 18.5 | В | 37.8 | D | 19.3 | NO | | No wingation kequ | uneu | |
| 6. | Waiale Road / Waiko Road ^{4,9} | Signal | AM | 9.0 | Α | 15.0 | В | 6.0 | NO | | No Mitigation Required | | |
| 0. | Walale Road / Walko Road | Signal | PM | 7.5 | Α | 8.9 | Α | 1.4 | NO | | No willigation Kequ | uneu | |
| 7. | S. Kamehameha Avenue / Waiko | SSSC | AM | ** | F | ** | F | ** | YES | 10.1 | В | Same as Pro | |
| | Road ^{6,7} | 3330 | PM | > 180 | F | ** | F | ** | YES | 8.1 | Α | Mitiga | tion |
| 8. | Kuihelani Highway / Waiko Road | Signal | AM | 41.6 | D | 58.2 | E | 16.6 | YES | 25.2 | С | Same as Pro | e-Project |
| 0. | Rullielatii Fiigriway / Walko Road | Signal | PM | 17.1 | В | 19.7 | В | 2.6 | NO | 15.6 | В | Mitiga | tion |
| 9. | Honoapiilani Highway / Main Street ^{5,8} | Signal | AM | Only built wit | h project | 9.8 | Α | 9.8 | NO | | No Mitigation Requ | iirad | |
| ٦. | Tionoapmani riigilway / Waiii Street | Signal | AM | Offiny Built Will | in project | 11.6 | В | 11.6 | NO | | No wingation kequ | uneu | |
| 10. | Waiale Road / Main Street ⁵ | Roundabout | AM | Only built wit | h project | 9.9 | Α | 9.9 | NO | | No Mitigation Requ | iirad | |
| 10. | | Rodridabout | PM | Offiny Built Will | in project | 10.3 | В | 10.3 | NO | | No wingation kequ | anea | |
| 11. | , , , | Signal | AM | Only built wit | h project | 8.3 | Α | 8.3 | NO | | No Mitigation Requ | iirad | |
| | Residential Street ^{5,8} | Signal | PM | Offiny Duffit Wife | in project | 6.1 | Α | 6.1 | NO | | No Mitigation Required | | |
| 12. | North-South Residential Street / | SSSC | AM | Only built wit | h project | 17.4 | C | 17.4 | NO | | No Mitigation Required | | |
| | Waiale Road ^{5,7} | 3330 | PM | Offig built wit | in project | 19.2 | C | 19.2 | NO | | | | |
| 13. | Honoapiilani Highway / Waiale Road ^{5,9} | Signal | AM | 6.0 | Α | 12.9 | В | 6.9 | NO | | No Mitigation Required | | |
| 15. | Honoapillatii Highway / Walale Kodu- | Signal | PM | 15.5 | В | 30.2 | C | 14.7 | NO | | | | |
| 14. | Honoapiilani Highway / Kuihelani | Cianal | AM | 22.5 | С | 24.0 | C | 1.5 | NO | | No Mitigation Requ | بندما | |
| | Highway | Signal | PM | 22.4 C | | 25.2 | С | 2.8 | NO | | ııred | | |

Source: Fehr & Peers, 2014

Notes:

^{**} Indicated oversaturated conditions. Delay cannot be calculated. AWSC = All-way stop-controlled intersection; SSSC = Side-street stop-controlled intersection.

¹Whole intersection weighted average stopped delay expressed in seconds per vehicle for signalized and all-way stop-controlled intersections. The vehicular delay for the worst movement is reported for side street stop-controlled intersections.

²LOS calculations performed using the 2000 Highway Capacity Manual (HCM) method.

³ Unacceptable LOS highlighted in **bold.**

⁴ With the construction of the Waiale Bypass under future conditions, the intersection will include a fourth (south) leg and is assumed to be signalized.

⁵ Intersection provides access to the project site.

⁶ The proposed mitigation measure at this location is signalization and the delay and LOS displayed under this condition is based on the average control delay for the intersection as a whole.

⁷ Intersection is or is assumed to be controlled by stop signs on the minor approach(es).

⁸ The project intersection is assumed to be signalized in 2026.

⁹ Intersection assumed to be signalized as part of the Waiale Bypass project.

YEAR 2026 WITH PROJECT TRAFFIC CONDITIONS

The Year 2026 with Project or cumulative plus project Phase 1 & 2 peak hour traffic volumes illustrated in **Figure 9**, were analyzed to determine 2026 operating conditions with the addition of project-related traffic. The results of the Year 2026 with Project analysis is presented in **Table 7** and the corresponding LOS calculation sheets are included in **Appendix B**.

The proposed project would contribute to cumulative impacts (LOS E or F conditions) during one or both peak hours at six study intersections:

- Intersection 1: Honoapiilani Highway (Highway 30) & Kuikahi Drive (LOS F AM peak hour)
- Intersection 2: Waiale Road & Kuikahi Drive (LOS F AM peak hour and PM peak hour)
- <u>Intersection 3: S. Kamehameha Avenue & Maui Lani Parkway</u> (LOS F AM peak hour and PM peak hour)
- <u>Intersection 4: Kuihelani Highway (Highway 380) & Maui Lani Parkway</u> (LOS F AM peak hour and PM peak hour)
- Intersection 7: S. Kamehameha Avenue & Waiko Road (LOS F AM peak hour and PM peak hour)

In addition, project-specific impacts have been identified at intersections where the addition of project-generated traffic would cause their overall intersection operations to degrade below LOS D in the peak hours. The project-related impacts identified are:

- <u>Intersection 1: Honoapiilani Highway (Highway 30) & Kuikahi Drive</u> (cumulative and project-specific impact)
- Intersection 8: Kuihelani Highway (Highway 380) & Waiko Road (LOS E AM peak hour)

POTENTIAL TRAFFIC IMPROVEMENTS

Potential traffic improvements were developed to increase the capacity and/or efficiency of the roadway system at the locations where the addition of project-related traffic would cause or contribute to poor operating conditions. The emphasis was to identify physical and/or operational improvements that could be implemented within the existing or planned roadway rights-of-way. The potential intersection improvement measures are illustrated in **Appendix F. Table 6** and **Table 7** summarize the projected LOS in 2022/2026 at the impacted locations with these proposed measures in place.

The potential measures to address the identified traffic impacts are described later in this chapter. Each of the identified impacts would be reduced such that future operations would be at the minimum desired LOS (LOS D) for the overall intersection with the project in place. Although HDOT also strives to maintain

LOS D or better conditions at the movement level, measures to improve turning movement conditions would only be proposed where feasible and appropriate from a traffic engineering perspective since adding lanes just to achieve the desired LOS for a particular movement also has secondary negative impacts to the environment and to active transportation modes.

The scope of corresponding improvements for this type of mitigation process can be well beyond the project's actual impact, and could effectively eliminate existing or cumulative deficiencies, which should not be the project's responsibility consistent with State of Hawaii law. Therefore, in addition to developing improvements that will result in LOS D or better operations, measures that only return operations to preproject levels have also been identified (i.e., under Year 2022 No Project Conditions and Year 2026 No Project Conditions). This is especially important where the addition of project traffic alone would not degrade operations below LOS D, but would contribute to projected poor levels of service caused by the addition of traffic from other cumulative developments (e.g., Puunani Residences, Waiale Development, etc.).

The full range of improvements that address both project-related and/or cumulative traffic impacts are discussed in detail below. The specific improvements that are proposed to be fully implemented by WCT are specified in a subsequent section.

Intersection 1: Honoapi`ilani Highway & Kuikahi Drive (Year 2022 & 2026) – The impact at this intersection could be reduced by widening the westbound approach from a shared through/left-turn lane and right-turn lane to a left-turn lane, a through lane, and a right-turn lane, and widening the southbound approach from a left-turn lane, a through lane, and a right-turn lane to two left-turn lanes, a through lane, and a right-turn lane. Additionally, to complement the addition of a second southbound left-turn lane, the east leg would need to be widened to provide a second departure lane and the northbound and southbound left-turn phasing would need to be converted to protected left turns. This improvement would result in LOS D operations, and no other measure is feasible that would only mitigate the operations to pre-project levels.

Although the measures described above would improve the Year 2022 AM and PM peak hour impacts at the overall intersection level, half of the left-turn movements are projected to continue to operate at LOS E or F in both peak hours. The volumes and V/C ratios for the left-turn movements are as follows:

- o AM Peak Hour
 - Westbound: single left-turn lane with 330 vehicles and a V/C ratio of 1.09
 - Southbound: dual left-turn lanes with 440 vehicles and a V/C ratio of 0.98

o PM Peak Hour

- Westbound: single left-turn lane with 384 vehicles and a V/C ratio of 0.98
- Southbound: dual left-turn lanes with 370 vehicles and a V/C ratio of 0.94

The HCM recommends considering the provision of double left-turn lanes when the volume exceeds 300 vehicles. In the case of the southbound approach, the left-turn movement already has two left-lanes and from a volume standpoint does not warrant a third left-turn lane and the V/C ratios are within the acceptable range. Therefore, no further improvements are proposed for the southbound approach.

Although the westbound approach, is projected to warrant the provision of double left-turn lanes from a volume standpoint during both peak hours and the V/C ratio is greater than 1.0 during the AM peak hour, these movements and approaches were already operating below LOS D in preproject conditions. Thus, proposing dual westbound left-turn lanes would be well beyond the project's actual impact. Additionally, implementing a second westbound left-turn lane would require more widening on the east leg, and widening of the south leg of Honoapiilani Highway to provide a second receiving lane to accommodate the left-turn movement. Therefore, no further project improvements are recommended for the westbound approach.

Similarly, the measures would only reduce the Year 2026 AM and PM peak hour impacts at the overall intersection level. During the AM and PM peak hour, three of the four left-turn movements are projected to continue to operate at LOSE or F. The volumes and V/C ratios for the left-turn movements are as follows:

o AM Peak Hour

- Westbound: single left-turn lane with 303 vehicles and a V/C ratio of 1.08
- Northbound: single left-turn lane with 61 vehicles and a V/C ratio of 0.99
- Southbound: dual left-turn lanes with 460 vehicles and a V/C ratio of 1.01

PM Peak Hour

- Westbound: single left-turn lane with 367 vehicles and a V/C ratio of 1.02
- Northbound: single left-turn lane with 73 vehicles and a V/C ratio of 0.90
- Southbound: dual left-turn lanes with 400 vehicles and a V/C ratio of 0.92

In the case of the southbound approach, the left turn movement already has two left-lanes and from a volume standpoint does not warrant a third left-turn lane and the V/C ratios are mostly within the acceptable range. For the northbound left-turn lanes, the deficient lane operations are

not a result of capacity constraints, but rather signal operations. Therefore, no further improvements are proposed for both the southbound and northbound approaches.

Although the westbound approach, is projected to warrant the provision of double left-turn lanes from a volume standpoint and the V/C ratios are greater than 1.0 during both peak hours, these movements and approaches were already operating below LOS D in pre-project conditions. Thus, proposing dual westbound left-turns would be well beyond the project's actual impact. Additionally, implementing a second westbound left-turn lane would require more widening on the east leg, and widening of the south leg of Honoapiilani Highway to provide a second receiving lane to accommodate the left-turn movement. Therefore, no further project improvements are recommended for the westbound approach.

Additionally, under Year 2026 with Project Conditions the northbound through movement is projected to operate at LOS E in the AM peak hour with a V/C ratio of 0.97. However, because the 572 vehicles traveling through do not necessarily warrant an additional through lane and the improvement would require right-of-way acquisition along Honoapiilani Highway, no further physical improvements are proposed for this approach.

• Intersection 2: Waiale Road & Kuikahi Drive (Year 2022 & 2026) – The pre-project improvement includes widening the eastbound and westbound approaches to provide a left-turn lane, two through lanes, and a right-turn lane. To complement the widening of the eastbound and westbound approaches, both the eastbound and westbound departures would also need to be widened to each provide a second receiving lane. The LOS D or better measure includes the pre-project improvements plus widening the northbound approach to provide a left-turn lane, a through lane, and a right-turn lane.

The measures described above would mitigate the Year 2022 PM peak hour impact so that the overall intersection and intersection movements or approaches would operate at acceptable LOS D or better.

For the Year 2022 AM peak hour, the impact at the overall intersection level would be mitigated; however, two of the four left-turn movements are projected to continue to operate at LOS E or F. The volumes and V/C ratios for the left-turn movements are as follows:

o AM Peak Hour

- Eastbound: single left-turn lane with 364 vehicles and a V/C ratio of 1.04
- Southbound: single left-turn lane with 240 vehicles and a V/C ratio of 1.00

The HCM recommends considering the provision of double left-turn lanes when the volume exceeds 300 vehicles. In the case of the southbound approach, the left turn movement does not warrant the provision of a second left-turn lane from a volume standpoint and the V/C ratios is within the acceptable range. Therefore, no further improvements are proposed for the southbound approach.

Although the eastbound approach is projected to warrant the provision of double left-turn lanes from a volume standpoint and the V/C ratio is greater than 1.0, this movement and approach were already operating below LOS D in pre-project conditions. Thus, proposing dual eastbound left-turns would be well beyond the project's actual impact at the approach-level. Additionally, implementing a second eastbound left-turn lane would require more widening on the west leg, and widening of the north leg of Waiale Road to provide a second receiving lane to accommodate the left-turn movement. Therefore, no further project improvements are recommended for the eastbound approach.

Similarly, the measures described would mitigate the Year 2026 PM peak hour impact so that the overall intersection and intersection movements or approaches would operate at acceptable LOS D or better.

For the Year 2026 AM peak hour, the impact at the overall intersection level would be mitigated; however, two of the four left-turn movements are projected to continue to operate at LOS F. The volumes and V/C ratios for the left-turn movements are as follows:

o AM Peak Hour

- Eastbound: single left-turn lane with 372 vehicles and a V/C ratio of 1.07
- Southbound: single left-turn lane with 250 vehicles and a V/C ratio of 1.15

For the southbound approach, the left turn movement does not warrant the provision of a second left-turn lane from a volume standpoint. Therefore, no further improvements are proposed for the southbound approach.

Although the eastbound approach is projected to warrant the provision of double left-turn lanes from a volume standpoint and the V/C ratio is greater than 1.0, this movement and approach were already operating below LOS D in pre-project conditions. Thus, proposing dual eastbound left-turn lanes would be well beyond the project's actual impact at the approach level. Additionally, implementing a second eastbound left-turn lane would require more widening on the west leg, and widening of the north leg of Waiale Road to provide a second receiving lane to

accommodate the left-turn movement. Therefore, no further project improvements are recommended for the eastbound approach.

Additionally, under Year 2026 with Project Conditions the northbound through movement is projected to operate at LOS E in the AM peak hour with a V/C ratio of 0.98. However, because the 587 vehicles traveling through do not necessarily warrant an additional through lane and the improvement would require right-of-way acquisition along Waiale Road, no further physical improvements are proposed for this approach.

• Intersection 3: S. Kamehameha Avenue/Maui Lani Parkway (Year 2022) – The pre-project improvement is installing a traffic control signal with permitted phasing at all approaches. Although the intersection conditions are better than pre-project conditions with the implementation of a traffic control signal, the intersection would still operate with long delays in excess of 180 seconds during both peak hours in 2022. For LOS D or better operations, not only would the traffic signal need to be installed but the eastbound approach would need to provide a left-turn lane and a shared through/right-turn lane and the westbound approach would need to provide a left-turn lane, a through lane, and a right-turn lane.

Although the measures described above would mitigate the Year 2022 AM peak hour impact at the overall intersection level, the northbound left-turn movement is projected to operate at LOS F with a V/C ratio of 1.22. Since the volumes at this movement do not warrant the provision of a second left-turn lane based on the HCM recommended provision of dual left-turn lanes, no further improvements are proposed for this approach.

Similarly, the improvements would also mitigate the PM peak hour impact at the overall intersection level; however, the following left-turn movements are projected to continue to operate at LOS E or F. The volumes and V/C ratios for the left-turn movements are as follows:

- Eastbound: single left-turn lane with 286 vehicles and a V/C ratio of 1.01
- Northbound: single left-turn lane with 150 vehicles and a V/C ratio of 0.93

Since the eastbound and northbound left-turn movements do not warrant the provision of a second left-turn lane from a volume standpoint and the V/C ratios are mostly within the acceptable range, no further improvements are proposed for these movements.

¹⁰ For this location and any other where a new signal is proposed, it is recommended that the need for a traffic signal at this location be monitored as overall development proceeds in the greater study area and that signal installation be dependent on future traffic engineering studies and full warrant analysis.

Additionally, under Year 2022 with Project Conditions the southbound shared through/right-turn lane is projected to operate at LOS E in the PM peak hour with 412 vehicles traveling through and 341 vehicles turning right and a V/C ratio of 1.08. Although the southbound approach does warrant the provision of a separate right-turn lane from a volume standpoint, this approach was already operating below LOS D in pre-project conditions. Thus, proposing dual right-turn lanes would be well beyond the project's actual impact and would require right-of-way acquisition along Kamehameha Avenue. Therefore, no further project improvements are recommended for the southbound approach.

Intersection 3: S. Kamehameha Avenue/Maui Lani Parkway (Year 2026) – The pre-project improvement is installing a traffic control signal with permitted phasing at all approaches. Although the intersection conditions are better than pre-project conditions with the implementation of the traffic control signal, the intersection would still operate with long delays in excess of 180 seconds during both peak hours in 2026. For LOS D or better operations, not only would the traffic signal need to be installed but the eastbound approach would need to provide a left-turn lane and a shared through/right-turn lane, the westbound approach would need to provide a left-turn lane, a through lane, and a right-turn lane, and the southbound would need to provide a left-turn lane, a through lane, and a right-turn lane.

The measures described above would mitigate the Year 2026 PM peak hour impact so that the overall intersection and intersection movements or approaches would operate at acceptable LOS D or better.

For the Year 2026 AM peak hour impact, however, the measures would only mitigate the impact at the overall intersection level. During the AM peak hour, three of the four left-turn movements are projected still operate at LOS E. The volumes and V/C ratios for the left-turn movements are as follows:

- o Northbound: single left-turn lane with 250 vehicles and a V/C ratio of 1.01
- o Southbound: single left-turn lane with 120 vehicles and a V/C ratio of 0.93
- Eastbound: single left-turn lane with 189 vehicles and a V/C ratio of 0.97

The HCM recommends considering the provision of double left-turn lanes when the volume exceeds 300 vehicles. Since these movements do not warrant the provision of a second left-turn lane from a volume standpoint and the V/C ratios are mostly within the acceptable range, no further improvements are proposed for these approaches.

• Intersection 4: Kuihelani Highway & Maui Lani Parkway (Year 2022 & 2026) – The impact at this intersection could be reduced by widening the eastbound approach to provide a left-turn lane, a shared through/left-turn lane, and a right-turn lane. In addition to the change in configuration, the eastbound and westbound left-turn phasing would need to be modified to split phasing. This improvement would result in LOS D operations, and no other measure is feasible that would only mitigate operations to pre-project levels.

Although the measures described above would reduce the Year 2022 AM and PM peak hour impacts at the overall intersection level, under AM peak hour conditions the northbound left-turn movement is projected to continue to operate at LOS F with 60 vehicles and a V/C ratio of 1.00.

During the Year 2022 PM peak hour, all three left-turn movements are projected to continue to operate at LOS E or F. The volumes and V/C ratios for the left-turn movements are as follows:

- Eastbound: single left-turn lane and shared through/left lane with 671 vehicles and a V/C
 ratio of 0.95
- Northbound: single left-turn lane with 60 vehicles and a V/C ratio of 1.07
- o Southbound: single left-turn lane with 10 vehicles and a V/C ratio of 0.73

The HCM recommends considering the provision of double left-turn lanes when the volume exceeds 300 vehicles. Since these movements either already have two left-turn lanes or do not warrant the provision of a second left-turn lane from a volume standpoint and the V/C ratios are mostly within the acceptable range, no further improvements are proposed for these approaches. Additionally, the deficient lane operations are not a result of capacity constraints, but rather signal operations.

The measures described above would mitigate the Year 2026 AM peak hour impact so that the overall intersection and intersection movements or approaches would operate at acceptable LOS D or better.

For the Year 2026 PM peak hour impact, however, the measures would only mitigate the impact at the overall intersection level. During the AM peak hour, three of the four left-turn movements are projected still operate at LOS E or F. The volumes and V/C ratios for the left-turn movements are as follows:

- Eastbound: single left-turn lane and shared through/left lane with 743 vehicles and a V/C
 ratio of 0.96
- o Northbound: single left-turn lane with 70 vehicles and a V/C ratio of 1.00
- Southbound: single left-turn lane with 10 vehicles and a V/C ratio of 1.00

Since these movements either already have two left-lanes or do not warrant the provision of a second left-turn lane from a volume standpoint and the V/C ratios are mostly within the acceptable range, no further improvements are proposed for these approaches. Additionally, the deficient lane operations are not a result of capacity constraints, but rather signal operations.

- <u>Intersection 7: S. Kamehameha Avenue/Waiko Road (2022 & 2026)</u> This impact at this intersection could be reduced by installing a traffic signal with permitted phasing at all approaches.¹⁰ This improvement would result in LOS D or better operations at both the overall intersection level and the turning movement level. No other measure is feasible that would only improve operations to pre-project levels.
- <u>Intersection 8: Kuihelani Highway/Waiko Road (2026)</u> This impact at this intersection could be reduced by widening and restriping the eastbound approach to provide a left-turn lane and a right-turn lane. No changes are proposed to the signal timing. No other improvement is feasible that would only mitigate operations to pre-project levels.

The measure described above would improve the Year 2026 PM peak hour impact so that the overall intersection and intersection movements or approaches would operate at acceptable LOS D or better. For the Year 2026 AM peak hour impacts, however, the measure would only mitigate the impact at the overall intersection level. During the AM peak hour, the northbound left-turn movement is projected to operate at LOS E with 90 vehicles and a V/C ratio of 0.80. Based on HCM provisions for double left-turn lanes, the northbound left-turn movement does not warrant the provision of a second left-turn lane from a volume standpoint and the V/C ratio is within the acceptable range. Therefore, no further improvements are proposed for this approach.

MITIGATION FUNDING

For a project such as WCT that will be constructed in phases over an extended period of time, it is appropriate to identify the proposed project's share for the cost of the intersection improvements. Fairshare calculations for developer contributions were made for the intersections impacted by project-generated traffic. The estimates were developed by calculating the increase in traffic volumes from existing conditions to the Year 2026 with Project conditions. The increase establishes the total amount of projected growth at each location. Next, the WCT project-only volumes are divided by the total volume increase at each impacted intersection. This step determines the amount of traffic that the WCT project is contributing to the intersection and the approximate proportional contribution towards funding each potential proposed improvement.

The fair share calculations were performed for both the AM and PM peak hours, as shown in **Table 8**. For all but one location, the range of maximum project contribution is between 15.4% and 33.8%. At one location, the calculated maximum fair share does not accurately reflect the cause of the impacts at the intersection (i.e., the WCT causes the intersections to degrade from LOS D or better to LOS E or F). Based on the intersection analysis, the impact at Intersection 8: Kuihelani Highway & Waiko Road is project-specific (rather than a cumulative impact to which the project would make a fair-share contribution), and so that WCT should make a 100% contribution at this location.

While the project could make monetary contributions to partly fund the mitigation at all of the impacted locations, those improvements may not be implemented in a timely manner if the remaining funding is not available. Alternatively, HDOT has requested that projects fully fund the design and construction of improvements at selected locations under its jurisdiction that are roughly equal in value to the project's total collective fair-share contribution. While the project's fair-share contributions and the planning-level cost estimates for each element of the recommended mitigation program has not yet been finalized, a potential mitigation program for WCT is presented in the following section.

TABLE 8 – YEAR 2026 PROJECT FAIR SHARE INTERSECTION TRAFFIC CONTRIBUTION

| | | | AM Peak Hour | | | | | PM Peak Hour | | | | | |
|----|--|---------------------|------------------------------|-------------------------|----------------------------|-----------------------------------|---------------------|------------------------------|-------------------------|----------------------------|-----------------------------------|-------------------------|--|
| | Impacted Intersection | Existing Traffic | 2026 Projected Traffic | Total New Traffic | Project Only Traffic | Project % of New Traffic | Existing Traffic | 2026 Projected Traffic | Total New Traffic | Project Only Traffic | Project % of New Traffic | Maximum Contribution | |
| 1. | Honoapiilani Highway / Kuikahi Drive** | 2,073 | 3,238 | 318 | 1,165 | 27.3% | 1,928 | 3,184 | 424 | 1,256 | 33.8% | 33.8% | |
| 2. | Waiale Road / Kuikahi Drive* | 1,935 | 3,786 | 436 | 1,851 | 23.6% | 1,849 | 3,627 | 507 | 1,778 | 28.5% | 28.5% | |
| 3. | S. Kamehameha Avenue / Maui Lani Parkway* | 1,700 | 3,428 | 298 | 1,728 | 17.2% | 1,593 | 3,173 | 353 | 1,580 | 22.3% | 22.3% | |
| 4. | Kuihelani Highway / Maui Lani Parkway** | 1,856 | 4,013 | 273 | 2,157 | 12.7% | 2,011 | 4,150 | 330 | 2,139 | 15.4% | 15.4% | |
| 7. | S. Kamehameha Avenue / Waiko Road* | 0 | 1,709 | 229 | 1,709 | 13.4% | 0 | 1,629 | 289 | 1,629 | 17.7% | 17.7% | |
| 8. | Kuihelani Highway / Waiko Road** | 1,336 | 2,285 | 105 | 949 | 11.1% | 1,407 | 2,242 | 122 | 835 | 14.6% | 100 %¹ | |

Source: Fehr & Peers, 2014

^{*} County of Maui jurisdiction

^{**} State HDOT jurisdiction

¹ Based on Table 7, the impact at this intersection is directly attributable to the project. Therefore, the maximum contribution is assumed for this intersection.

PROPOSED WCT MITIGATION PROGRAM

As discussed, improvements are proposed at intersections identified as significantly impacted under Year 2026 with Project Conditions. In the past, development projects would make a fair share financial contribution for each mitigation measure to the appropriate governing agency (i.e., the County or HDOT). However, simply providing partial funds for a variety of different improvements does not ensure construction of any individual improvement.

More recently, HDOT has indicated a preference for development projects like WCT to fully design and build improvements at a select set of locations to ensure their implementation. Accordingly, a mitigation program for WCT was developed that would require construction of improvements at intersections closer to the project site where the project contributes to, but does not directly cause a significant impact. Note that the mitigation program described below is a preliminary recommendation based on project proximity to intersections and without planning level cost estimates. As such, it is subject to change as the planning process continues.

The project proposes to fully fund mitigation measures that would return operations to pre-project levels at Intersection 1: Honoapi`ilani Highway & Kuikahi Drive and Intersection 8: Kuihelani Highway & Waiko Road. Additionally, although Intersection 13: Honoapiilani Highway & Waiale Road is not significantly impacted under Year 2026 with Project Conditions, the project may also be responsible for funding intersection improvements necessary to provide access to the project site (i.e., a fourth/west leg).

IMPROVEMENTS TO BE IMPLEMENTED BY OTHERS

For the remaining impacted intersections listed below, it is assumed that other development projects that are adjacent or in closer proximity to these impacted locations would be responsible for implementing the necessary intersection improvements:

- Intersection 2: Waiale Road & Kuikahi Drive
- Intersection 3: S. Kamehameha Avenue & Maui Lani Parkway
- Intersection 4: Kuihelani Highway & Maui Lani Parkway
- Intersection 7: S. Kamehameha Avenue & Waiko Road

6. ASSESSMENT OF SITE PLAN AND MULTI-MODAL REVIEW

The following section provides a summary of WCT's site access and circulation plan for bicycle, pedestrian, and transit facilities.

ROADWAY NETWORK

The proposed WCT site plan details an extensive internal roadway system which allows community residents and visitors to have multiple options for accessing neighborhoods, employment centers, and commercial and institutional uses. At full buildout of the project, access to mauka and makai land uses are provided along Honoapiilani Highway at four-legged, controlled intersections with Main Street, East-West Residential Street, and Waiale Road. Additional access to the makai land uses are provided along the Waiale Bypass at a roundabout with Main Street and a three-legged intersection with the major North-South Residential Street. Overall, the proposed WCT would provide sufficient vehicular connectivity to varying project uses and the multiple site access points help to better distribute traffic entering and exiting the community.

Proposed intersection spacing along Honoapiilani Highway in this area averages about every 2,100 feet. The distance from Waiko Road to the future Main Street is about 2,400 feet, from the future Main Street to the future East-West Road is about 1,600 feet, and from the future East-West Road to the southern terminus of the future Waiale Bypass is about 2,400 feet. Although spacing is less than ½ a mile between these intersections, which is HDOT's recommended and desired spacing on major arterials, the project site lies within the urbanized area of Maui rather than a rural area, and so more closely-spaced intersections are reasonable in this project setting, even for a major arterial. Furthermore, intersection level of service analysis results under Year 2022 and 2026 conditions demonstrated that each of these intersections would operate at acceptable levels during the peak hours.

ROUNDABOUT ANALYSIS

Roundabouts are not recommended at any of the study intersections along Honoapiilani Highway. The rationale of this recommendation is based on the review of the HDOT's roundabout guidelines. According to the *Hawaii Department of Transportation Modern Roundabout Policy Guideline* (HDOT, 2008):

• Modern roundabouts involve low speeds for entering and circulating traffic and would need to be designed so that speeds of all vehicles is restricted to 35 mph or less within the roundabout.

- In situations where traffic volumes on both roadways are high and well balanced and/or where turning movements are relatively high, roundabouts provide better overall intersection operations and greater capacity than conventional intersection layouts.
- When the volumes on the major road are heavier than that on the minor road, the equal treatment of approaches may increase delay to the major road. Also, if the major road carries a heavy stream of through traffic, the lack of adequate gaps in the dominant flow may deter the minor flow from entering the roundabout during peak periods. Unless there are compelling reasons to do so, modern roundabouts need not be considered when less than 10% of the traffic enters the intersection from the minor roadway.
- No pedestrian activities take place across the circulating roadway or within the center island.
- Pedestrians and bicyclists may have difficulty finding the proper route through a modern roundabout due to unfamiliarity with operations.

Along Honoapiilani Highway the projected northbound and southbound volumes are considerably higher than the volumes on the cross streets, and since the traffic flow through roundabouts is limited only by the availability of gaps in the circulating flow, this minor street-major street volume imbalance could lead to potential greater delay experienced at the side streets trying to access Honoapiilani Highway. In particular, at Honoapiilani Highway & East-West Residential Street (Intersection 11) the minor roadway does not comprise more than 10% of the total intersection volume in either the AM or the PM peak hour under both 2022 and 2026 conditions. Thus, based on HDOT's factors to consider for modern roundabouts, none of the proposed intersections along Highway 30 (Intersections 9, 11, and 13) appear suitable for roundabout installation.

PEDESTRIAN NETWORK

The Waikapu Country Town Project follows new urbanist design principles that include compact, higher-density, mixed-uses, and an emphasis on walkability and connectivity through extensive pedestrian and bicycle networks on the project site. These characteristics by nature reduce vehicle trip making and promote use of non-motorized modes. Consistent with State of Hawaii and County of Maui policies on Complete Streets, the transportation facilities for the residential and commercial districts will be developed to form a balanced multi-modal network designed to provide mobility choices and to meet the needs of the community and all roadway users.

A primary objective of the project is to develop a community where walking and biking are the preferred modes of transportation for short commutes. Therefore, approximately eight miles of hiking, biking and walking trails will be incorporated into the project site along with one or two pedestrian/bicycle bridges

over Waiko Stream to the north. Also, the development makai of the highway will focus on a pedestrian oriented "main street" close to an elementary school and parks. A principal objective of the project's active transportation plan is to separate pedestrians and bicyclists from automobiles through the use of multi-use cycle tracks and trails. Such facilities will link the project's mauka and makai neighborhoods with the project's commercial areas, civic, and recreational facilities.

All of the project's streets will emphasize traffic calming and street scape beautification. The use of residential roundabouts at key intersections, landscape planting strips to buffer pedestrians from traffic and linear greenways will serve to beautify the project while providing motivation for residents to walk and bike more. The project's pedestrian and bicycle facilities will be designed to make walking and bicycling safe, accessible and an enjoyable activity for all age groups. Within the project's residential neighborhoods, sidewalks will be provided on both sides of the street and traffic calming will encourage on-street bicycle riding. **Figure 10** shows the project's non-motorized network of multi-use trails, pedestrian and bicycle facilities.

BIKE NETWORK

According to *Bike Plan Hawaii*, there will be more future bicycle facilities provided in the Wailuku-Kahului area, where the project site is located, based on its list of proposed facilities. Listed below are the proposed facilities in the project study area:

- Kamehameha Avenue between Papa Avenue and Maui Lani Parkway is planned to provide 0.7 miles of bicycle lane.
- Waiale Road is planned to become a signed shared road for a length of 4.0 miles between Maui Lani and Honoapiilani Highway.
- Also 5.3 miles of Kuihelani Highway is planned to become a signed shared road or path from Puunene Avenue to Honoapiilani Highway.

The Central Maui Pedestrian and Bicycle Master Plan for 2030 (State of Hawaii – Department of Health-Healthy Hawaii Initiative, 2012) further highlights that Waiale Road/Drive has significant unused ROW that could be used to create a separated pedestrian and bicycle path that will be an important link in connecting future growth in Waikapu to Kahului and Wailuku. The specific vision for this Waikapu-Waiale Road Connector is to connect Waikapu to Wailuku and Kahului by the Waiale Road Bikeway and provide a safe and convenient commute between communities. The Waiale Road Bikeway will be a contiguous bike path or cycle track between Kuikahi Drive and Waiko Road, which would then transition into a separated bike path, or at a minimum a bike lane with signage to Waiinu Road, and eventually transition into a multi-use path with a two-way bikeway and possible pedestrian path that would connect Waiinu Road or





Figure 10

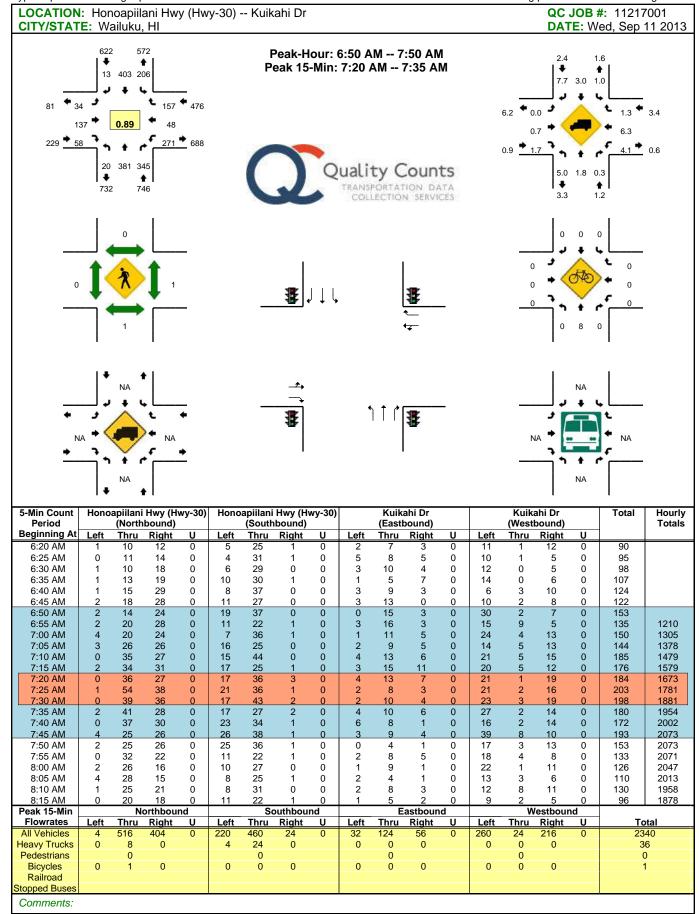
the Sandhills residential area with Lower Main Street or Wailuku. A local example of such a bikeway is in Kihei along Liola Drive between Waipuilani Road and Lipoa Street. The WCT project provides an opportunity to develop a major segment of this bikeway and to integrate it into the new community.

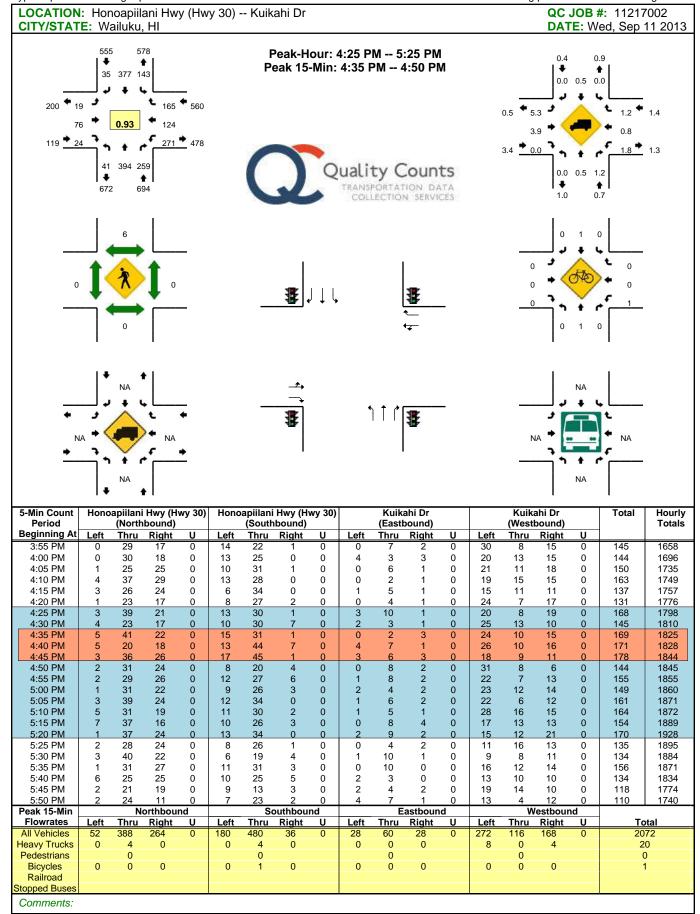
Additionally, the *Final Environmental Assessment for the Proposed Waiale Road Extension and East Waiko Road Improvements* (County of Maui, 2014) states that the Waiale Bypass will include a 10-foot bicycle/pedestrian path on the west side of the roadway.

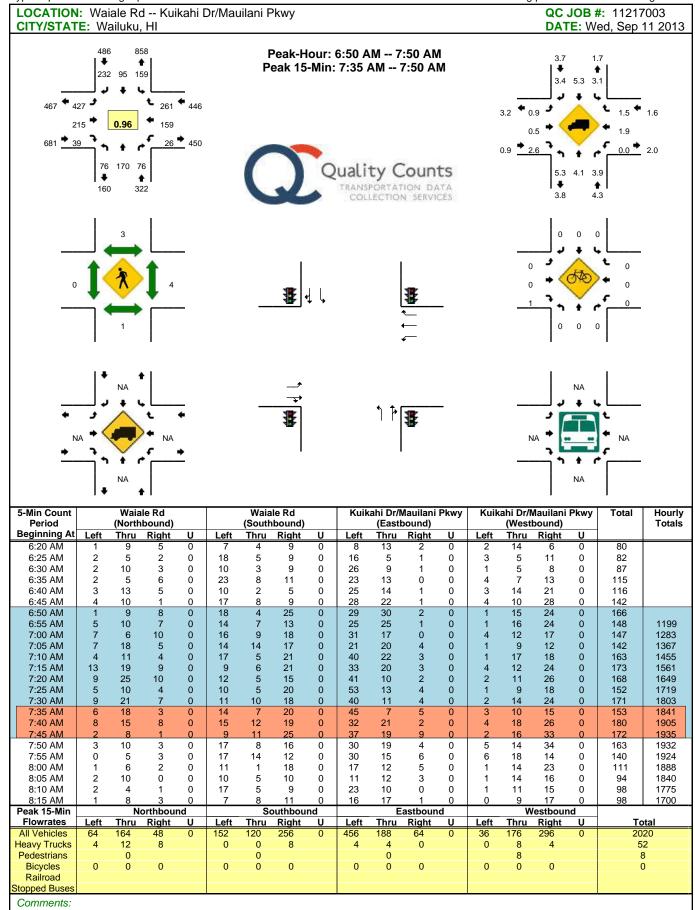
TRANSIT NETWORK

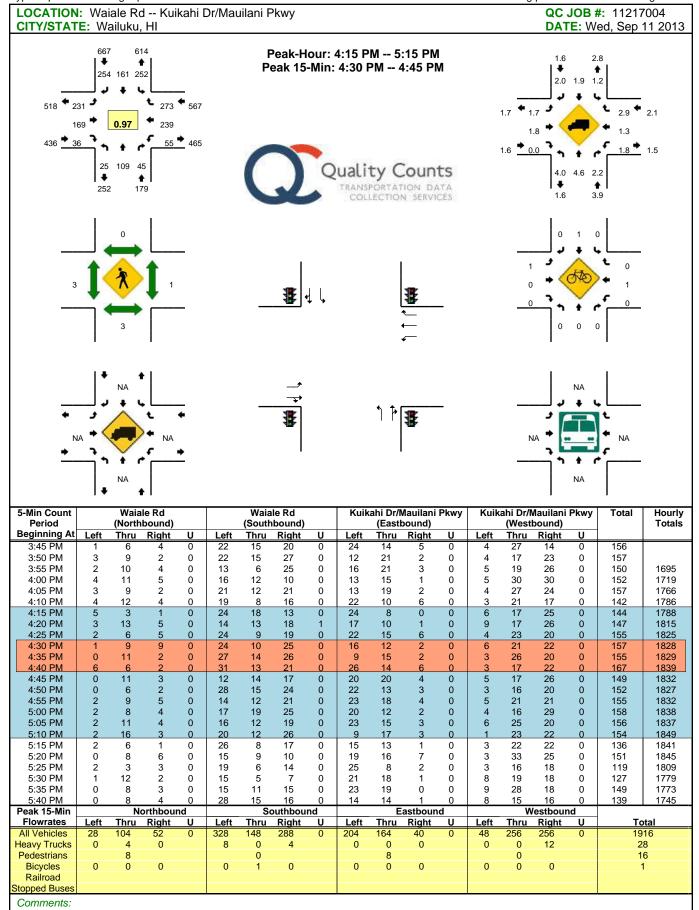
Under existing conditions, the Honoapiilani & Waiko bus stop is the only bus stop located in the project vicinity. While the Maui Bus has no immediate plans to expand service in this area, as the WCT site develops, the project allows for the introduction of public transit to the site, and service to the Waikapu Country Town should be considered as the County plans future expansion of public transit service in this area. Additionally, enhancements and amenities (i.e., benches or covered shelter) could be installed at the existing bus stop and any new bus stops to support future transit riders in this area.

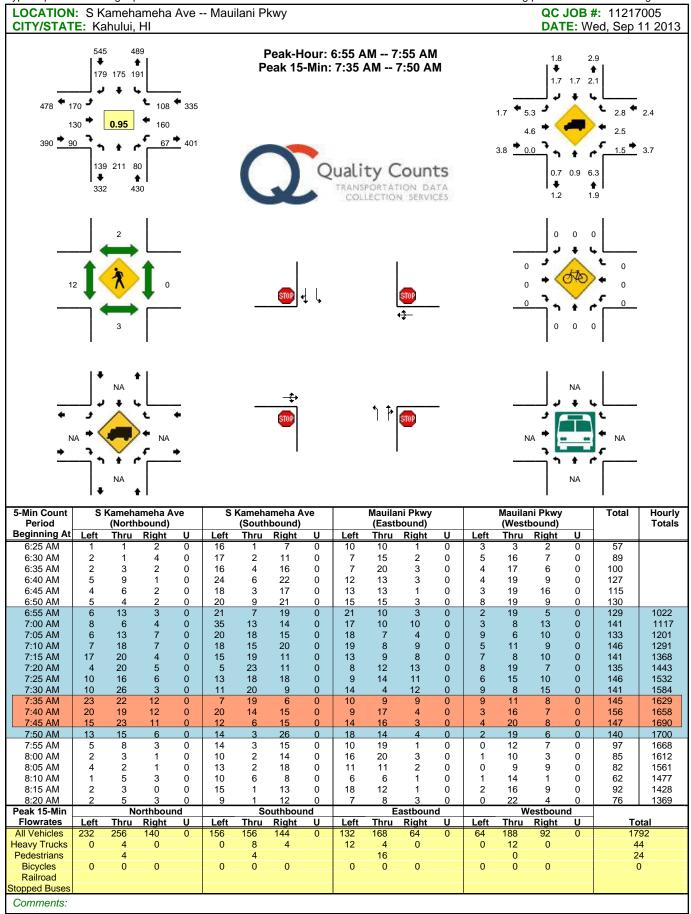
APPENDIX A: TRAFFIC COUNT DATA

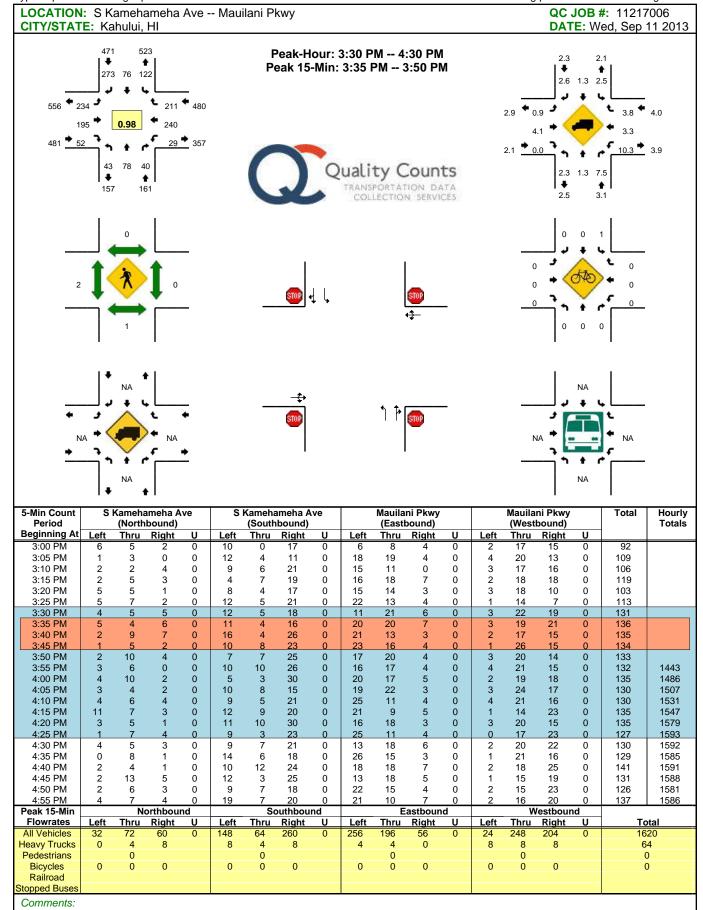


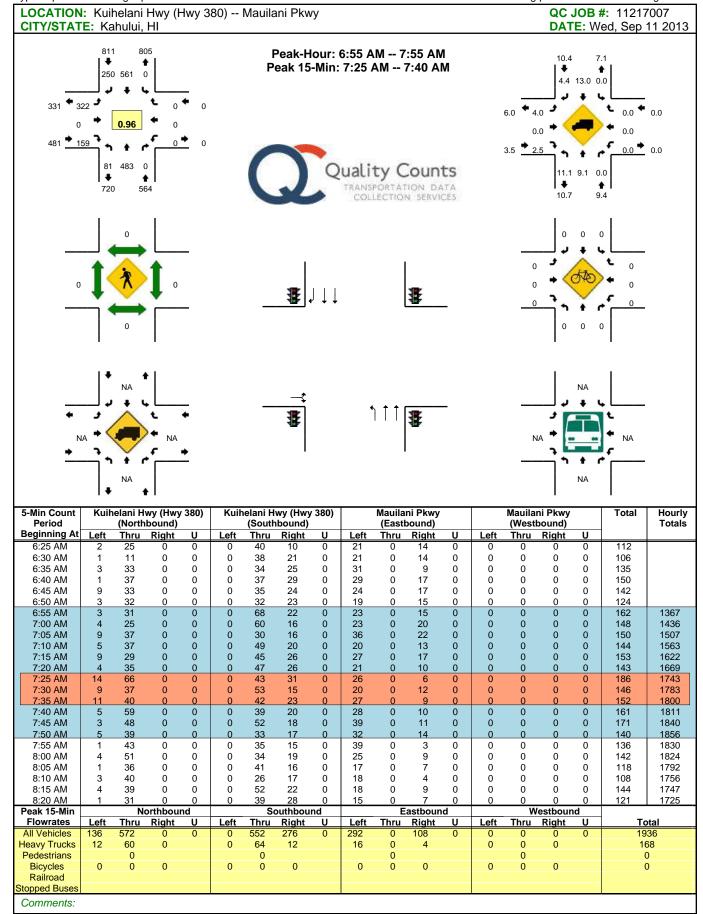


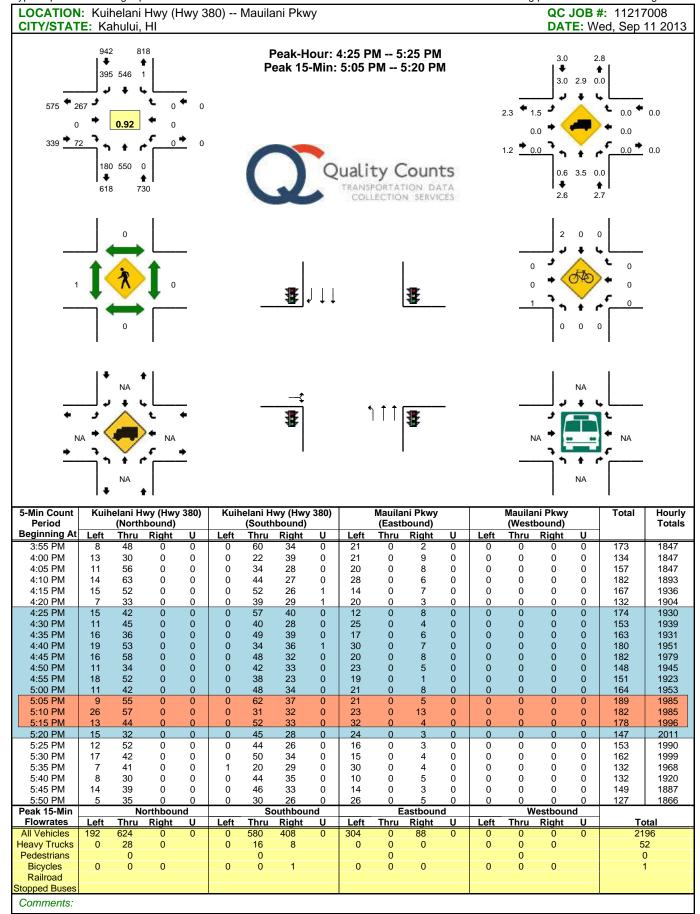


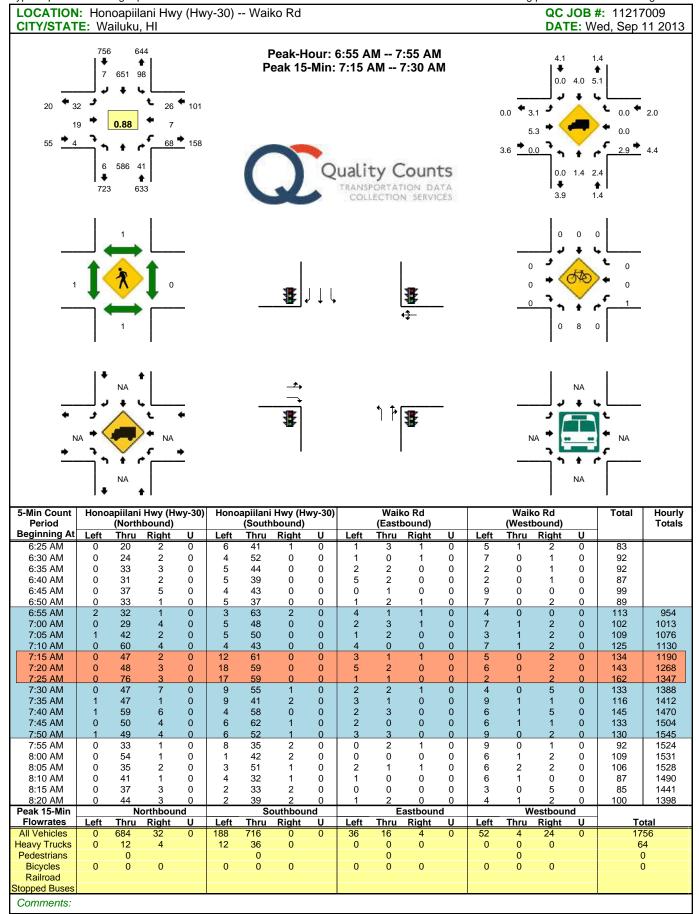


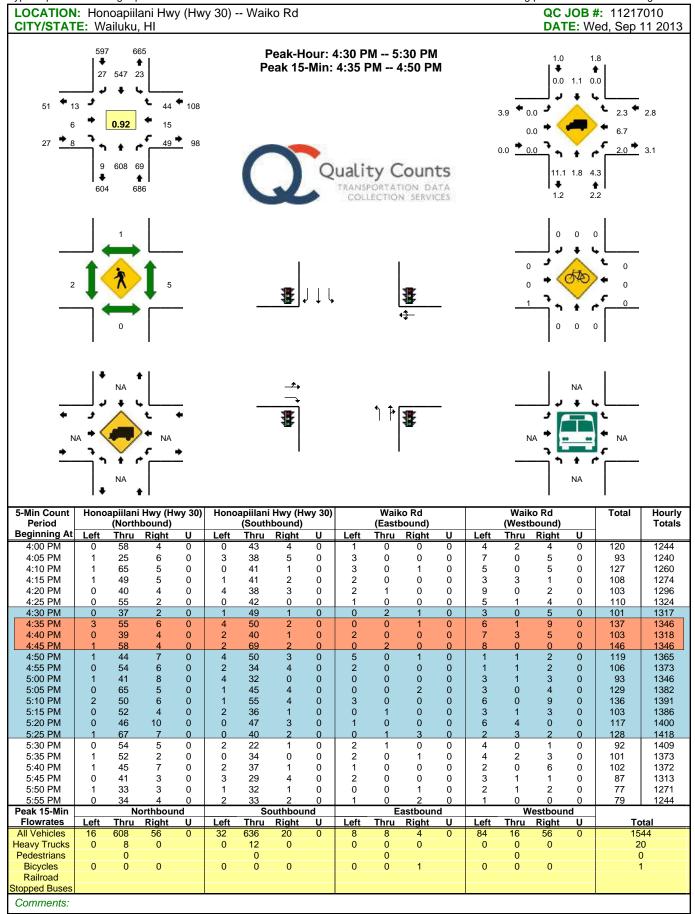


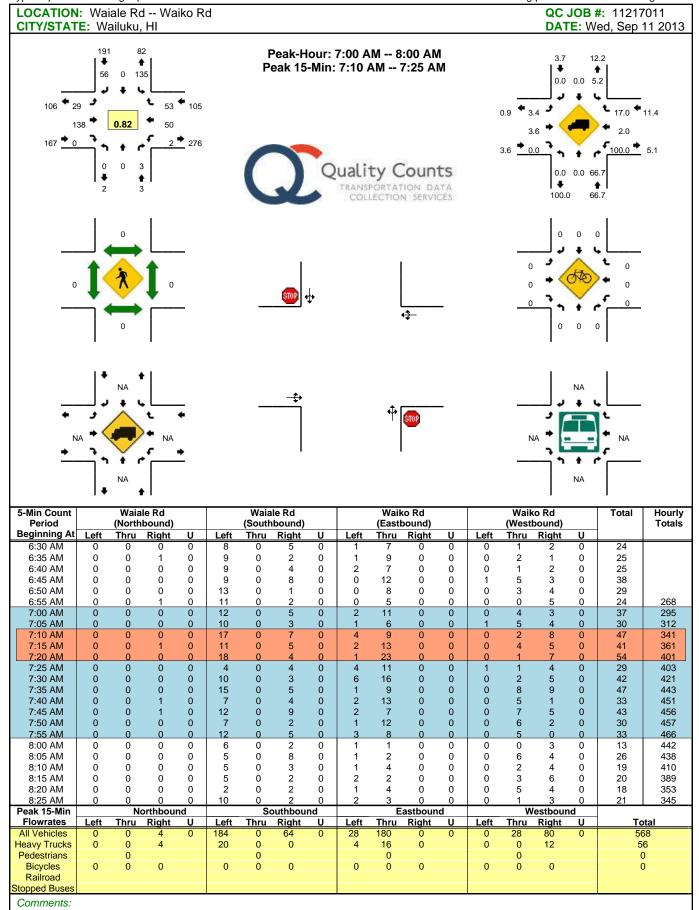


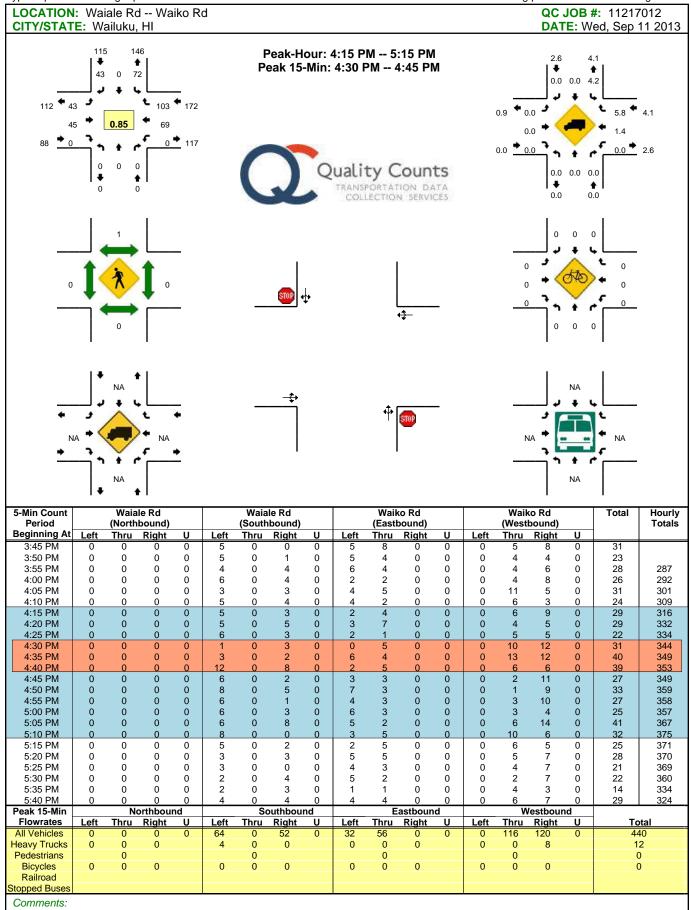


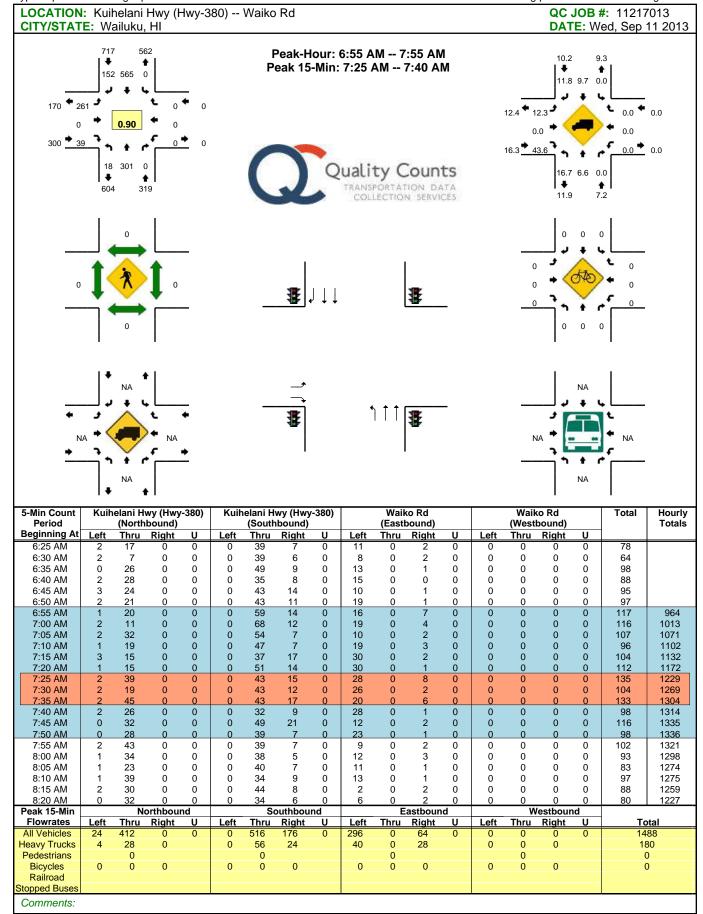


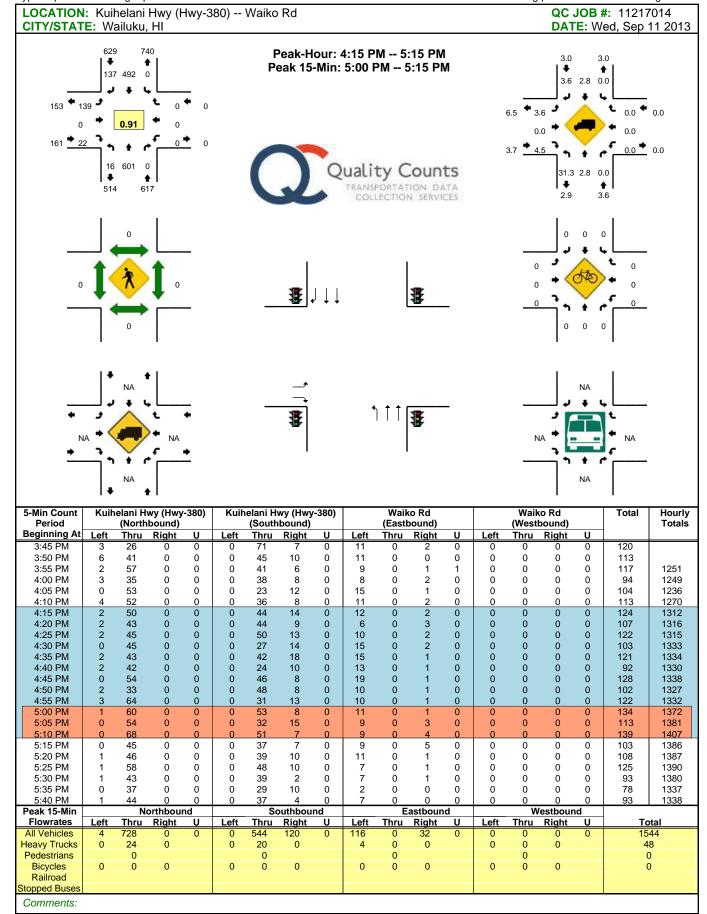


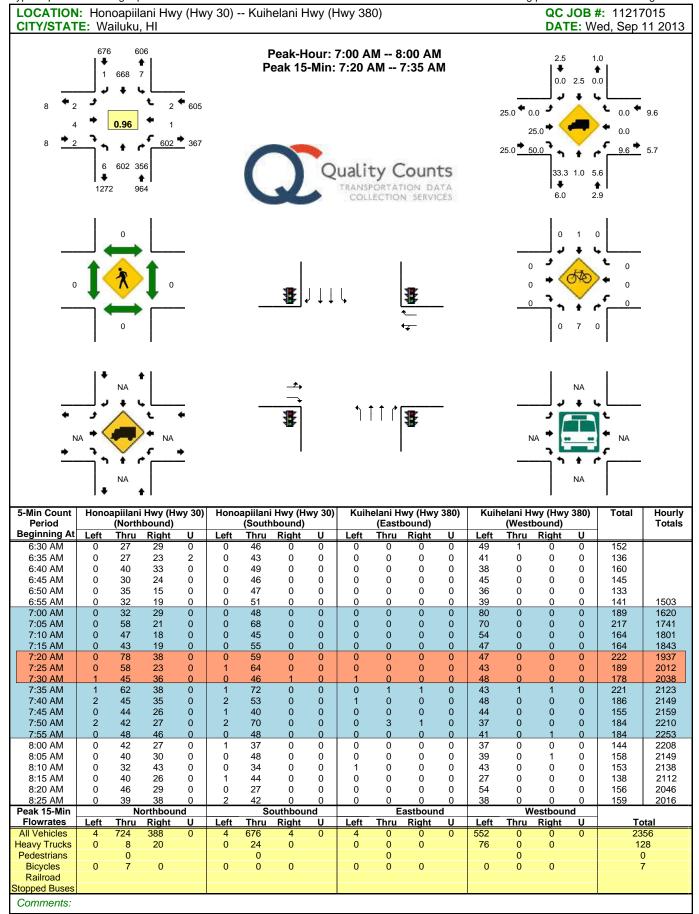


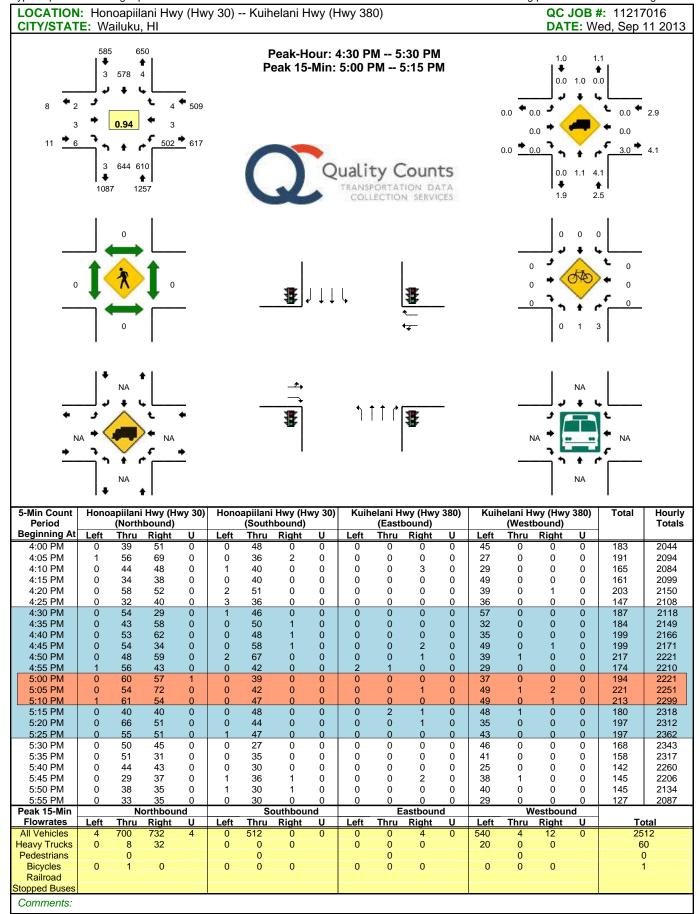












APPENDIX B: LOS WORKSHEETS

LOS Worksheets – Existing Conditions

| | • | → | • | • | + | • | • | † | ~ | / | ↓ | - ✓ |
|--------------------------------|-----------|----------|-------|------|-----------|------------|---------|----------|------|----------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | 7 | | 4 | 7 | Ĭ | † | 7 | Ť | † | 7 |
| Volume (vph) | 34 | 137 | 58 | 271 | 48 | 157 | 20 | 381 | 345 | 206 | 403 | 13 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 5.0 | 5.0 | | 5.0 | 5.0 | 4.0 | 5.0 | 5.0 | 4.0 | 5.0 | 5.0 |
| Lane Util. Factor | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frpb, ped/bikes | | 1.00 | 0.98 | | 1.00 | 1.00 | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 1.00 |
| Flpb, ped/bikes | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | | 1.00 | 0.85 | | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | | 0.99 | 1.00 | | 0.96 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | | 1844 | 1550 | | 1784 | 1583 | 1770 | 1863 | 1547 | 1770 | 1863 | 1583 |
| Flt Permitted | | 0.88 | 1.00 | | 0.59 | 1.00 | 0.46 | 1.00 | 1.00 | 0.27 | 1.00 | 1.00 |
| Satd. Flow (perm) | | 1640 | 1550 | | 1105 | 1583 | 862 | 1863 | 1547 | 510 | 1863 | 1583 |
| Peak-hour factor, PHF | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Adj. Flow (vph) | 38 | 154 | 65 | 304 | 54 | 176 | 22 | 428 | 388 | 231 | 453 | 15 |
| RTOR Reduction (vph) | 0 | 0 | 41 | 0 | 0 | 111 | 0 | 0 | 248 | 0 | 0 | 8 |
| Lane Group Flow (vph) | 0 | 192 | 24 | 0 | 358 | 65 | 22 | 428 | 140 | 231 | 453 | 7 |
| Confl. Peds. (#/hr) | | | 1 | 1 | | | | | 1 | | | |
| Turn Type | Perm | NA | Perm | Perm | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | 8 | 2 | | 2 | 6 | | 6 |
| Actuated Green, G (s) | | 34.6 | 34.6 | | 34.6 | 34.6 | 36.0 | 34.0 | 34.0 | 49.4 | 43.4 | 43.4 |
| Effective Green, g (s) | | 34.6 | 34.6 | | 34.6 | 34.6 | 36.0 | 34.0 | 34.0 | 49.4 | 43.4 | 43.4 |
| Actuated g/C Ratio | | 0.37 | 0.37 | | 0.37 | 0.37 | 0.38 | 0.36 | 0.36 | 0.53 | 0.46 | 0.46 |
| Clearance Time (s) | | 5.0 | 5.0 | | 5.0 | 5.0 | 4.0 | 5.0 | 5.0 | 4.0 | 5.0 | 5.0 |
| Vehicle Extension (s) | | 2.5 | 2.5 | | 2.5 | 2.5 | 2.0 | 5.0 | 5.0 | 2.0 | 5.0 | 5.0 |
| Lane Grp Cap (vph) | | 603 | 570 | | 406 | 582 | 349 | 673 | 559 | 420 | 860 | 730 |
| v/s Ratio Prot | | | | | | | 0.00 | c0.23 | | c0.07 | 0.24 | |
| v/s Ratio Perm | | 0.12 | 0.02 | | c0.32 | 0.04 | 0.02 | | 0.09 | 0.22 | | 0.00 |
| v/c Ratio | | 0.32 | 0.04 | | 0.88 | 0.11 | 0.06 | 0.64 | 0.25 | 0.55 | 0.53 | 0.01 |
| Uniform Delay, d1 | | 21.3 | 19.1 | | 27.8 | 19.6 | 18.2 | 24.9 | 21.1 | 14.4 | 18.0 | 13.7 |
| Progression Factor | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | | 0.2 | 0.0 | | 19.5 | 0.1 | 0.0 | 2.7 | 0.5 | 0.9 | 1.1 | 0.0 |
| Delay (s) | | 21.5 | 19.1 | | 47.3 | 19.6 | 18.2 | 27.6 | 21.6 | 15.3 | 19.1 | 13.7 |
| Level of Service | | С | В | | D | В | В | С | С | В | В | В |
| Approach Delay (s) | | 20.9 | | | 38.1 | | | 24.6 | | | 17.7 | |
| Approach LOS | | С | | | D | | | С | | | В | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 25.2 | H | CM 2000 | Level of | Service | | С | | | |
| HCM 2000 Volume to Capac | ity ratio | | 0.73 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 94.0 | | um of los | | | | 14.0 | | | |
| Intersection Capacity Utilizat | ion | | 73.9% | IC | CU Level | of Service | Э | | D | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| a Critical Lana Croun | | | | | | | | | | | | |

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|------------------------------|-------------|----------|-------|-------|-----------|------------|---------|------|-------------|----------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ħ | f) | | ሻ | † | 7 | 7 | f) | | ۲ | f) | |
| Volume (vph) | 427 | 215 | 39 | 26 | 159 | 261 | 76 | 170 | 76 | 159 | 95 | 232 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 5.0 | 5.0 | | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | | 5.0 | 5.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | 0.97 | 1.00 | 0.99 | | 1.00 | 1.00 | |
| Flpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frt | 1.00 | 0.98 | | 1.00 | 1.00 | 0.85 | 1.00 | 0.95 | | 1.00 | 0.89 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1767 | 1813 | | 1768 | 1863 | 1543 | 1770 | 1762 | | 1768 | 1664 | |
| Flt Permitted | 0.44 | 1.00 | | 0.60 | 1.00 | 1.00 | 0.36 | 1.00 | | 0.30 | 1.00 | |
| Satd. Flow (perm) | 818 | 1813 | | 1109 | 1863 | 1543 | 668 | 1762 | | 567 | 1664 | |
| Peak-hour factor, PHF | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Adj. Flow (vph) | 445 | 224 | 41 | 27 | 166 | 272 | 79 | 177 | 79 | 166 | 99 | 242 |
| RTOR Reduction (vph) | 0 | 4 | 0 | 0 | 0 | 219 | 0 | 13 | 0 | 0 | 69 | 0 |
| Lane Group Flow (vph) | 445 | 261 | 0 | 27 | 166 | 53 | 79 | 243 | 0 | 166 | 272 | 0 |
| Confl. Peds. (#/hr) | 3 | | 1 | 1 | | 3 | | | 4 | 4 | | |
| Turn Type | pm+pt | NA | | pm+pt | NA | Perm | pm+pt | NA | | pm+pt | NA | |
| Protected Phases | 7 | 4 | | 3 | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | | 8 | | 8 | 2 | | | 6 | | |
| Actuated Green, G (s) | 47.5 | 40.5 | | 19.8 | 17.8 | 17.8 | 24.1 | 18.6 | | 32.7 | 22.9 | |
| Effective Green, g (s) | 47.5 | 40.5 | | 19.8 | 17.8 | 17.8 | 24.1 | 18.6 | | 32.7 | 22.9 | |
| Actuated g/C Ratio | 0.52 | 0.45 | | 0.22 | 0.20 | 0.20 | 0.27 | 0.20 | | 0.36 | 0.25 | |
| Clearance Time (s) | 5.0 | 5.0 | | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | | 5.0 | 5.0 | |
| Vehicle Extension (s) | 2.0 | 3.0 | | 2.0 | 3.0 | 3.0 | 2.0 | 3.0 | | 2.0 | 3.0 | |
| Lane Grp Cap (vph) | 685 | 807 | | 256 | 364 | 302 | 243 | 360 | | 333 | 419 | |
| v/s Ratio Prot | c0.18 | 0.14 | | 0.00 | 0.09 | | 0.02 | 0.14 | | c0.05 | c0.16 | |
| v/s Ratio Perm | c0.16 | | | 0.02 | | 0.03 | 0.07 | | | 0.13 | | |
| v/c Ratio | 0.65 | 0.32 | | 0.11 | 0.46 | 0.18 | 0.33 | 0.68 | | 0.50 | 0.65 | |
| Uniform Delay, d1 | 14.3 | 16.3 | | 28.2 | 32.3 | 30.4 | 26.0 | 33.4 | | 21.4 | 30.4 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 1.6 | 0.2 | | 0.1 | 0.9 | 0.3 | 0.3 | 5.0 | | 0.4 | 3.5 | |
| Delay (s) | 15.9 | 16.6 | | 28.3 | 33.2 | 30.7 | 26.2 | 38.3 | | 21.8 | 33.9 | |
| Level of Service | В | В | | С | С | С | С | D | | С | С | |
| Approach Delay (s) | | 16.2 | | | 31.5 | | | 35.5 | | | 29.9 | |
| Approach LOS | | В | | | С | | | D | | | С | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 26.4 | Н | CM 2000 | Level of | Service | | С | | | |
| HCM 2000 Volume to Capa | acity ratio | | 0.69 | | | | | | | | | |
| Actuated Cycle Length (s) | • | | 90.9 | S | um of los | t time (s) | | | 20.0 | | | |
| Intersection Capacity Utiliz | ation | | 73.4% | | U Level | | е | | D | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| a Critical Lana Croup | | | | | | | | | | | | |

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|--------------------------------|-------|----------|-------|-------|---------|------------|------|------|-------------|-------------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | | | 4 | | ň | ₽ | | ň | 1> | |
| Sign Control | | Stop | | | Stop | | | Stop | | | Stop | |
| Volume (vph) | 170 | 130 | 90 | 67 | 160 | 108 | 139 | 211 | 80 | 191 | 175 | 179 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Hourly flow rate (vph) | 179 | 137 | 95 | 71 | 168 | 114 | 146 | 222 | 84 | 201 | 184 | 188 |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | NB 2 | SB 1 | SB 2 | | | | | | |
| Volume Total (vph) | 411 | 353 | 146 | 306 | 201 | 373 | | | | | | |
| Volume Left (vph) | 179 | 71 | 146 | 0 | 201 | 0 | | | | | | |
| Volume Right (vph) | 95 | 114 | 0 | 84 | 0 | 188 | | | | | | |
| Hadj (s) | -0.02 | -0.12 | 0.53 | -0.16 | 0.53 | -0.32 | | | | | | |
| Departure Headway (s) | 8.8 | 8.8 | 9.8 | 9.1 | 9.6 | 8.8 | | | | | | |
| Degree Utilization, x | 1.01 | 0.86 | 0.40 | 0.78 | 0.54 | 0.91 | | | | | | |
| Capacity (veh/h) | 411 | 403 | 351 | 386 | 361 | 400 | | | | | | |
| Control Delay (s) | 77.1 | 47.1 | 18.0 | 36.3 | 22.1 | 53.4 | | | | | | |
| Approach Delay (s) | 77.1 | 47.1 | 30.4 | | 42.4 | | | | | | | |
| Approach LOS | F | Е | D | | Е | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Delay | | | 48.3 | | | | | | | | | |
| Level of Service | | | Ε | | | | | | | | | |
| Intersection Capacity Utilizat | ion | | 81.1% | IC | U Level | of Service | | | D | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

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|-----------------------------------|----------|----------|-------|------|-------------|------------|---------|------------|-------------|----------|------------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | | | | | 7 | ∱ ∱ | | 7 | † † | 7 |
| Volume (vph) | 322 | 0 | 159 | 0 | 0 | 0 | 81 | 483 | 0 | 0 | 561 | 250 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 6.0 | | | | | 5.0 | 7.0 | | | 7.0 | 7.0 |
| Lane Util. Factor | | 1.00 | | | | | 1.00 | 0.95 | | | 0.95 | 1.00 |
| Frt | | 0.96 | | | | | 1.00 | 1.00 | | | 1.00 | 0.85 |
| Flt Protected | | 0.97 | | | | | 0.95 | 1.00 | | | 1.00 | 1.00 |
| Satd. Flow (prot) | | 1722 | | | | | 1770 | 3539 | | | 3539 | 1583 |
| Flt Permitted | | 0.97 | | | | | 0.95 | 1.00 | | | 1.00 | 1.00 |
| Satd. Flow (perm) | | 1722 | | | | | 1770 | 3539 | | | 3539 | 1583 |
| Peak-hour factor, PHF | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Adj. Flow (vph) | 335 | 0 | 166 | 0 | 0 | 0 | 84 | 503 | 0 | 0 | 584 | 260 |
| RTOR Reduction (vph) | 0 | 43 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 179 |
| Lane Group Flow (vph) | 0 | 458 | 0 | 0 | 0 | 0 | 84 | 503 | 0 | 0 | 584 | 81 |
| Turn Type | Perm | NA | | | | | Prot | NA | | Prot | NA | Perm |
| Protected Phases | | 4 | | | | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | | | | | | | | | | 6 |
| Actuated Green, G (s) | | 30.5 | | | | | 7.0 | 36.9 | | | 24.9 | 24.9 |
| Effective Green, g (s) | | 30.5 | | | | | 7.0 | 36.9 | | | 24.9 | 24.9 |
| Actuated g/C Ratio | | 0.38 | | | | | 0.09 | 0.46 | | | 0.31 | 0.31 |
| Clearance Time (s) | | 6.0 | | | | | 5.0 | 7.0 | | | 7.0 | 7.0 |
| Vehicle Extension (s) | | 2.0 | | | | | 2.0 | 5.0 | | | 5.0 | 5.0 |
| Lane Grp Cap (vph) | | 653 | | | | | 154 | 1624 | | | 1096 | 490 |
| v/s Ratio Prot | | | | | | | c0.05 | 0.14 | | | c0.17 | |
| v/s Ratio Perm | | 0.27 | | | | | | | | | | 0.05 |
| v/c Ratio | | 0.70 | | | | | 0.55 | 0.31 | | | 0.53 | 0.16 |
| Uniform Delay, d1 | | 21.1 | | | | | 35.2 | 13.7 | | | 22.9 | 20.2 |
| Progression Factor | | 1.00 | | | | | 1.00 | 1.00 | | | 1.00 | 1.00 |
| Incremental Delay, d2 | | 2.8 | | | | | 2.1 | 0.2 | | | 0.9 | 0.3 |
| Delay (s) | | 23.9 | | | | | 37.3 | 13.9 | | | 23.9 | 20.5 |
| Level of Service | | C | | | 0.0 | | D | B | | | C | С |
| Approach Delay (s) | | 23.9 | | | 0.0 | | | 17.3 | | | 22.8 | |
| Approach LOS | | С | | | Α | | | В | | | С | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 21.4 | H | CM 2000 | Level of S | Service | | С | | | |
| HCM 2000 Volume to Capaci | ty ratio | | 0.62 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 80.4 | | um of lost | | | | 18.0 | | | |
| Intersection Capacity Utilization | on | | 63.7% | IC | CU Level of | of Service | | | В | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

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|-----------------------------------|---------|----------|-------|------|-------------|------------|---------|-------|-------------|-------------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | 7 | | 4 | | ሻ | f) | | ሻ | † | 7 |
| Volume (vph) | 32 | 19 | 4 | 68 | 7 | 26 | 6 | 586 | 41 | 98 | 651 | 7 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 6.5 | 6.5 | | 6.0 | | 4.0 | 6.0 | | 4.0 | 6.0 | 6.0 |
| Lane Util. Factor | | 1.00 | 1.00 | | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Frpb, ped/bikes | | 1.00 | 0.98 | | 0.99 | | 1.00 | 1.00 | | 1.00 | 1.00 | 0.98 |
| Flpb, ped/bikes | | 1.00 | 1.00 | | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Frt | | 1.00 | 0.85 | | 0.96 | | 1.00 | 0.99 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | | 0.97 | 1.00 | | 0.97 | | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | | 1805 | 1546 | | 1718 | | 1769 | 1844 | | 1770 | 1863 | 1549 |
| Flt Permitted | | 0.79 | 1.00 | | 0.76 | | 0.30 | 1.00 | | 0.24 | 1.00 | 1.00 |
| Satd. Flow (perm) | | 1467 | 1546 | | 1355 | | 563 | 1844 | | 439 | 1863 | 1549 |
| Peak-hour factor, PHF | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |
| Adj. Flow (vph) | 36 | 22 | 5 | 77 | 8 | 30 | 7 | 666 | 47 | 111 | 740 | 8 |
| RTOR Reduction (vph) | 0 | 0 | 4 | 0 | 11 | 0 | 0 | 2 | 0 | 0 | 0 | 3 |
| Lane Group Flow (vph) | 0 | 58 | 1 | 0 | 104 | 0 | 7 | 711 | 0 | 111 | 740 | 5 |
| Confl. Peds. (#/hr) | 1 | | 1 | 1 | | 1 | 1 | | | | | 1 |
| Confl. Bikes (#/hr) | | | | | | 8 | | | | | | |
| Turn Type | Perm | NA | Perm | Perm | NA | | pm+pt | NA | | pm+pt | NA | Perm |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | | 2 | | | 6 | | 6 |
| Actuated Green, G (s) | | 11.1 | 11.1 | | 11.6 | | 44.9 | 44.2 | | 53.2 | 48.5 | 48.5 |
| Effective Green, g (s) | | 11.1 | 11.1 | | 11.6 | | 44.9 | 44.2 | | 53.2 | 48.5 | 48.5 |
| Actuated g/C Ratio | | 0.14 | 0.14 | | 0.15 | | 0.58 | 0.58 | | 0.69 | 0.63 | 0.63 |
| Clearance Time (s) | | 6.5 | 6.5 | | 6.0 | | 4.0 | 6.0 | | 4.0 | 6.0 | 6.0 |
| Vehicle Extension (s) | | 2.0 | 2.0 | | 2.0 | | 2.0 | 5.0 | | 2.0 | 5.0 | 5.0 |
| Lane Grp Cap (vph) | | 212 | 223 | | 204 | | 340 | 1061 | | 390 | 1176 | 978 |
| v/s Ratio Prot | | | | | | | 0.00 | c0.39 | | c0.02 | c0.40 | |
| v/s Ratio Perm | | 0.04 | 0.00 | | c0.08 | | 0.01 | | | 0.18 | | 0.00 |
| v/c Ratio | | 0.27 | 0.00 | | 0.51 | | 0.02 | 0.67 | | 0.28 | 0.63 | 0.01 |
| Uniform Delay, d1 | | 29.3 | 28.1 | | 30.0 | | 7.2 | 11.3 | | 6.8 | 8.7 | 5.2 |
| Progression Factor | | 1.00 | 1.00 | | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | | 0.3 | 0.0 | | 0.7 | | 0.0 | 2.2 | | 0.1 | 1.5 | 0.0 |
| Delay (s) | | 29.5 | 28.1 | | 30.7 | | 7.2 | 13.5 | | 6.9 | 10.2 | 5.2 |
| Level of Service | | С | С | | С | | Α | В | | Α | В | Α |
| Approach Delay (s) | | 29.4 | | | 30.7 | | | 13.4 | | | 9.7 | |
| Approach LOS | | С | | | С | | | В | | | Α | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 13.3 | Н | CM 2000 | Level of | Service | | В | | | |
| HCM 2000 Volume to Capacit | y ratio | | 0.62 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 76.8 | | um of lost | . , | | | 16.5 | | | |
| Intersection Capacity Utilization | n | | 64.7% | IC | CU Level of | of Service |) | | С | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

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|--------------------------------|------|----------|----------|------|------------|------------|
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations | | 4 | f) | | W | |
| Volume (veh/h) | 29 | 138 | 50 | 53 | 135 | 56 |
| Sign Control | | Free | Free | | Stop | |
| Grade | | 0% | 0% | | 0% | |
| Peak Hour Factor | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 |
| Hourly flow rate (vph) | 35 | 168 | 61 | 65 | 165 | 68 |
| Pedestrians | | | | | | |
| Lane Width (ft) | | | | | | |
| Walking Speed (ft/s) | | | | | | |
| Percent Blockage | | | | | | |
| Right turn flare (veh) | | | | | | |
| Median type | | None | None | | | |
| Median storage veh) | | | | | | |
| Upstream signal (ft) | | | | | | |
| pX, platoon unblocked | | | | | | |
| vC, conflicting volume | 126 | | | | 332 | 93 |
| vC1, stage 1 conf vol | 120 | | | | 002 | 70 |
| vC2, stage 2 conf vol | | | | | | |
| vCu, unblocked vol | 126 | | | | 332 | 93 |
| tC, single (s) | 4.1 | | | | 6.4 | 6.2 |
| tC, 2 stage (s) | | | | | 0.1 | 0.2 |
| tF (s) | 2.2 | | | | 3.5 | 3.3 |
| p0 queue free % | 98 | | | | 75 | 93 |
| cM capacity (veh/h) | 1461 | | | | 647 | 964 |
| | | | | | 017 | 701 |
| Direction, Lane # | EB 1 | WB 1 | SB 1 | | | |
| Volume Total | 204 | 126 | 233 | | | |
| Volume Left | 35 | 0 | 165 | | | |
| Volume Right | 0 | 65 | 68 | | | |
| cSH | 1461 | 1700 | 716 | | | |
| Volume to Capacity | 0.02 | 0.07 | 0.33 | | | |
| Queue Length 95th (ft) | 2 | 0 | 35 | | | |
| Control Delay (s) | 1.5 | 0.0 | 12.4 | | | |
| Lane LOS | Α | | В | | | |
| Approach Delay (s) | 1.5 | 0.0 | 12.4 | | | |
| Approach LOS | | | В | | | |
| Intersection Summary | | | | | | |
| Average Delay | | | 5.7 | | | |
| Intersection Capacity Utilizat | ion | | 33.1% | IC | CU Level c | of Service |
| Analysis Period (min) | | | 15 | | | |
| | | | | | | |

| | ۶ | • | • | † | | 4 | |
|-------------------------------|-------------|------|-------|------------|------------|-----------------|---|
| Movement | EBL | EBR | NBL | NBT | SBT | SBR | |
| Lane Configurations | ¥ | | ħ | † † | † † | 7 | |
| Volume (vph) | 261 | 39 | 18 | 301 | 565 | 152 | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | |
| Total Lost time (s) | 6.8 | | 5.0 | 6.3 | 6.3 | 6.3 | |
| Lane Util. Factor | 1.00 | | 1.00 | 0.95 | 0.95 | 1.00 | |
| Frt | 0.98 | | 1.00 | 1.00 | 1.00 | 0.85 | |
| Flt Protected | 0.96 | | 0.95 | 1.00 | 1.00 | 1.00 | |
| Satd. Flow (prot) | 1754 | | 1770 | 3539 | 3539 | 1583 | |
| Flt Permitted | 0.96 | | 0.95 | 1.00 | 1.00 | 1.00 | |
| Satd. Flow (perm) | 1754 | | 1770 | 3539 | 3539 | 1583 | |
| Peak-hour factor, PHF | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | |
| Adj. Flow (vph) | 290 | 43 | 20 | 334 | 628 | 169 | |
| RTOR Reduction (vph) | 4 | 0 | 0 | 0 | 0 | 105 | |
| Lane Group Flow (vph) | 329 | 0 | 20 | 334 | 628 | 64 | |
| Turn Type | NA | | Prot | NA | NA | Perm | |
| Protected Phases | 4 | | 5 | 2 | 6 | | |
| Permitted Phases | | | | | | 6 | |
| Actuated Green, G (s) | 17.0 | | 2.0 | 29.5 | 22.5 | 22.5 | |
| Effective Green, g (s) | 17.0 | | 2.0 | 29.5 | 22.5 | 22.5 | |
| Actuated g/C Ratio | 0.29 | | 0.03 | 0.49 | 0.38 | 0.38 | |
| Clearance Time (s) | 6.8 | | 5.0 | 6.3 | 6.3 | 6.3 | |
| Vehicle Extension (s) | 2.0 | | 2.0 | 3.0 | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 500 | | 59 | 1751 | 1336 | 597 | |
| v/s Ratio Prot | c0.19 | | 0.01 | c0.09 | c0.18 | | |
| v/s Ratio Perm | | | | | | 0.04 | |
| v/c Ratio | 0.66 | | 0.34 | 0.19 | 0.47 | 0.11 | |
| Uniform Delay, d1 | 18.7 | | 28.2 | 8.4 | 14.0 | 12.0 | |
| Progression Factor | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d2 | 2.4 | | 1.2 | 0.1 | 0.3 | 0.1 | |
| Delay (s) | 21.1 | | 29.4 | 8.4 | 14.3 | 12.1 | |
| Level of Service | С | | С | Α | В | В | |
| Approach Delay (s) | 21.1 | | | 9.6 | 13.8 | | |
| Approach LOS | С | | | Α | В | | |
| Intersection Summary | | | | | | | |
| HCM 2000 Control Delay | _ | | 14.5 | Н | CM 2000 | Level of Servic | 9 |
| HCM 2000 Volume to Capa | icity ratio | | 0.55 | | | | |
| Actuated Cycle Length (s) | | | 59.6 | S | um of lost | t time (s) | |
| Intersection Capacity Utiliza | ation | | 44.4% | | | of Service | |
| Analysis Period (min) | | | 15 | | | | |
| c Critical Lane Group | | | | | | | |

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|-----------------------------------|----------|----------|-------|-------|-------------|------------|---------|----------|-------------|----------|------------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | 7 | Ť | र्स | 7 | ሻ | ^ | 7 | ř | † † | 7 |
| Volume (vph) | 2 | 4 | 2 | 602 | 1 | 2 | 6 | 602 | 356 | 7 | 668 | 1 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 5.0 | 5.0 | 5.0 | 5.0 | 4.0 | 4.0 | 5.0 | 4.0 | 4.0 | 5.0 | 5.0 |
| Lane Util. Factor | | 1.00 | 1.00 | 0.95 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frt | | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | | 0.98 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | | 1832 | 1583 | 1681 | 1686 | 1583 | 1770 | 3539 | 1583 | 1770 | 3539 | 1583 |
| Flt Permitted | | 0.98 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | | 1832 | 1583 | 1681 | 1686 | 1583 | 1770 | 3539 | 1583 | 1770 | 3539 | 1583 |
| Peak-hour factor, PHF | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Adj. Flow (vph) | 2 | 4 | 2 | 627 | 1 | 2 | 6 | 627 | 371 | 7 | 696 | 1 |
| RTOR Reduction (vph) | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| Lane Group Flow (vph) | 0 | 6 | 0 | 313 | 315 | 2 | 6 | 627 | 371 | 7 | 696 | 0 |
| Turn Type | Split | NA | Perm | Split | NA | Free | Prot | NA | Free | Prot | NA | Perm |
| Protected Phases | 4 | 4 | | 3 | 3 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | | | 4 | | | Free | | | Free | | | 6 |
| Actuated Green, G (s) | | 0.8 | 8.0 | 20.8 | 20.8 | 65.8 | 0.7 | 24.5 | 65.8 | 0.7 | 24.5 | 24.5 |
| Effective Green, g (s) | | 0.8 | 8.0 | 20.8 | 20.8 | 65.8 | 0.7 | 24.5 | 65.8 | 0.7 | 24.5 | 24.5 |
| Actuated g/C Ratio | | 0.01 | 0.01 | 0.32 | 0.32 | 1.00 | 0.01 | 0.37 | 1.00 | 0.01 | 0.37 | 0.37 |
| Clearance Time (s) | | 5.0 | 5.0 | 5.0 | 5.0 | | 4.0 | 5.0 | | 4.0 | 5.0 | 5.0 |
| Vehicle Extension (s) | | 3.0 | 3.0 | 3.0 | 3.0 | | 2.0 | 4.0 | | 2.0 | 4.0 | 4.0 |
| Lane Grp Cap (vph) | | 22 | 19 | 531 | 532 | 1583 | 18 | 1317 | 1583 | 18 | 1317 | 589 |
| v/s Ratio Prot | | 0.00 | | 0.19 | c0.19 | | 0.00 | 0.18 | | 0.00 | c0.20 | |
| v/s Ratio Perm | | | 0.00 | | | 0.00 | | | c0.23 | | | 0.00 |
| v/c Ratio | | 0.27 | 0.00 | 0.59 | 0.59 | 0.00 | 0.33 | 0.48 | 0.23 | 0.39 | 0.53 | 0.00 |
| Uniform Delay, d1 | | 32.2 | 32.1 | 18.9 | 18.9 | 0.0 | 32.3 | 15.8 | 0.0 | 32.3 | 16.1 | 13.0 |
| Progression Factor | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | | 6.6 | 0.0 | 1.7 | 1.8 | 0.0 | 3.9 | 0.4 | 0.3 | 5.0 | 0.5 | 0.0 |
| Delay (s) | | 38.8 | 32.1 | 20.6 | 20.7 | 0.0 | 36.3 | 16.1 | 0.3 | 37.3 | 16.6 | 13.0 |
| Level of Service | | D | С | С | С | Α | D | В | Α | D | В | В |
| Approach Delay (s) | | 37.2 | | | 20.6 | | | 10.4 | | | 16.8 | |
| Approach LOS | | D | | | С | | | В | | | В | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 15.2 | Н | CM 2000 | Level of S | Service | | В | | | |
| HCM 2000 Volume to Capaci | ty ratio | | 0.59 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 65.8 | | um of lost | | | | 19.0 | | | |
| Intersection Capacity Utilization | on | | 51.8% | IC | CU Level of | of Service | | | Α | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

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|---------------------------------|-----------|----------|-------|------|------------|------------|---------|----------|------|-------------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | र्स | 7 | | 4 | 7 | ሻ | † | 7 | 75 | † | 7 |
| Volume (vph) | 19 | 76 | 24 | 271 | 124 | 165 | 41 | 394 | 259 | 143 | 377 | 35 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 5.0 | 5.0 | | 5.0 | 5.0 | 4.0 | 5.0 | 5.0 | 4.0 | 5.0 | 5.0 |
| Lane Util. Factor | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frpb, ped/bikes | | 1.00 | 1.00 | | 1.00 | 0.97 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Flpb, ped/bikes | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | | 1.00 | 0.85 | | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | | 0.99 | 1.00 | | 0.97 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | | 1843 | 1583 | | 1801 | 1532 | 1770 | 1863 | 1583 | 1770 | 1863 | 1583 |
| Flt Permitted | | 0.90 | 1.00 | | 0.73 | 1.00 | 0.47 | 1.00 | 1.00 | 0.29 | 1.00 | 1.00 |
| Satd. Flow (perm) | | 1666 | 1583 | | 1364 | 1532 | 870 | 1863 | 1583 | 540 | 1863 | 1583 |
| Peak-hour factor, PHF | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Adj. Flow (vph) | 20 | 82 | 26 | 291 | 133 | 177 | 44 | 424 | 278 | 154 | 405 | 38 |
| RTOR Reduction (vph) | 0 | 0 | 17 | 0 | 0 | 97 | 0 | 0 | 175 | 0 | 0 | 21 |
| Lane Group Flow (vph) | 0 | 102 | 9 | 0 | 424 | 80 | 44 | 424 | 103 | 154 | 405 | 17 |
| Confl. Peds. (#/hr) | 6 | | | | | 6 | | | | | | |
| Turn Type | Perm | NA | Perm | Perm | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | 8 | 2 | | 2 | 6 | | 6 |
| Actuated Green, G (s) | | 31.1 | 31.1 | | 31.1 | 31.1 | 35.1 | 31.8 | 31.8 | 44.7 | 37.4 | 37.4 |
| Effective Green, g (s) | | 31.1 | 31.1 | | 31.1 | 31.1 | 35.1 | 31.8 | 31.8 | 44.7 | 37.4 | 37.4 |
| Actuated g/C Ratio | | 0.36 | 0.36 | | 0.36 | 0.36 | 0.41 | 0.37 | 0.37 | 0.52 | 0.44 | 0.44 |
| Clearance Time (s) | | 5.0 | 5.0 | | 5.0 | 5.0 | 4.0 | 5.0 | 5.0 | 4.0 | 5.0 | 5.0 |
| Vehicle Extension (s) | | 2.5 | 2.5 | | 2.5 | 2.5 | 2.0 | 5.0 | 5.0 | 2.0 | 5.0 | 5.0 |
| Lane Grp Cap (vph) | | 603 | 573 | | 494 | 555 | 390 | 690 | 586 | 408 | 812 | 690 |
| v/s Ratio Prot | | | | | | | 0.00 | c0.23 | | c0.04 | 0.22 | |
| v/s Ratio Perm | | 0.06 | 0.01 | | c0.31 | 0.05 | 0.04 | | 0.07 | 0.16 | | 0.01 |
| v/c Ratio | | 0.17 | 0.02 | | 0.86 | 0.14 | 0.11 | 0.61 | 0.18 | 0.38 | 0.50 | 0.02 |
| Uniform Delay, d1 | | 18.6 | 17.5 | | 25.3 | 18.4 | 15.4 | 22.0 | 18.2 | 12.5 | 17.4 | 13.8 |
| Progression Factor | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | | 0.1 | 0.0 | | 13.6 | 0.1 | 0.0 | 2.3 | 0.3 | 0.2 | 1.0 | 0.0 |
| Delay (s) | | 18.7 | 17.5 | | 38.9 | 18.5 | 15.5 | 24.4 | 18.5 | 12.7 | 18.5 | 13.8 |
| Level of Service | | В | В | | D | В | В | С | В | В | В | В |
| Approach Delay (s) | | 18.4 | | | 32.9 | | | 21.6 | | | 16.7 | |
| Approach LOS | | В | | | С | | | С | | | В | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 23.3 | H | CM 2000 | Level of | Service | | С | | | |
| HCM 2000 Volume to Capac | ity ratio | | 0.69 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 85.8 | | um of lost | | | | 14.0 | | | |
| Intersection Capacity Utilizati | on | | 68.5% | IC | U Level | of Service | 9 | | С | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| | | | | | | | | | - | | | |

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|-------------------------------|-------------|----------|-------|-------|-----------|------------|---------|------|------|-------------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ň | f) | | Ŋ | † | 7 | 7 | f) | | ň | 4î | |
| Volume (vph) | 231 | 169 | 36 | 55 | 239 | 273 | 25 | 109 | 45 | 252 | 161 | 254 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 5.0 | 5.0 | | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | | 5.0 | 5.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 0.99 | | 1.00 | 0.98 | |
| Flpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frt | 1.00 | 0.97 | | 1.00 | 1.00 | 0.85 | 1.00 | 0.96 | | 1.00 | 0.91 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 1806 | | 1765 | 1863 | 1583 | 1767 | 1770 | | 1769 | 1664 | |
| Flt Permitted | 0.35 | 1.00 | | 0.63 | 1.00 | 1.00 | 0.43 | 1.00 | | 0.49 | 1.00 | |
| Satd. Flow (perm) | 649 | 1806 | | 1163 | 1863 | 1583 | 806 | 1770 | | 907 | 1664 | |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 238 | 174 | 37 | 57 | 246 | 281 | 26 | 112 | 46 | 260 | 166 | 262 |
| RTOR Reduction (vph) | 0 | 5 | 0 | 0 | 0 | 216 | 0 | 12 | 0 | 0 | 39 | 0 |
| Lane Group Flow (vph) | 238 | 206 | 0 | 57 | 246 | 65 | 26 | 146 | 0 | 260 | 389 | 0 |
| Confl. Peds. (#/hr) | | | 3 | 3 | | | 3 | | 1 | 1 | | 3 |
| Turn Type | pm+pt | NA | | pm+pt | NA | Perm | pm+pt | NA | | pm+pt | NA | |
| Protected Phases | 7 | 4 | | 3 | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | | 8 | | 8 | 2 | | | 6 | | |
| Actuated Green, G (s) | 40.8 | 30.9 | | 25.1 | 20.2 | 20.2 | 22.2 | 20.2 | | 37.1 | 30.1 | |
| Effective Green, g (s) | 40.8 | 30.9 | | 25.1 | 20.2 | 20.2 | 22.2 | 20.2 | | 37.1 | 30.1 | |
| Actuated g/C Ratio | 0.46 | 0.35 | | 0.29 | 0.23 | 0.23 | 0.25 | 0.23 | | 0.42 | 0.34 | |
| Clearance Time (s) | 5.0 | 5.0 | | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | | 5.0 | 5.0 | |
| Vehicle Extension (s) | 2.0 | 3.0 | | 2.0 | 3.0 | 3.0 | 2.0 | 3.0 | | 2.0 | 3.0 | |
| Lane Grp Cap (vph) | 500 | 634 | | 365 | 428 | 363 | 225 | 406 | | 499 | 569 | |
| v/s Ratio Prot | c0.08 | 0.11 | | 0.01 | c0.13 | | 0.00 | 0.08 | | c0.07 | c0.23 | |
| v/s Ratio Perm | 0.14 | | | 0.04 | | 0.04 | 0.03 | | | 0.15 | | |
| v/c Ratio | 0.48 | 0.32 | | 0.16 | 0.57 | 0.18 | 0.12 | 0.36 | | 0.52 | 0.68 | |
| Uniform Delay, d1 | 15.4 | 20.9 | | 23.2 | 30.0 | 27.2 | 25.0 | 28.4 | | 17.5 | 24.8 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.3 | 0.3 | | 0.1 | 1.9 | 0.2 | 0.1 | 0.5 | | 0.5 | 3.4 | |
| Delay (s) | 15.7 | 21.2 | | 23.3 | 31.9 | 27.4 | 25.1 | 29.0 | | 18.0 | 28.2 | |
| Level of Service | В | С | | С | С | С | С | С | | В | С | |
| Approach Delay (s) | | 18.3 | | | 28.9 | | | 28.4 | | | 24.3 | |
| Approach LOS | | В | | | С | | | С | | | С | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 24.7 | Н | CM 2000 | Level of | Service | | С | | | |
| HCM 2000 Volume to Capa | acity ratio | | 0.62 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 87.9 | S | um of los | t time (s) | | | 20.0 | | | |
| Intersection Capacity Utiliza | ation | | 69.6% | IC | CU Level | of Service | 9 | | С | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lana Croup | | | | | | | | | | | | |

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|-----------------------------------|------|----------|-------|-------|-------------|------------|------|----------|----------|----------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | | | 4 | | ሻ | ₽ | | 7 | ₽ | |
| Sign Control | | Stop | | | Stop | | | Stop | | | Stop | |
| Volume (vph) | 234 | 195 | 52 | 29 | 240 | 211 | 43 | 78 | 40 | 122 | 76 | 273 |
| Peak Hour Factor | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Hourly flow rate (vph) | 239 | 199 | 53 | 30 | 245 | 215 | 44 | 80 | 41 | 124 | 78 | 279 |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | NB 2 | SB 1 | SB 2 | | | | | | |
| Volume Total (vph) | 491 | 490 | 44 | 120 | 124 | 356 | | | | | | |
| Volume Left (vph) | 239 | 30 | 44 | 0 | 124 | 0 | | | | | | |
| Volume Right (vph) | 53 | 215 | 0 | 41 | 0 | 279 | | | | | | |
| Hadj (s) | 0.07 | -0.22 | 0.53 | -0.20 | 0.53 | -0.51 | | | | | | |
| Departure Headway (s) | 7.7 | 7.3 | 9.8 | 9.1 | 8.9 | 7.8 | | | | | | |
| Degree Utilization, x | 1.05 | 0.99 | 0.12 | 0.30 | 0.31 | 0.78 | | | | | | |
| Capacity (veh/h) | 463 | 490 | 356 | 385 | 397 | 451 | | | | | | |
| Control Delay (s) | 83.0 | 65.8 | 13.0 | 14.8 | 14.6 | 31.8 | | | | | | |
| Approach Delay (s) | 83.0 | 65.8 | 14.3 | | 27.3 | | | | | | | |
| Approach LOS | F | F | В | | D | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Delay | | | 54.4 | | | | | | | | | |
| Level of Service | | | F | | | | | | | | | |
| Intersection Capacity Utilization | n | | 91.2% | IC | CU Level of | of Service | | | F | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
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|-----------------------------------|---------|----------|-------|------|------------|------------|---------|------------|-------------|----------|------------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | | | | | ሻ | ∱ Љ | | ሻ | † † | 7 |
| Volume (vph) | 267 | 0 | 72 | 0 | 0 | 0 | 180 | 550 | 0 | 1 | 546 | 395 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 6.0 | | | | | 5.0 | 7.0 | | 5.0 | 7.0 | 7.0 |
| Lane Util. Factor | | 1.00 | | | | | 1.00 | 0.95 | | 1.00 | 0.95 | 1.00 |
| Frpb, ped/bikes | | 1.00 | | | | | 1.00 | 1.00 | | 1.00 | 1.00 | 0.98 |
| Flpb, ped/bikes | | 1.00 | | | | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Frt | | 0.97 | | | | | 1.00 | 1.00 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | | 0.96 | | | | | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | | 1741 | | | | | 1770 | 3539 | | 1770 | 3539 | 1550 |
| Flt Permitted | | 0.96 | | | | | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | | 1741 | | | | | 1770 | 3539 | | 1770 | 3539 | 1550 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 290 | 0 | 78 | 0 | 0 | 0 | 196 | 598 | 0 | 1 | 593 | 429 |
| RTOR Reduction (vph) | 0 | 53 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 264 |
| Lane Group Flow (vph) | 0 | 315 | 0 | 0 | 0 | 0 | 196 | 598 | 0 | 1 | 593 | 165 |
| Confl. Peds. (#/hr) | | | | | | | | | | | | 1 |
| Turn Type | Perm | NA | | | | | Prot | NA | | Prot | NA | Perm |
| Protected Phases | | 4 | | | | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | | | | | | | | | | 6 |
| Actuated Green, G (s) | | 21.2 | | | | | 14.3 | 47.0 | | 0.7 | 33.4 | 33.4 |
| Effective Green, g (s) | | 21.2 | | | | | 14.3 | 47.0 | | 0.7 | 33.4 | 33.4 |
| Actuated g/C Ratio | | 0.24 | | | | | 0.16 | 0.54 | | 0.01 | 0.38 | 0.38 |
| Clearance Time (s) | | 6.0 | | | | | 5.0 | 7.0 | | 5.0 | 7.0 | 7.0 |
| Vehicle Extension (s) | | 2.0 | | | | | 2.0 | 5.0 | | 2.0 | 5.0 | 5.0 |
| Lane Grp Cap (vph) | | 424 | | | | | 291 | 1914 | | 14 | 1360 | 595 |
| v/s Ratio Prot | | | | | | | c0.11 | 0.17 | | 0.00 | c0.17 | |
| v/s Ratio Perm | | 0.18 | | | | | | | | | | 0.11 |
| v/c Ratio | | 0.74 | | | | | 0.67 | 0.31 | | 0.07 | 0.44 | 0.28 |
| Uniform Delay, d1 | | 30.3 | | | | | 34.1 | 11.0 | | 42.8 | 19.8 | 18.4 |
| Progression Factor | | 1.00 | | | | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | | 6.1 | | | | | 4.8 | 0.2 | | 0.8 | 0.5 | 0.5 |
| Delay (s) | | 36.4 | | | | | 38.9 | 11.2 | | 43.6 | 20.3 | 19.0 |
| Level of Service | | D | | | | | D | В | | D | С | В |
| Approach Delay (s) | | 36.4 | | | 0.0 | | | 18.0 | | | 19.7 | |
| Approach LOS | | D | | | Α | | | В | | | В | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 21.9 | H | CM 2000 | Level of S | Service | | С | | | |
| HCM 2000 Volume to Capacit | y ratio | | 0.58 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 86.9 | | um of lost | | | | 18.0 | | | |
| Intersection Capacity Utilization | n | | 60.8% | IC | U Level o | of Service | | | В | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

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|--------------------------------|-----------|----------|-------|------|-------------|------------|---------|-------|------|-------------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | र्स | 7 | | 4 | | ሻ | f) | | ሻ | † | 7 |
| Volume (vph) | 13 | 6 | 8 | 49 | 15 | 44 | 9 | 608 | 69 | 23 | 547 | 27 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 6.5 | 6.5 | | 6.0 | | 4.0 | 6.0 | | 4.0 | 6.0 | 6.0 |
| Lane Util. Factor | | 1.00 | 1.00 | | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Frpb, ped/bikes | | 1.00 | 1.00 | | 0.98 | | 1.00 | 1.00 | | 1.00 | 1.00 | 0.98 |
| Flpb, ped/bikes | | 1.00 | 1.00 | | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Frt | | 1.00 | 0.85 | | 0.94 | | 1.00 | 0.98 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | | 0.97 | 1.00 | | 0.98 | | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | | 1801 | 1583 | | 1692 | | 1769 | 1829 | | 1769 | 1863 | 1546 |
| Flt Permitted | | 0.81 | 1.00 | | 0.84 | | 0.37 | 1.00 | | 0.25 | 1.00 | 1.00 |
| Satd. Flow (perm) | | 1508 | 1583 | | 1461 | | 686 | 1829 | | 471 | 1863 | 1546 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 14 | 7 | 9 | 53 | 16 | 48 | 10 | 661 | 75 | 25 | 595 | 29 |
| RTOR Reduction (vph) | 0 | 0 | 8 | 0 | 21 | 0 | 0 | 3 | 0 | 0 | 0 | 11 |
| Lane Group Flow (vph) | 0 | 21 | 1 | 0 | 96 | 0 | 10 | 733 | 0 | 25 | 595 | 18 |
| Confl. Peds. (#/hr) | 1 | | | | | 1 | 2 | | 5 | 5 | | 2 |
| Confl. Bikes (#/hr) | | | | | | 8 | | | | | | |
| Turn Type | Perm | NA | Perm | Perm | NA | | pm+pt | NA | | pm+pt | NA | Perm |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | | 2 | | | 6 | | 6 |
| Actuated Green, G (s) | | 10.5 | 10.5 | | 11.0 | | 42.5 | 41.8 | | 44.3 | 42.7 | 42.7 |
| Effective Green, g (s) | | 10.5 | 10.5 | | 11.0 | | 42.5 | 41.8 | | 44.3 | 42.7 | 42.7 |
| Actuated g/C Ratio | | 0.15 | 0.15 | | 0.16 | | 0.60 | 0.59 | | 0.63 | 0.61 | 0.61 |
| Clearance Time (s) | | 6.5 | 6.5 | | 6.0 | | 4.0 | 6.0 | | 4.0 | 6.0 | 6.0 |
| Vehicle Extension (s) | | 2.0 | 2.0 | | 2.0 | | 2.0 | 5.0 | | 2.0 | 5.0 | 5.0 |
| Lane Grp Cap (vph) | | 224 | 236 | | 228 | | 424 | 1085 | | 325 | 1129 | 937 |
| v/s Ratio Prot | | | | | | | 0.00 | c0.40 | | c0.00 | 0.32 | |
| v/s Ratio Perm | | 0.01 | 0.00 | | c0.07 | | 0.01 | | | 0.05 | | 0.01 |
| v/c Ratio | | 0.09 | 0.01 | | 0.42 | | 0.02 | 0.68 | | 0.08 | 0.53 | 0.02 |
| Uniform Delay, d1 | | 25.8 | 25.5 | | 26.8 | | 5.9 | 9.7 | | 6.5 | 8.0 | 5.5 |
| Progression Factor | | 1.00 | 1.00 | | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | | 0.1 | 0.0 | | 0.5 | | 0.0 | 2.2 | | 0.0 | 0.8 | 0.0 |
| Delay (s) | | 25.9 | 25.5 | | 27.3 | | 5.9 | 11.9 | | 6.5 | 8.9 | 5.5 |
| Level of Service | | С | С | | С | | Α | В | | Α | Α | Α |
| Approach Delay (s) | | 25.8 | | | 27.3 | | | 11.8 | | | 8.6 | |
| Approach LOS | | С | | | С | | | В | | | А | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 11.9 | Н | CM 2000 | Level of | Service | | В | | | |
| HCM 2000 Volume to Capac | ity ratio | | 0.61 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 70.4 | | um of lost | | | | 16.5 | | | |
| Intersection Capacity Utilizat | ion | | 59.3% | IC | CU Level of | of Service | 9 | | В | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

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|-------------------------------|----------|----------|-----------|------|-----------|------------|--|
| Movement | EBL | EBT | WBT | WBR | SBL | SBR | |
| Lane Configurations | | 4 | 4î | | ¥ | | |
| Volume (veh/h) | 43 | 45 | 69 | 103 | 72 | 43 | |
| Sign Control | | Free | Free | | Stop | | |
| Grade | | 0% | 0% | | 0% | | |
| Peak Hour Factor | 0.85 | 0.85 | 0.85 | 0.85 | 0.85 | 0.85 | |
| Hourly flow rate (vph) | 51 | 53 | 81 | 121 | 85 | 51 | |
| Pedestrians | | | | | 1 | | |
| Lane Width (ft) | | | | | 12.0 | | |
| Walking Speed (ft/s) | | | | | 4.0 | | |
| Percent Blockage | | | | | 0 | | |
| Right turn flare (veh) | | | | | | | |
| Median type | | None | None | | | | |
| Median storage veh) | | | | | | | |
| Upstream signal (ft) | | | | | | | |
| pX, platoon unblocked | | | | | | | |
| vC, conflicting volume | 203 | | | | 297 | 143 | |
| vC1, stage 1 conf vol | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | |
| vCu, unblocked vol | 203 | | | | 297 | 143 | |
| tC, single (s) | 4.1 | | | | 6.4 | 6.2 | |
| tC, 2 stage (s) | | | | | | | |
| tF (s) | 2.2 | | | | 3.5 | 3.3 | |
| p0 queue free % | 96 | | | | 87 | 94 | |
| cM capacity (veh/h) | 1367 | | | | 668 | 904 | |
| Direction, Lane # | EB 1 | WB 1 | SB 1 | | | | |
| Volume Total | 104 | 202 | 135 | | | | |
| Volume Left | 51 | 0 | 85 | | | | |
| Volume Right | 0 | 121 | 51 | | | | |
| cSH | 1367 | 1700 | 740 | | | | |
| Volume to Capacity | 0.04 | 0.12 | 0.18 | | | | |
| Queue Length 95th (ft) | 3 | 0.12 | 17 | | | | |
| Control Delay (s) | 3.9 | 0.0 | 10.9 | | | | |
| Lane LOS | 3.9 A | 0.0 | 10.9 B | | | | |
| Approach Delay (s) | 3.9 | 0.0 | 10.9 | | | | |
| | 3.9 | 0.0 | | | | | |
| Approach LOS | | | В | | | | |
| Intersection Summary | | | | | | | |
| Average Delay | | | 4.3 | | | | |
| Intersection Capacity Utiliza | ition | | 31.5% | IC | U Level o | of Service | |
| Analysis Period (min) | | | 15 | | | | |
| | | | | | | | |

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|-------------------------------|------------|------|-------|----------|------------|--------------|------|
| Movement | EBL | EBR | NBL | NBT | SBT | SBR | |
| Lane Configurations | W | | ሻ | ^ | ^ | 7 | |
| Volume (vph) | 139 | 22 | 16 | 601 | 492 | 137 | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | |
| Total Lost time (s) | 6.8 | | 5.0 | 6.3 | 6.3 | 6.3 | |
| Lane Util. Factor | 1.00 | | 1.00 | 0.95 | 0.95 | 1.00 | |
| Frt | 0.98 | | 1.00 | 1.00 | 1.00 | 0.85 | |
| Flt Protected | 0.96 | | 0.95 | 1.00 | 1.00 | 1.00 | |
| Satd. Flow (prot) | 1753 | | 1770 | 3539 | 3539 | 1583 | |
| Flt Permitted | 0.96 | | 0.95 | 1.00 | 1.00 | 1.00 | |
| Satd. Flow (perm) | 1753 | | 1770 | 3539 | 3539 | 1583 | |
| Peak-hour factor, PHF | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | |
| Adj. Flow (vph) | 153 | 24 | 18 | 660 | 541 | 151 | |
| RTOR Reduction (vph) | 4 | 0 | 0 | 0 | 0 | 90 | |
| Lane Group Flow (vph) | 173 | 0 | 18 | 660 | 541 | 61 | |
| Turn Type | NA | | Prot | NA | NA | Perm | |
| Protected Phases | 4 | | 5 | 2 | 6 | | |
| Permitted Phases | | | | | | 6 | |
| Actuated Green, G (s) | 13.7 | | 0.9 | 27.8 | 21.9 | 21.9 | |
| Effective Green, g (s) | 13.7 | | 0.9 | 27.8 | 21.9 | 21.9 | |
| Actuated g/C Ratio | 0.25 | | 0.02 | 0.51 | 0.40 | 0.40 | |
| Clearance Time (s) | 6.8 | | 5.0 | 6.3 | 6.3 | 6.3 | |
| Vehicle Extension (s) | 2.0 | | 2.0 | 3.0 | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 439 | | 29 | 1801 | 1419 | 634 | |
| v/s Ratio Prot | c0.10 | | 0.01 | c0.19 | 0.15 | | |
| v/s Ratio Perm | | | | | | 0.04 | |
| v/c Ratio | 0.39 | | 0.62 | 0.37 | 0.38 | 0.10 | |
| Uniform Delay, d1 | 17.0 | | 26.7 | 8.1 | 11.6 | 10.2 | |
| Progression Factor | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.2 | | 26.1 | 0.1 | 0.2 | 0.1 | |
| Delay (s) | 17.2 | | 52.8 | 8.2 | 11.7 | 10.2 | |
| Level of Service | В | | D | Α | В | В | |
| Approach Delay (s) | 17.2 | | | 9.4 | 11.4 | | |
| Approach LOS | В | | | Α | В | | |
| Intersection Summary | | | | | | | |
| HCM 2000 Control Delay | | | 11.2 | H | CM 2000 | Level of Ser | vice |
| HCM 2000 Volume to Capa | city ratio | | 0.43 | | | | |
| Actuated Cycle Length (s) | | | 54.6 | | ım of lost | | |
| Intersection Capacity Utiliza | ation | | 36.6% | IC | U Level o | of Service | |
| Analysis Period (min) | | | 15 | | | | |
| c Critical Lane Group | | | | | | | |

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|-----------------------------------|-------|----------|-------|-------|-------------|------------|---------|------------|-------------|----------|------------|------|--|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | |
| Lane Configurations | | 4 | 7 | ř | 4 | 7 | ¥ | † † | 7 | ň | † † | 7 | |
| Volume (vph) | 2 | 3 | 6 | 502 | 3 | 4 | 3 | 644 | 610 | 4 | 578 | 3 | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | |
| Total Lost time (s) | | 5.0 | 5.0 | 5.0 | 5.0 | 4.0 | 4.0 | 5.0 | 4.0 | 4.0 | 5.0 | 5.0 | |
| Lane Util. Factor | | 1.00 | 1.00 | 0.95 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Frt | | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | |
| Flt Protected | | 0.98 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | |
| Satd. Flow (prot) | | 1826 | 1583 | 1681 | 1686 | 1583 | 1770 | 3539 | 1583 | 1770 | 3539 | 1583 | |
| Flt Permitted | | 0.98 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | |
| Satd. Flow (perm) | | 1826 | 1583 | 1681 | 1686 | 1583 | 1770 | 3539 | 1583 | 1770 | 3539 | 1583 | |
| Peak-hour factor, PHF | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | |
| Adj. Flow (vph) | 2 | 3 | 6 | 534 | 3 | 4 | 3 | 685 | 649 | 4 | 615 | 3 | |
| RTOR Reduction (vph) | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | |
| Lane Group Flow (vph) | 0 | 5 | 0 | 267 | 270 | 4 | 3 | 685 | 649 | 4 | 615 | 1 | |
| Turn Type | Split | NA | Perm | Split | NA | Free | Prot | NA | Free | Prot | NA | Perm | |
| Protected Phases | 4 | 4 | | 3 | 3 | | 5 | 2 | | 1 | 6 | | |
| Permitted Phases | | | 4 | | | Free | | | Free | | | 6 | |
| Actuated Green, G (s) | | 0.8 | 8.0 | 17.7 | 17.7 | 60.9 | 0.6 | 22.8 | 60.9 | 0.6 | 22.8 | 22.8 | |
| Effective Green, g (s) | | 0.8 | 8.0 | 17.7 | 17.7 | 60.9 | 0.6 | 22.8 | 60.9 | 0.6 | 22.8 | 22.8 | |
| Actuated g/C Ratio | | 0.01 | 0.01 | 0.29 | 0.29 | 1.00 | 0.01 | 0.37 | 1.00 | 0.01 | 0.37 | 0.37 | |
| Clearance Time (s) | | 5.0 | 5.0 | 5.0 | 5.0 | | 4.0 | 5.0 | | 4.0 | 5.0 | 5.0 | |
| Vehicle Extension (s) | | 3.0 | 3.0 | 3.0 | 3.0 | | 2.0 | 4.0 | | 2.0 | 4.0 | 4.0 | |
| Lane Grp Cap (vph) | | 23 | 20 | 488 | 490 | 1583 | 17 | 1324 | 1583 | 17 | 1324 | 592 | |
| v/s Ratio Prot | | 0.00 | | 0.16 | c0.16 | | 0.00 | c0.19 | | 0.00 | 0.17 | | |
| v/s Ratio Perm | | | 0.00 | | | 0.00 | | | c0.41 | | | 0.00 | |
| v/c Ratio | | 0.22 | 0.00 | 0.55 | 0.55 | 0.00 | 0.18 | 0.52 | 0.41 | 0.24 | 0.46 | 0.00 | |
| Uniform Delay, d1 | | 29.7 | 29.7 | 18.2 | 18.2 | 0.0 | 29.9 | 14.8 | 0.0 | 29.9 | 14.4 | 11.9 | |
| Progression Factor | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d2 | | 4.7 | 0.1 | 1.3 | 1.3 | 0.0 | 1.8 | 0.5 | 0.8 | 2.6 | 0.4 | 0.0 | |
| Delay (s) | | 34.5 | 29.7 | 19.5 | 19.6 | 0.0 | 31.7 | 15.2 | 0.8 | 32.5 | 14.8 | 11.9 | |
| Level of Service | | C | С | В | В | Α | С | В | A | С | B | В | |
| Approach Delay (s) | | 31.9 | | | 19.4 | | | 8.3 | | | 14.9 | | |
| Approach LOS | | С | | | В | | | A | | | В | | |
| Intersection Summary | | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 12.4 | Н | CM 2000 | Level of S | Service | | В | | | | |
| HCM 2000 Volume to Capacity ratio | | | 0.62 | | | | | | | | | | |
| Actuated Cycle Length (s) | | | 60.9 | | um of lost | | | | 19.0 | | | | |
| Intersection Capacity Utilization | on | | 46.8% | IC | CU Level of | of Service | | | Α | | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | | |

LOS Worksheets – Year 2022 without Project Conditions

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|-------------------------------|-------------|----------|--------------|------|------------|------------|-------|----------|------|----------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | र्स | 7 | | र्स | 7 | ¥ | † | 7 | ¥ | † | 7 |
| Volume (vph) | 30 | 170 | 70 | 290 | 80 | 280 | 30 | 480 | 380 | 440 | 490 | 10 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 5.0 | 5.0 | | 5.0 | 5.0 | 4.0 | 5.0 | 5.0 | 4.0 | 5.0 | 5.0 |
| Lane Util. Factor | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frpb, ped/bikes | | 1.00 | 0.98 | | 1.00 | 1.00 | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 1.00 |
| Flpb, ped/bikes | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | | 1.00 | 0.85 | | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | | 0.99 | 1.00 | | 0.96 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | | 1849 | 1550 | | 1790 | 1583 | 1770 | 1863 | 1547 | 1770 | 1863 | 1583 |
| Flt Permitted | | 0.82 | 1.00 | | 0.56 | 1.00 | 0.35 | 1.00 | 1.00 | 0.15 | 1.00 | 1.00 |
| Satd. Flow (perm) | | 1532 | 1550 | | 1039 | 1583 | 657 | 1863 | 1547 | 286 | 1863 | 1583 |
| Peak-hour factor, PHF | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Adj. Flow (vph) | 34 | 191 | 79 | 326 | 90 | 315 | 34 | 539 | 427 | 494 | 551 | 11 |
| RTOR Reduction (vph) | 0 | 0 | 50 | 0 | 0 | 174 | 0 | 0 | 265 | 0 | 0 | 6 |
| Lane Group Flow (vph) | 0 | 225 | 29 | 0 | 416 | 141 | 34 | 539 | 162 | 494 | 551 | 5 |
| Confl. Peds. (#/hr) | | | 1 | 1 | | | | | 1 | | | |
| Turn Type | Perm | NA | Perm | Perm | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | 8 | 2 | | 2 | 6 | | 6 |
| Actuated Green, G (s) | | 40.1 | 40.1 | | 40.1 | 40.1 | 42.2 | 38.7 | 38.7 | 57.7 | 50.2 | 50.2 |
| Effective Green, g (s) | | 40.1 | 40.1 | | 40.1 | 40.1 | 42.2 | 38.7 | 38.7 | 57.7 | 50.2 | 50.2 |
| Actuated g/C Ratio | | 0.37 | 0.37 | | 0.37 | 0.37 | 0.39 | 0.36 | 0.36 | 0.54 | 0.47 | 0.47 |
| Clearance Time (s) | | 5.0 | 5.0 | | 5.0 | 5.0 | 4.0 | 5.0 | 5.0 | 4.0 | 5.0 | 5.0 |
| Vehicle Extension (s) | | 2.5 | 2.5 | | 2.5 | 2.5 | 2.0 | 5.0 | 5.0 | 2.0 | 5.0 | 5.0 |
| Lane Grp Cap (vph) | | 569 | 576 | | 386 | 588 | 293 | 668 | 555 | 359 | 867 | 737 |
| v/s Ratio Prot | | | | | | | 0.00 | 0.29 | | c0.19 | 0.30 | |
| v/s Ratio Perm | | 0.15 | 0.02 | | c0.40 | 0.09 | 0.04 | | 0.10 | c0.54 | | 0.00 |
| v/c Ratio | | 0.40 | 0.05 | | 1.08 | 0.24 | 0.12 | 0.81 | 0.29 | 1.38 | 0.64 | 0.01 |
| Uniform Delay, d1 | | 24.9 | 21.7 | | 33.8 | 23.3 | 20.7 | 31.2 | 24.7 | 26.0 | 21.9 | 15.4 |
| Progression Factor | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | | 0.3 | 0.0 | | 68.2 | 0.2 | 0.1 | 8.0 | 0.6 | 185.9 | 2.1 | 0.0 |
| Delay (s) | | 25.3 | 21.7 | | 102.0 | 23.5 | 20.8 | 39.2 | 25.3 | 211.9 | 24.0 | 15.4 |
| Level of Service | | С | С | | F | С | С | D | С | F | С | В |
| Approach Delay (s) | | 24.3 | | | 68.2 | | | 32.7 | | | 111.8 | |
| Approach LOS | | С | | | Е | | | С | | | F | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 67.3 1.29 | | | | | | Е | | | |
| HCM 2000 Volume to Capa | acity ratio | | | | | | | | | | | |
| Actuated Cycle Length (s) | | | | | um of lost | | | | 14.0 | | | |
| Intersection Capacity Utiliza | ation | | 96.3% | IC | U Level | of Service | 9 | | F | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

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|-------------------------------|--------------------------------------|----------|------|-------|----------|----------|---------|-----------|----------|-------------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ሻ | ĥ | | ሻ | † | 7 | ሻ | ^} | | ሻ | ∱ | |
| Volume (vph) | 340 | 570 | 70 | 80 | 410 | 420 | 70 | 470 | 140 | 240 | 170 | 160 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 5.0 | 5.0 | | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | | 5.0 | 5.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | 0.97 | 1.00 | 0.99 | | 1.00 | 1.00 | |
| Flpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frt | 1.00 | 0.98 | | 1.00 | 1.00 | 0.85 | 1.00 | 0.97 | | 1.00 | 0.93 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 1828 | | 1770 | 1863 | 1539 | 1770 | 1786 | | 1770 | 1727 | |
| Flt Permitted | 0.14 | 1.00 | | 0.11 | 1.00 | 1.00 | 0.44 | 1.00 | | 0.09 | 1.00 | |
| Satd. Flow (perm) | 256 | 1828 | | 203 | 1863 | 1539 | 827 | 1786 | | 161 | 1727 | |
| Peak-hour factor, PHF | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Adj. Flow (vph) | 354 | 594 | 73 | 83 | 427 | 438 | 73 | 490 | 146 | 250 | 177 | 167 |
| RTOR Reduction (vph) | 0 | 2 | 0 | 0 | 0 | 166 | 0 | 8 | 0 | 0 | 22 | 0 |
| Lane Group Flow (vph) | 354 | 665 | 0 | 83 | 427 | 272 | 73 | 628 | 0 | 250 | 322 | 0 |
| Confl. Peds. (#/hr) | 3 | | 1 | 1 | | 3 | | | 4 | 4 | | |
| Turn Type | pm+pt | NA | | pm+pt | NA | Perm | pm+pt | NA | | pm+pt | NA | |
| Protected Phases | 7 | 4 | | 3 | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | | 8 | | 8 | 2 | | | 6 | | |
| Actuated Green, G (s) | 65.5 | 52.5 | | 44.7 | 36.7 | 36.7 | 47.2 | 41.3 | | 59.4 | 48.5 | |
| Effective Green, g (s) | 65.5 | 52.5 | | 44.7 | 36.7 | 36.7 | 47.2 | 41.3 | | 59.4 | 48.5 | |
| Actuated g/C Ratio | 0.49 | 0.39 | | 0.33 | 0.27 | 0.27 | 0.35 | 0.31 | | 0.44 | 0.36 | |
| Clearance Time (s) | 5.0 | 5.0 | | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | | 5.0 | 5.0 | |
| Vehicle Extension (s) | 2.0 | 3.0 | | 2.0 | 3.0 | 3.0 | 2.0 | 3.0 | | 2.0 | 3.0 | |
| Lane Grp Cap (vph) | 391 | 711 | | 160 | 506 | 418 | 330 | 546 | | 227 | 620 | |
| v/s Ratio Prot | c0.16 | c0.36 | | 0.03 | 0.23 | | 0.01 | 0.35 | | c0.11 | 0.19 | |
| v/s Ratio Perm | 0.28 | | | 0.14 | | 0.18 | 0.07 | | | c0.38 | | |
| v/c Ratio | 0.91 | 0.93 | | 0.52 | 0.84 | 0.65 | 0.22 | 1.15 | | 1.10 | 0.52 | |
| Uniform Delay, d1 | 35.1 | 39.6 | | 34.8 | 46.4 | 43.4 | 30.0 | 46.8 | | 40.4 | 34.0 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 23.3 | 19.4 | | 1.2 | 12.2 | 3.6 | 0.1 | 87.4 | | 89.5 | 0.7 | |
| Delay (s) | 58.4 | 58.9 | | 36.0 | 58.6 | 47.0 | 30.1 | 134.2 | | 129.9 | 34.7 | |
| Level of Service | Е | Е | | D | Е | D | С | F | | F | С | |
| Approach Delay (s) | | 58.7 | | | 51.3 | | | 123.5 | | | 74.8 | |
| Approach LOS | | E | | | D | | | F | | | Е | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 73.5 | H | CM 2000 | Level of | Service | | Е | | | |
| HCM 2000 Volume to Capa | acity ratio | | 1.06 | | | | | | | | | |
| Actuated Cycle Length (s) | | | | | | time (s) | | | 20.0 | | | |
| Intersection Capacity Utiliza | n Capacity Utilization 103.7% ICU Le | | | | | | 9 | | G | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

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|-------------------------------|-------|-------|--------|-------|----------|------------|------|----------|----------|----------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | | | 4 | | , | f) | | Ž | ĥ | |
| Sign Control | | Stop | | | Stop | | | Stop | | | Stop | |
| Volume (vph) | 130 | 340 | 170 | 70 | 420 | 210 | 220 | 560 | 80 | 100 | 470 | 170 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Hourly flow rate (vph) | 137 | 358 | 179 | 74 | 442 | 221 | 232 | 589 | 84 | 105 | 495 | 179 |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | NB 2 | SB 1 | SB 2 | | | | | | |
| Volume Total (vph) | 674 | 737 | 232 | 674 | 105 | 674 | | | | | | |
| Volume Left (vph) | 137 | 74 | 232 | 0 | 105 | 0 | | | | | | |
| Volume Right (vph) | 179 | 221 | 0 | 84 | 0 | 179 | | | | | | |
| Hadj (s) | -0.08 | -0.13 | 0.53 | -0.05 | 0.53 | -0.15 | | | | | | |
| Departure Headway (s) | 9.4 | 9.3 | 10.2 | 9.6 | 10.2 | 9.5 | | | | | | |
| Degree Utilization, x | 1.75 | 1.91 | 0.65 | 1.79 | 0.30 | 1.77 | | | | | | |
| Capacity (veh/h) | 389 | 391 | 347 | 381 | 351 | 384 | | | | | | |
| Control Delay (s) | 372.3 | 440.7 | 29.2 | 388.2 | 16.2 | 379.9 | | | | | | |
| Approach Delay (s) | 372.3 | 440.7 | 296.4 | | 330.7 | | | | | | | |
| Approach LOS | F | F | F | | F | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Delay | | | 355.9 | | | | | | | | | |
| Level of Service | | | F | | | | | | | | | |
| Intersection Capacity Utiliza | tion | | 119.3% | IC | CU Level | of Service | | | Н | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| | | | | | | | | | | | | |

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|-----------------------------------|----------|----------|-------|------|-----------|------------|---------|------------|----------|----------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | | | | | ¥ | ∱ } | | ¥ | ^ | 7 |
| Volume (vph) | 760 | 0 | 50 | 0 | 0 | 0 | 60 | 1090 | 0 | 0 | 880 | 550 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 6.0 | | | | | 5.0 | 7.0 | | | 7.0 | 7.0 |
| Lane Util. Factor | | 1.00 | | | | | 1.00 | 0.95 | | | 0.95 | 1.00 |
| Frt | | 0.99 | | | | | 1.00 | 1.00 | | | 1.00 | 0.85 |
| Flt Protected | | 0.96 | | | | | 0.95 | 1.00 | | | 1.00 | 1.00 |
| Satd. Flow (prot) | | 1764 | | | | | 1770 | 3539 | | | 3539 | 1583 |
| Flt Permitted | | 0.96 | | | | | 0.95 | 1.00 | | | 1.00 | 1.00 |
| Satd. Flow (perm) | | 1764 | | | | | 1770 | 3539 | | | 3539 | 1583 |
| Peak-hour factor, PHF | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Adj. Flow (vph) | 792 | 0 | 52 | 0 | 0 | 0 | 62 | 1135 | 0 | 0 | 917 | 573 |
| RTOR Reduction (vph) | 0 | 49 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 311 |
| Lane Group Flow (vph) | 0 | 795 | 0 | 0 | 0 | 0 | 62 | 1135 | 0 | 0 | 917 | 262 |
| Turn Type | Perm | NA | | | | | Prot | NA | | Prot | NA | Perm |
| Protected Phases | | 4 | | | | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | | | | | | | | | | 6 |
| Actuated Green, G (s) | | 31.3 | | | | | 6.9 | 59.2 | | | 47.3 | 47.3 |
| Effective Green, g (s) | | 31.3 | | | | | 6.9 | 59.2 | | | 47.3 | 47.3 |
| Actuated g/C Ratio | | 0.30 | | | | | 0.07 | 0.57 | | | 0.46 | 0.46 |
| Clearance Time (s) | | 6.0 | | | | | 5.0 | 7.0 | | | 7.0 | 7.0 |
| Vehicle Extension (s) | | 2.0 | | | | | 2.0 | 5.0 | | | 5.0 | 5.0 |
| Lane Grp Cap (vph) | | 533 | | | | | 118 | 2024 | | | 1617 | 723 |
| v/s Ratio Prot | | | | | | | 0.04 | c0.32 | | | 0.26 | |
| v/s Ratio Perm | | 0.45 | | | | | | | | | | 0.17 |
| v/c Ratio | | 1.49 | | | | | 0.53 | 0.56 | | | 0.57 | 0.36 |
| Uniform Delay, d1 | | 36.1 | | | | | 46.7 | 14.0 | | | 20.6 | 18.3 |
| Progression Factor | | 1.00 | | | | | 1.00 | 1.00 | | | 1.00 | 1.00 |
| Incremental Delay, d2 | | 231.2 | | | | | 1.9 | 0.6 | | | 0.8 | 0.6 |
| Delay (s) | | 267.3 | | | | | 48.7 | 14.5 | | | 21.4 | 18.9 |
| Level of Service | | F | | | 0.0 | | D | В | | | C | В |
| Approach Delay (s) | | 267.3 | | | 0.0 | | | 16.3 | | | 20.4 | |
| Approach LOS | | F | | | Α | | | В | | | С | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 78.0 | H | CM 2000 | Level of S | Service | | E | | | |
| HCM 2000 Volume to Capacit | ty ratio | | 0.93 | _ | | | | | | | | |
| Actuated Cycle Length (s) | | | 103.5 | | um of los | | | | 18.0 | | | |
| Intersection Capacity Utilization | on | | 93.6% | IC | U Level | of Service | | | F | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

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|---|------------|----------|-------|------|-------------|------------|-----------|----------|------|----------|----------|-----------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ર્ન | 7 | | 4 | | Į, | £ | | ¥ | † | 7 |
| Volume (vph) | 10 | 100 | 10 | 30 | 40 | 130 | 10 | 670 | 20 | 190 | 700 | 10 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 6.5 | 6.5 | | 6.0 | | 4.0 | 6.0 | | 4.0 | 6.0 | 6.0 |
| Lane Util. Factor | | 1.00 | 1.00 | | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Frpb, ped/bikes | | 1.00 | 0.98 | | 0.97 | | 1.00 | 1.00 | | 1.00 | 1.00 | 0.98 |
| Flpb, ped/bikes | | 1.00 | 1.00 | | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Frt | | 1.00 | 0.85 | | 0.91 | | 1.00 | 1.00 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | | 1.00 | 1.00 | | 0.99 | | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | | 1854 | 1547 | | 1642 | | 1769 | 1855 | | 1770 | 1863 | 1548 |
| Flt Permitted | | 0.93 | 1.00 | | 0.93 | | 0.29 | 1.00 | | 0.18 | 1.00 | 1.00 |
| Satd. Flow (perm) | 0.00 | 1727 | 1547 | 0.00 | 1531 | 0.00 | 531 | 1855 | 0.00 | 328 | 1863 | 1548 |
| Peak-hour factor, PHF | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |
| Adj. Flow (vph) | 11 | 114 | 11 | 34 | 45 | 148 | 11 | 761 | 23 | 216 | 795 | 11 |
| RTOR Reduction (vph) | 0 | 125 | 9 | 0 | 56 | 0 | 0 11 | 1 783 | 0 | 0 | 0 795 | 4 7 |
| Lane Group Flow (vph) | 0 | 125 | 2 | 0 | 171 | 0 | 11 | 783 | 0 | 216 | 795 | 1 |
| Confl. Peds. (#/hr) Confl. Bikes (#/hr) | ļ | | I | 1 | | 1 8 | ı | | | | | ı |
| | Dorm | NΙΛ | Dorm | Dorm | NΙΛ | 0 | n ma . mt | NIA | | nm. nt | NIA | Dorm |
| Turn Type | Perm | NA 4 | Perm | Perm | NA 8 | | pm+pt | NA 2 | | pm+pt | NA 6 | Perm |
| Protected Phases Permitted Phases | 1 | 4 | 4 | 8 | Ö | | 5 2 | Z | | 1 | 0 | 4 |
| Actuated Green, G (s) | 4 | 14.3 | 14.3 | 0 | 14.8 | | 51.0 | 50.3 | | 62.9 | 58.2 | 6 58.2 |
| Effective Green, g (s) | | 14.3 | 14.3 | | 14.8 | | 51.0 | 50.3 | | 62.9 | 58.2 | 58.2 |
| Actuated g/C Ratio | | 0.16 | 0.16 | | 0.16 | | 0.57 | 0.56 | | 0.70 | 0.65 | 0.65 |
| Clearance Time (s) | | 6.5 | 6.5 | | 6.0 | | 4.0 | 6.0 | | 4.0 | 6.0 | 6.0 |
| Vehicle Extension (s) | | 2.0 | 2.0 | | 2.0 | | 2.0 | 5.0 | | 2.0 | 5.0 | 5.0 |
| Lane Grp Cap (vph) | | 275 | 246 | | 252 | | 311 | 1040 | | 368 | 1208 | 1004 |
| v/s Ratio Prot | | 213 | 240 | | 232 | | 0.00 | c0.42 | | c0.06 | 0.43 | 1004 |
| v/s Ratio Perm | | 0.07 | 0.00 | | c0.11 | | 0.02 | 60.42 | | 0.36 | 0.43 | 0.00 |
| v/c Ratio | | 0.45 | 0.01 | | 0.68 | | 0.04 | 0.75 | | 0.59 | 0.66 | 0.01 |
| Uniform Delay, d1 | | 34.2 | 31.7 | | 35.2 | | 9.1 | 15.0 | | 11.1 | 9.7 | 5.6 |
| Progression Factor | | 1.00 | 1.00 | | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | | 0.4 | 0.0 | | 5.6 | | 0.0 | 3.7 | | 1.5 | 1.8 | 0.0 |
| Delay (s) | | 34.6 | 31.7 | | 40.8 | | 9.1 | 18.7 | | 12.7 | 11.4 | 5.6 |
| Level of Service | | С | С | | D | | Α | В | | В | В | Α |
| Approach Delay (s) | | 34.4 | | | 40.8 | | | 18.6 | | | 11.6 | |
| Approach LOS | | С | | | D | | | В | | | В | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 18.6 | Н | CM 2000 | Level of | Service | | В | | | |
| HCM 2000 Volume to Capac | city ratio | | 0.73 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 89.7 | | um of lost | | | | 16.5 | | | |
| Intersection Capacity Utilizat | tion | | 78.8% | IC | CU Level of | of Service | 9 | | D | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

| | ٠ | → | • | • | ← | • | • | † | / | > | ļ | 4 |
|-------------------------------|-------------|----------|-------|-------------------------------|------------|------------|------|----------|------|-------------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | J. | eî | | ¥ | † | 7 | ¥ | † | 7 | ¥ | f) | |
| Volume (vph) | 10 | 290 | 20 | 110 | 190 | 290 | 10 | 190 | 80 | 260 | 70 | 10 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Frpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | |
| Flpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Frt | 1.00 | 0.99 | | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.98 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1767 | 1842 | | 1768 | 1863 | 1549 | 1767 | 1863 | 1549 | 1767 | 1822 | |
| Flt Permitted | 0.63 | 1.00 | | 0.52 | 1.00 | 1.00 | 0.70 | 1.00 | 1.00 | 0.63 | 1.00 | |
| Satd. Flow (perm) | 1169 | 1842 | | 966 | 1863 | 1549 | 1303 | 1863 | 1549 | 1169 | 1822 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 11 | 315 | 22 | 120 | 207 | 315 | 11 | 207 | 87 | 283 | 76 | 11 |
| RTOR Reduction (vph) | 0 | 6 | 0 | 0 | 0 | 201 | 0 | 0 | 53 | 0 | 7 | 0 |
| Lane Group Flow (vph) | 11 | 331 | 0 | 120 | 207 | 114 | 11 | 207 | 34 | 283 | 80 | 0 |
| Confl. Peds. (#/hr) | 2 | | 2 | 2 | | 2 | 2 | | 2 | 2 | | 2 |
| Turn Type | Perm | NA | | Perm | NA | Perm | Perm | NA | Perm | Perm | NA | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | 8 | 2 | | 2 | 6 | | |
| Actuated Green, G (s) | 11.8 | 11.8 | | 11.8 | 11.8 | 11.8 | 12.9 | 12.9 | 12.9 | 12.9 | 12.9 | |
| Effective Green, g (s) | 11.8 | 11.8 | | 11.8 | 11.8 | 11.8 | 12.9 | 12.9 | 12.9 | 12.9 | 12.9 | |
| Actuated g/C Ratio | 0.36 | 0.36 | | 0.36 | 0.36 | 0.36 | 0.39 | 0.39 | 0.39 | 0.39 | 0.39 | |
| Clearance Time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 421 | 664 | | 348 | 672 | 558 | 514 | 734 | 611 | 461 | 718 | |
| v/s Ratio Prot | | c0.18 | | | 0.11 | | | 0.11 | | | 0.04 | |
| v/s Ratio Perm | 0.01 | | | 0.12 | | 0.07 | 0.01 | | 0.02 | c0.24 | | |
| v/c Ratio | 0.03 | 0.50 | | 0.34 | 0.31 | 0.20 | 0.02 | 0.28 | 0.06 | 0.61 | 0.11 | |
| Uniform Delay, d1 | 6.7 | 8.1 | | 7.6 | 7.5 | 7.2 | 6.0 | 6.7 | 6.1 | 7.9 | 6.3 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.0 | 0.6 | | 0.6 | 0.3 | 0.2 | 0.0 | 0.2 | 0.0 | 2.4 | 0.1 | |
| Delay (s) | 6.8 | 8.7 | | 8.2 | 7.8 | 7.4 | 6.1 | 7.0 | 6.2 | 10.3 | 6.3 | |
| Level of Service | А | Α | | Α | А | Α | Α | Α | Α | В | Α | |
| Approach Delay (s) | | 8.7 | | | 7.7 | | | 6.7 | | | 9.4 | |
| Approach LOS | | Α | | | А | | | Α | | | Α | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 8.1 | 3.1 HCM 2000 Level of Service | | | | | Α | | | |
| HCM 2000 Volume to Capa | icity ratio | | 0.56 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 32.7 | Sı | um of lost | t time (s) | | | 8.0 | | | |
| Intersection Capacity Utiliza | ation | | 60.6% | IC | U Level | of Service | | | В | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

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|---------------------------------|------|----------|-------|------|-------------|------------|------|----------|------|----------|----------|----------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ሻ | f) | | ሻ | ĵ» | | Ť | ∱ | | ሻ | ^ | |
| Volume (veh/h) | 170 | 130 | 130 | 10 | 100 | 50 | 240 | 160 | 10 | 100 | 90 | 160 |
| Sign Control | | Free | | | Free | | | Stop | | | Stop | |
| Grade | | 0% | | | 0% | | | 0% | | | 0% | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 185 | 141 | 141 | 11 | 109 | 54 | 261 | 174 | 11 | 109 | 98 | 174 |
| Pedestrians | | | | | | | | | | | | |
| Lane Width (ft) | | | | | | | | | | | | |
| Walking Speed (ft/s) | | | | | | | | | | | | |
| Percent Blockage | | | | | | | | | | | | |
| Right turn flare (veh) | | | | | | | | | | | | |
| Median type | | None | | | None | | | | | | | |
| Median storage veh) | | | | | | | | | | | | |
| Upstream signal (ft) | | | | | | | | | | | | |
| pX, platoon unblocked | | | | | | | | | | | | |
| vC, conflicting volume | 163 | | | 283 | | | 935 | 766 | 212 | 766 | 810 | 136 |
| vC1, stage 1 conf vol | | | | | | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | | | | | | |
| vCu, unblocked vol | 163 | | | 283 | | | 935 | 766 | 212 | 766 | 810 | 136 |
| tC, single (s) | 4.1 | | | 4.1 | | | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| tC, 2 stage (s) | | | | | | | | | | | | |
| tF (s) | 2.2 | | | 2.2 | | | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| p0 queue free % | 87 | | | 99 | | | 0 | 39 | 99 | 26 | 64 | 81 |
| cM capacity (veh/h) | 1416 | | | 1280 | | | 129 | 287 | 828 | 148 | 271 | 913 |
| Direction, Lane # | EB 1 | EB 2 | WB 1 | WB 2 | NB 1 | NB 2 | SB 1 | SB 2 | | | | |
| Volume Total | 185 | 283 | 11 | 163 | 261 | 185 | 109 | 272 | | | | |
| Volume Left | 185 | 0 | 11 | 0 | 261 | 0 | 109 | 0 | | | | |
| Volume Right | 0 | 141 | 0 | 54 | 0 | 11 | 0 | 174 | | | | |
| cSH | 1416 | 1700 | 1280 | 1700 | 129 | 298 | 148 | 492 | | | | |
| Volume to Capacity | 0.13 | 0.17 | 0.01 | 0.10 | 2.02 | 0.62 | 0.74 | 0.55 | | | | |
| Queue Length 95th (ft) | 11 | 0 | 1 | 0 | 528 | 96 | 110 | 83 | | | | |
| Control Delay (s) | 7.9 | 0.0 | 7.8 | 0.0 | 543.5 | 34.9 | 77.7 | 20.9 | | | | |
| Lane LOS | Α | | Α | | F | D | F | С | | | | |
| Approach Delay (s) | 3.1 | | 0.5 | | 332.6 | | 37.2 | | | | | |
| Approach LOS | | | | | F | | Е | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Average Delay | | | 111.7 | | | | | | | | | |
| Intersection Capacity Utilizati | on | | 59.3% | 10 | CU Level of | of Service | | | В | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| | | | | | | | | | | | | |

| | • | • | 4 | † | ↓ | 4 |
|-------------------------------|-------------|------|-------|------------|------------|-------------|
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | ¥ | | ሻ | † † | ^ | 7 |
| Volume (vph) | 460 | 200 | 90 | 490 | 560 | 220 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 6.8 | | 5.0 | 6.3 | 6.3 | 6.3 |
| Lane Util. Factor | 1.00 | | 1.00 | 0.95 | 0.95 | 1.00 |
| Frt | 0.96 | | 1.00 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.97 | | 0.95 | 1.00 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1726 | | 1770 | 3539 | 3539 | 1583 |
| Flt Permitted | 0.97 | | 0.95 | 1.00 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1726 | | 1770 | 3539 | 3539 | 1583 |
| Peak-hour factor, PHF | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Adj. Flow (vph) | 511 | 222 | 100 | 544 | 622 | 244 |
| RTOR Reduction (vph) | 10 | 0 | 0 | 0 | 0 | 175 |
| Lane Group Flow (vph) | 723 | 0 | 100 | 544 | 622 | 69 |
| Turn Type | NA | | Prot | NA | NA | Perm |
| Protected Phases | 4 | | 5 | 2 | 6 | |
| Permitted Phases | | | | | | 6 |
| Actuated Green, G (s) | 32.4 | | 7.7 | 35.5 | 22.8 | 22.8 |
| Effective Green, g (s) | 32.4 | | 7.7 | 35.5 | 22.8 | 22.8 |
| Actuated g/C Ratio | 0.40 | | 0.10 | 0.44 | 0.28 | 0.28 |
| Clearance Time (s) | 6.8 | | 5.0 | 6.3 | 6.3 | 6.3 |
| Vehicle Extension (s) | 2.0 | | 2.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 690 | | 168 | 1551 | 996 | 445 |
| v/s Ratio Prot | c0.42 | | c0.06 | 0.15 | c0.18 | |
| v/s Ratio Perm | | | | | | 0.04 |
| v/c Ratio | 1.05 | | 0.60 | 0.35 | 0.62 | 0.15 |
| Uniform Delay, d1 | 24.3 | | 35.2 | 15.1 | 25.4 | 21.9 |
| Progression Factor | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 47.6 | | 3.7 | 0.1 | 1.2 | 0.2 |
| Delay (s) | 71.9 | | 38.9 | 15.2 | 26.6 | 22.0 |
| Level of Service | Е | | D | В | С | С |
| Approach Delay (s) | 71.9 | | | 18.9 | 25.3 | |
| Approach LOS | Е | | | В | С | |
| Intersection Summary | | | | | | |
| HCM 2000 Control Delay | | | 38.7 | Н | CM 2000 | Level of Se |
| HCM 2000 Volume to Capa | acity ratio | | 0.84 | | | |
| Actuated Cycle Length (s) | | | 81.0 | S | um of lost | t time (s) |
| Intersection Capacity Utiliza | ation | | 74.4% | | | of Service |
| Analysis Period (min) | | | 15 | | | |
| c Critical Lane Group | | | | | | |

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|--------------------------------|-----------|--------|----------|------|-------------|------------------|---|
| Movement | WBL | WBR | NBT | NBR | SBL | SBT | |
| Lane Configurations | ሻ | 7 | ^ | 7 | ሻ | † | |
| Volume (vph) | 120 | 0 | 740 | 280 | 0 | 850 | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | |
| Total Lost time (s) | 4.0 | | 4.0 | 4.0 | | 4.0 | |
| Lane Util. Factor | 1.00 | | 1.00 | 1.00 | | 1.00 | |
| Frt | 1.00 | | 1.00 | 0.85 | | 1.00 | |
| Flt Protected | 0.95 | | 1.00 | 1.00 | | 1.00 | |
| Satd. Flow (prot) | 1770 | | 1863 | 1583 | | 1863 | |
| Flt Permitted | 0.95 | | 1.00 | 1.00 | | 1.00 | |
| Satd. Flow (perm) | 1770 | | 1863 | 1583 | | 1863 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | |
| Adj. Flow (vph) | 130 | 0 | 804 | 304 | 0 | 924 | |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | |
| Lane Group Flow (vph) | 130 | 0 | 804 | 304 | 0 | 924 | |
| Turn Type | NA | custom | NA | Free | Perm | NA | |
| Protected Phases | | | 2 | | | 6 | |
| Permitted Phases | 8 | 8 | | Free | 6 | | |
| Actuated Green, G (s) | 7.7 | | 38.0 | 53.7 | | 38.0 | |
| Effective Green, g (s) | 7.7 | | 38.0 | 53.7 | | 38.0 | |
| Actuated g/C Ratio | 0.14 | | 0.71 | 1.00 | | 0.71 | |
| Clearance Time (s) | 4.0 | | 4.0 | | | 4.0 | |
| Vehicle Extension (s) | 3.0 | | 3.0 | | | 3.0 | |
| Lane Grp Cap (vph) | 253 | | 1318 | 1583 | | 1318 | |
| v/s Ratio Prot | | | 0.43 | | | c0.50 | |
| v/s Ratio Perm | c0.07 | | | 0.19 | | | |
| v/c Ratio | 0.51 | | 0.61 | 0.19 | | 0.70 | |
| Uniform Delay, d1 | 21.3 | | 4.0 | 0.0 | | 4.6 | |
| Progression Factor | 1.00 | | 1.00 | 1.00 | | 1.00 | |
| Incremental Delay, d2 | 1.8 | | 8.0 | 0.3 | | 1.7 | |
| Delay (s) | 23.0 | | 4.9 | 0.3 | | 6.3 | |
| Level of Service | С | | Α | Α | | Α | |
| Approach Delay (s) | 23.0 | | 3.6 | | | 6.3 | |
| Approach LOS | С | | Α | | | Α | |
| Intersection Summary | | | | | | | |
| HCM 2000 Control Delay | | | 5.9 | Н | CM 2000 | Level of Service | 9 |
| HCM 2000 Volume to Capac | ity ratio | | 0.67 | | | | |
| Actuated Cycle Length (s) | | | 53.7 | | um of lost | | |
| Intersection Capacity Utilizat | ion | | 58.1% | IC | CU Level of | of Service | |
| Analysis Period (min) | | | 15 | | | | |
| c Critical Lane Group | | | | | | | |

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|-----------------------------------|----------|----------|-------|-------|-----------|------------|---------|----------|----------|-------------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ર્ન | 7 | ¥ | ર્ન | 7 | ¥ | † | 7 | ¥ | † | 7 |
| Volume (vph) | 10 | 10 | 10 | 760 | 10 | 10 | 10 | 940 | 610 | 10 | 770 | 10 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 5.0 | 5.0 | 5.0 | 5.0 | 4.0 | 4.0 | 5.0 | 4.0 | 4.0 | 5.0 | 5.0 |
| Lane Util. Factor | | 1.00 | 1.00 | 0.95 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frt | | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | | 0.98 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | | 1817 | 1583 | 1681 | 1687 | 1583 | 1770 | 3539 | 1583 | 1770 | 3539 | 1583 |
| Flt Permitted | | 0.98 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | | 1817 | 1583 | 1681 | 1687 | 1583 | 1770 | 3539 | 1583 | 1770 | 3539 | 1583 |
| Peak-hour factor, PHF | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Adj. Flow (vph) | 10 | 10 | 10 | 792 | 10 | 10 | 10 | 979 | 635 | 10 | 802 | 10 |
| RTOR Reduction (vph) | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| Lane Group Flow (vph) | 0 | 20 | 0 | 404 | 398 | 10 | 10 | 979 | 635 | 10 | 802 | 4 |
| Turn Type | Split | NA | Perm | Split | NA | Free | Prot | NA | Free | Prot | NA | Perm |
| Protected Phases | 4 | 4 | | 3 | 3 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | | | 4 | | | Free | | | Free | | | 6 |
| Actuated Green, G (s) | | 3.9 | 3.9 | 36.0 | 36.0 | 101.3 | 0.9 | 41.5 | 101.3 | 0.9 | 41.5 | 41.5 |
| Effective Green, g (s) | | 3.9 | 3.9 | 36.0 | 36.0 | 101.3 | 0.9 | 41.5 | 101.3 | 0.9 | 41.5 | 41.5 |
| Actuated g/C Ratio | | 0.04 | 0.04 | 0.36 | 0.36 | 1.00 | 0.01 | 0.41 | 1.00 | 0.01 | 0.41 | 0.41 |
| Clearance Time (s) | | 5.0 | 5.0 | 5.0 | 5.0 | | 4.0 | 5.0 | | 4.0 | 5.0 | 5.0 |
| Vehicle Extension (s) | | 3.0 | 3.0 | 3.0 | 3.0 | | 2.0 | 4.0 | | 2.0 | 4.0 | 4.0 |
| Lane Grp Cap (vph) | | 69 | 60 | 597 | 599 | 1583 | 15 | 1449 | 1583 | 15 | 1449 | 648 |
| v/s Ratio Prot | | 0.01 | | c0.24 | 0.24 | | 0.01 | c0.28 | | 0.01 | 0.23 | |
| v/s Ratio Perm | | | 0.00 | | | 0.01 | | | c0.40 | | | 0.00 |
| v/c Ratio | | 0.29 | 0.01 | 0.68 | 0.66 | 0.01 | 0.67 | 0.68 | 0.40 | 0.67 | 0.55 | 0.01 |
| Uniform Delay, d1 | | 47.4 | 46.8 | 27.7 | 27.6 | 0.0 | 50.1 | 24.4 | 0.0 | 50.1 | 22.8 | 17.7 |
| Progression Factor | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | | 2.3 | 0.0 | 3.0 | 2.8 | 0.0 | 62.4 | 1.4 | 0.8 | 62.4 | 0.6 | 0.0 |
| Delay (s) | | 49.7 | 46.9 | 30.8 | 30.3 | 0.0 | 112.4 | 25.8 | 8.0 | 112.4 | 23.4 | 17.7 |
| Level of Service | | D | D | С | C | А | F | C | Α | F | C | В |
| Approach Delay (s) | | 48.7 | | | 30.2 | | | 16.5 | | | 24.4 | |
| Approach LOS | | D | | | С | | | В | | | С | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 22.2 | H | CM 2000 | Level of | Service | | С | | | |
| HCM 2000 Volume to Capaci | ty ratio | | 0.70 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 101.3 | | um of los | | | | 19.0 | | | |
| Intersection Capacity Utilization | on | | 62.3% | IC | :U Level | of Service | | | В | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

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|-------------------------------|-------|----------|-------|------|------------|------------|-------|----------|-------------|----------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ર્ન | 7 | | र्स | 7 | ¥ | † | 7 | ¥ | † | 7 |
| Volume (vph) | 20 | 80 | 30 | 290 | 140 | 390 | 40 | 480 | 280 | 370 | 480 | 30 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 5.0 | 5.0 | | 5.0 | 5.0 | 4.0 | 5.0 | 5.0 | 4.0 | 5.0 | 5.0 |
| Lane Util. Factor | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frpb, ped/bikes | | 1.00 | 1.00 | | 1.00 | 0.96 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Flpb, ped/bikes | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | | 1.00 | 0.85 | | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | | 0.99 | 1.00 | | 0.97 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | | 1842 | 1583 | | 1802 | 1528 | 1770 | 1863 | 1583 | 1770 | 1863 | 1583 |
| Flt Permitted | | 0.81 | 1.00 | | 0.73 | 1.00 | 0.40 | 1.00 | 1.00 | 0.17 | 1.00 | 1.00 |
| Satd. Flow (perm) | | 1508 | 1583 | | 1364 | 1528 | 749 | 1863 | 1583 | 325 | 1863 | 1583 |
| Peak-hour factor, PHF | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Adj. Flow (vph) | 22 | 86 | 32 | 312 | 151 | 419 | 43 | 516 | 301 | 398 | 516 | 32 |
| RTOR Reduction (vph) | 0 | 0 | 20 | 0 | 0 | 211 | 0 | 0 | 194 | 0 | 0 | 17 |
| Lane Group Flow (vph) | 0 | 108 | 12 | 0 | 463 | 208 | 43 | 516 | 107 | 398 | 516 | 15 |
| Confl. Peds. (#/hr) | 6 | | | | | 6 | | | | | | |
| Turn Type | Perm | NA | Perm | Perm | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | 8 | 2 | | 2 | 6 | | 6 |
| Actuated Green, G (s) | | 37.5 | 37.5 | | 37.5 | 37.5 | 40.5 | 36.9 | 36.9 | 56.1 | 48.5 | 48.5 |
| Effective Green, g (s) | | 37.5 | 37.5 | | 37.5 | 37.5 | 40.5 | 36.9 | 36.9 | 56.1 | 48.5 | 48.5 |
| Actuated g/C Ratio | | 0.36 | 0.36 | | 0.36 | 0.36 | 0.39 | 0.36 | 0.36 | 0.54 | 0.47 | 0.47 |
| Clearance Time (s) | | 5.0 | 5.0 | | 5.0 | 5.0 | 4.0 | 5.0 | 5.0 | 4.0 | 5.0 | 5.0 |
| Vehicle Extension (s) | | 2.5 | 2.5 | | 2.5 | 2.5 | 2.0 | 5.0 | 5.0 | 2.0 | 5.0 | 5.0 |
| Lane Grp Cap (vph) | | 545 | 572 | | 493 | 553 | 328 | 663 | 563 | 387 | 872 | 741 |
| v/s Ratio Prot | | | | | | | 0.00 | 0.28 | | c0.15 | 0.28 | |
| v/s Ratio Perm | | 0.07 | 0.01 | | c0.34 | 0.14 | 0.05 | | 0.07 | c0.40 | | 0.01 |
| v/c Ratio | | 0.20 | 0.02 | | 0.94 | 0.38 | 0.13 | 0.78 | 0.19 | 1.03 | 0.59 | 0.02 |
| Uniform Delay, d1 | | 22.7 | 21.2 | | 31.9 | 24.4 | 19.9 | 29.7 | 23.0 | 23.4 | 20.3 | 14.8 |
| Progression Factor | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | | 0.1 | 0.0 | | 25.8 | 0.3 | 0.1 | 6.7 | 0.3 | 53.2 | 1.6 | 0.0 |
| Delay (s) | | 22.8 | 21.3 | | 57.7 | 24.7 | 19.9 | 36.4 | 23.4 | 76.6 | 21.9 | 14.8 |
| Level of Service | | С | С | | Е | С | В | D | С | E | С | В |
| Approach Delay (s) | | 22.5 | | | 42.0 | | | 31.0 | | | 44.7 | |
| Approach LOS | | С | | | D | | | С | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 38.6 | | | | | | D | | | |
| HCM 2000 Volume to Capa | | | | | | | | | | | | |
| Actuated Cycle Length (s) | | | | | um of lost | | | | 14.0 | | | |
| Intersection Capacity Utiliza | ation | | 87.5% | IC | U Level | of Service | Э | | Е | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

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|------------------------------|-------------|----------|-------|-----------------------------|-------------|------------|-------|----------|-------------|-------------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | * | ĥ | | ሻ | † | 7 | ሻ | 1> | | ሻ | ^ | |
| Volume (vph) | 210 | 430 | 50 | 100 | 580 | 400 | 30 | 200 | 60 | 340 | 400 | 170 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 5.0 | 5.0 | | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | | 5.0 | 5.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 0.99 | | 1.00 | 0.99 | |
| Flpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Frt | 1.00 | 0.98 | | 1.00 | 1.00 | 0.85 | 1.00 | 0.97 | | 1.00 | 0.96 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1770 | 1828 | | 1768 | 1863 | 1583 | 1770 | 1789 | | 1769 | 1764 | |
| Flt Permitted | 0.09 | 1.00 | | 0.29 | 1.00 | 1.00 | 0.13 | 1.00 | | 0.34 | 1.00 | |
| Satd. Flow (perm) | 164 | 1828 | | 549 | 1863 | 1583 | 240 | 1789 | | 631 | 1764 | |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 216 | 443 | 52 | 103 | 598 | 412 | 31 | 206 | 62 | 351 | 412 | 175 |
| RTOR Reduction (vph) | 0 | 2 | 0 | 0 | 0 | 260 | 0 | 8 | 0 | 0 | 11 | 0 |
| Lane Group Flow (vph) | 216 | 493 | 0 | 103 | 598 | 152 | 31 | 260 | 0 | 351 | 576 | 0 |
| Confl. Peds. (#/hr) | | | 3 | 3 | | | 3 | | 1 | 1 | | 3 |
| Turn Type | pm+pt | NA | | pm+pt | NA | Perm | pm+pt | NA | | pm+pt | NA | |
| Protected Phases | 7 | 4 | | 3 | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | | 8 | | 8 | 2 | | | 6 | | |
| Actuated Green, G (s) | 60.4 | 47.1 | | 48.6 | 40.3 | 40.3 | 34.8 | 31.0 | | 49.1 | 40.3 | |
| Effective Green, g (s) | 60.4 | 47.1 | | 48.6 | 40.3 | 40.3 | 34.8 | 31.0 | | 49.1 | 40.3 | |
| Actuated g/C Ratio | 0.51 | 0.39 | | 0.41 | 0.34 | 0.34 | 0.29 | 0.26 | | 0.41 | 0.34 | |
| Clearance Time (s) | 5.0 | 5.0 | | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | | 5.0 | 5.0 | |
| Vehicle Extension (s) | 2.0 | 3.0 | | 2.0 | 3.0 | 3.0 | 2.0 | 3.0 | | 2.0 | 3.0 | |
| Lane Grp Cap (vph) | 285 | 720 | | 307 | 628 | 533 | 118 | 464 | | 384 | 594 | |
| v/s Ratio Prot | c0.10 | 0.27 | | 0.02 | c0.32 | | 0.01 | 0.15 | | c0.10 | c0.33 | |
| v/s Ratio Perm | 0.29 | | | 0.11 | | 0.10 | 0.07 | | | 0.28 | | |
| v/c Ratio | 0.76 | 0.68 | | 0.34 | 0.95 | 0.28 | 0.26 | 0.56 | | 0.91 | 0.97 | |
| Uniform Delay, d1 | 30.5 | 30.0 | | 23.5 | 38.7 | 29.0 | 33.0 | 38.3 | | 30.9 | 39.0 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | | 1.00 | 1.00 | |
| Incremental Delay, d2 | 9.8 | 2.7 | | 0.2 | 24.5 | 0.3 | 0.4 | 1.5 | | 25.3 | 29.4 | |
| Delay (s) | 40.3 | 32.7 | | 23.7 | 63.2 | 29.3 | 33.5 | 39.9 | | 56.2 | 68.5 | |
| Level of Service | D | C | | С | E | С | С | D | | Е | E | |
| Approach Delay (s) | | 35.0 | | | 47.0 | | | 39.2 | | | 63.9 | |
| Approach LOS | | D | | | D | | | D | | | E | |
| Intersection Summary | | | | 6 HCM 2000 Level of Service | | | | | | | | |
| HCM 2000 Control Delay | | | 48.6 | Н | Service | | D | | | | | |
| HCM 2000 Volume to Capa | acity ratio | | 0.96 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 119.5 | | um of lost | | | | 20.0 | | | |
| Intersection Capacity Utiliz | ation | | 93.7% | IC | CU Level of | of Service | 9 | | F | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

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|-------------------------------|-------|----------|--------|-------|----------|------------|------|----------|-------------|----------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | | | 4 | | ň | ĵ. | | J. | ą. | |
| Sign Control | | Stop | | | Stop | | | Stop | | | Stop | |
| Volume (vph) | 250 | 420 | 140 | 30 | 390 | 70 | 150 | 360 | 40 | 100 | 400 | 300 |
| Peak Hour Factor | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Hourly flow rate (vph) | 255 | 429 | 143 | 31 | 398 | 71 | 153 | 367 | 41 | 102 | 408 | 306 |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | NB 2 | SB 1 | SB 2 | | | | | | |
| Volume Total (vph) | 827 | 500 | 153 | 408 | 102 | 714 | | | | | | |
| Volume Left (vph) | 255 | 31 | 153 | 0 | 102 | 0 | | | | | | |
| Volume Right (vph) | 143 | 71 | 0 | 41 | 0 | 306 | | | | | | |
| Hadj (s) | -0.01 | -0.04 | 0.53 | -0.04 | 0.53 | -0.27 | | | | | | |
| Departure Headway (s) | 9.4 | 9.4 | 10.2 | 9.6 | 10.2 | 9.4 | | | | | | |
| Degree Utilization, x | 2.17 | 1.31 | 0.43 | 1.09 | 0.29 | 1.86 | | | | | | |
| Capacity (veh/h) | 388 | 390 | 342 | 384 | 350 | 390 | | | | | | |
| Control Delay (s) | 555.8 | 183.5 | 19.5 | 102.4 | 16.0 | 416.6 | | | | | | |
| Approach Delay (s) | 555.8 | 183.5 | 79.8 | | 366.5 | | | | | | | |
| Approach LOS | F | F | F | | F | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Delay | | | 331.0 | | | | | | | | | |
| Level of Service | | | F | | | | | | | | | |
| Intersection Capacity Utiliza | ation | | 132.0% | IC | CU Level | of Service | | | Н | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| | | | | | | | | | | | | |

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|-------------------------------|------------|----------|-------|------|------------|------------|---------|------------|-------------|----------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | | | | | 7 | ∱ ∱ | | Ť | ^ | 7 |
| Volume (vph) | 590 | 0 | 10 | 0 | 0 | 0 | 60 | 880 | 0 | 10 | 1210 | 790 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 6.0 | | | | | 5.0 | 7.0 | | 5.0 | 7.0 | 7.0 |
| Lane Util. Factor | | 1.00 | | | | | 1.00 | 0.95 | | 1.00 | 0.95 | 1.00 |
| Frpb, ped/bikes | | 1.00 | | | | | 1.00 | 1.00 | | 1.00 | 1.00 | 0.98 |
| Flpb, ped/bikes | | 1.00 | | | | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Frt | | 1.00 | | | | | 1.00 | 1.00 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | | 0.95 | | | | | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | | 1771 | | | | | 1770 | 3539 | | 1770 | 3539 | 1550 |
| Flt Permitted | | 0.95 | | | | | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | | 1771 | | | | | 1770 | 3539 | | 1770 | 3539 | 1550 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 641 | 0 | 11 | 0 | 0 | 0 | 65 | 957 | 0 | 11 | 1315 | 859 |
| RTOR Reduction (vph) | 0 | 53 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 380 |
| Lane Group Flow (vph) | 0 | 599 | 0 | 0 | 0 | 0 | 65 | 957 | 0 | 11 | 1315 | 479 |
| Confl. Peds. (#/hr) | | | | | | | | | | | | 1 |
| Turn Type | Perm | NA | | | | | Prot | NA | | Prot | NA | Perm |
| Protected Phases | | 4 | | | | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | | | | | | | | | | 6 |
| Actuated Green, G (s) | | 30.3 | | | | | 7.7 | 76.9 | | 1.3 | 70.5 | 70.5 |
| Effective Green, g (s) | | 30.3 | | | | | 7.7 | 76.9 | | 1.3 | 70.5 | 70.5 |
| Actuated g/C Ratio | | 0.24 | | | | | 0.06 | 0.61 | | 0.01 | 0.56 | 0.56 |
| Clearance Time (s) | | 6.0 | | | | | 5.0 | 7.0 | | 5.0 | 7.0 | 7.0 |
| Vehicle Extension (s) | | 2.0 | | | | | 2.0 | 5.0 | | 2.0 | 5.0 | 5.0 |
| Lane Grp Cap (vph) | | 424 | | | | | 107 | 2151 | | 18 | 1972 | 863 |
| v/s Ratio Prot | | | | | | | c0.04 | 0.27 | | 0.01 | c0.37 | |
| v/s Ratio Perm | | 0.34 | | | | | | | | | | 0.31 |
| v/c Ratio | | 1.41 | | | | | 0.61 | 0.44 | | 0.61 | 0.67 | 0.55 |
| Uniform Delay, d1 | | 48.1 | | | | | 57.9 | 13.3 | | 62.3 | 19.7 | 17.9 |
| Progression Factor | | 1.00 | | | | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | | 199.0 | | | | | 6.5 | 0.3 | | 36.2 | 1.1 | 1.3 |
| Delay (s) | | 247.1 | | | | | 64.5 | 13.6 | | 98.5 | 20.9 | 19.3 |
| Level of Service | | F | | | | | E | В | | F | С | В |
| Approach Delay (s) | | 247.1 | | | 0.0 | | | 16.9 | | | 20.6 | |
| Approach LOS | | F | | | А | | | В | | | С | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 57.9 | H | CM 2000 | Level of S | Service | | Е | | | |
| HCM 2000 Volume to Capa | city ratio | | 0.87 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 126.5 | | um of lost | | | | 18.0 | | | |
| Intersection Capacity Utiliza | ation | | 85.1% | IC | U Level | of Service | | | Е | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

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|---------------------------------------|------------|--------------|--------------|------|--------------|------------|--------------|--------------|------|---------------------------------------|--------------|--------------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | र्स | 7 | | 4 | | Į, | £ | | ¥ | † | 7 |
| Volume (vph) | 10 | 30 | 10 | 30 | 70 | 120 | 10 | 650 | 30 | 120 | 590 | 10 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 6.5 | 6.5 | | 6.0 | | 4.0 | 6.0 | | 4.0 | 6.0 | 6.0 |
| Lane Util. Factor | | 1.00 | 1.00 | | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Frpb, ped/bikes | | 1.00 | 1.00 | | 0.98 | | 1.00 | 1.00 | | 1.00 | 1.00 | 0.98 |
| Flpb, ped/bikes | | 1.00 | 1.00 | | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Frt | | 1.00 | 0.85 | | 0.93 | | 1.00 | 0.99 | | 1.00 | 1.00 | 0.85 |
| Flt Protected | | 0.99 | 1.00 | | 0.99 | | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | | 1839 | 1583 | | 1678 | | 1769 | 1848 | | 1769 | 1863 | 1545 |
| Flt Permitted | | 0.85 | 1.00 | | 0.95 | | 0.37 | 1.00 | | 0.20 | 1.00 | 1.00 |
| Satd. Flow (perm) | | 1574 | 1583 | | 1601 | | 692 | 1848 | | 368 | 1863 | 1545 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 11 | 33 | 11 | 33 | 76 | 130 | 11 | 707 | 33 | 130 | 641 | 11 |
| RTOR Reduction (vph) | 0 | 0 | 9 | 0 | 35 | 0 | 0 | 1 | 0 | 0 | 0 | 4 |
| Lane Group Flow (vph) | 0 | 44 | 2 | 0 | 204 | 0 | 11 | 739 | 0 | 130 | 641 | 7 |
| Confl. Peds. (#/hr) | 1 | | | | | 1 | 2 | | 5 | 5 | | 2 |
| Confl. Bikes (#/hr) | D | NI A | Dame | D | NI A | 8 | | NI A | | | NIA | Dame |
| Turn Type | Perm | NA | Perm | Perm | NA | | pm+pt | NA | | pm+pt | NA | Perm |
| Protected Phases | 4 | 4 | 4 | 0 | 8 | | 5 | 2 | | 1 | 6 | , |
| Permitted Phases | 4 | 117 | 4 | 8 | 1 - 2 | | 2 | 47.0 | | 6 | F2 0 | 6 |
| Actuated Green, G (s) | | 14.7 | 14.7 14.7 | | 15.2 | | 47.6 47.6 | 46.8 46.8 | | 57.8 57.8 | 53.0 | 53.0 |
| Effective Green, g (s) | | 14.7 0.17 | 0.17 | | 15.2 0.18 | | 0.56 | 0.55 | | 0.68 | 53.0 0.62 | 53.0 0.62 |
| Actuated g/C Ratio Clearance Time (s) | | 6.5 | 6.5 | | 6.0 | | 4.0 | 6.0 | | 4.0 | 6.0 | 6.0 |
| Vehicle Extension (s) | | 2.0 | 2.0 | | 2.0 | | 2.0 | 5.0 | | 2.0 | 5.0 | 5.0 |
| | | 272 | 273 | | 286 | | 397 | 1017 | | 365 | 1161 | 963 |
| Lane Grp Cap (vph) v/s Ratio Prot | | 212 | 2/3 | | 280 | | 0.00 | c0.40 | | c0.03 | c0.34 | 903 |
| v/s Ratio Prot v/s Ratio Perm | | 0.03 | 0.00 | | c0.13 | | 0.00 | CU.4U | | 0.21 | CU.34 | 0.00 |
| v/c Ratio | | 0.03 | 0.00 | | 0.71 | | 0.02 | 0.73 | | 0.21 | 0.55 | 0.00 |
| Uniform Delay, d1 | | 29.9 | 29.1 | | 32.8 | | 8.5 | 14.3 | | 9.1 | 9.2 | 6.1 |
| Progression Factor | | 1.00 | 1.00 | | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | | 0.1 | 0.0 | | 6.8 | | 0.0 | 3.2 | | 0.2 | 1.00 | 0.0 |
| Delay (s) | | 30.0 | 29.1 | | 39.6 | | 8.5 | 17.5 | | 9.3 | 10.2 | 6.1 |
| Level of Service | | C | C | | D | | Α | 17.5 B | | 7.5 A | В | A |
| Approach Delay (s) | | 29.8 | - O | | 39.6 | | Λ. | 17.4 | | , , , , , , , , , , , , , , , , , , , | 10.0 | , , |
| Approach LOS | | C | | | D | | | В | | | A | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 17.5 | Н | CM 2000 | Level of | Service | | В | | | |
| HCM 2000 Volume to Capac | city ratio | | 0.70 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 85.0 | | um of lost | | | | 16.5 | | | |
| Intersection Capacity Utilizat | tion | | 75.5% | IC | CU Level of | of Service | 9 | | D | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

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|-------------------------------|--|------------|-------|------------|----------------------|------------|------------|------------|------------|-------------|------------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | * | ĵ» | | * | † | 7 | ሻ | † | 7 | ň | ĵ» | |
| Volume (vph) | 10 | 170 | 10 | 70 | 180 | 210 | 20 | 60 | 100 | 210 | 190 | 20 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | |
| Lane Util. Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Frpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | |
| Flpb, ped/bikes | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Frt | 1.00 | 0.99 | | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.99 | |
| Flt Protected | 0.95 | 1.00 | | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | |
| Satd. Flow (prot) | 1767 | 1845 | | 1767 | 1863 | 1549 | 1767 | 1863 | 1549 | 1767 | 1832 | |
| Flt Permitted | 0.63 | 1.00 | | 0.63 | 1.00 | 1.00 | 0.62 | 1.00 | 1.00 | 0.71 | 1.00 | |
| Satd. Flow (perm) | 1180 | 1845 | | 1180 | 1863 | 1549 | 1145 | 1863 | 1549 | 1329 | 1832 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 11 | 185 | 11 | 76 | 196 | 228 | 22 | 65 | 109 | 228 | 207 | 22 |
| RTOR Reduction (vph) | 0 | 6 | 0 | 0 | 0 | 166 | 0 | 0 | 57 | 0 | 8 | 0 |
| Lane Group Flow (vph) | 11 | 190 | 0 | 76 | 196 | 62 | 22 | 65 | 52 | 228 | 221 | 0 |
| Confl. Peds. (#/hr) | 2 | | 2 | 2 | | 2 | 2 | | 2 | 2 | | 2 |
| Turn Type | Perm | NA | | Perm | NA | Perm | Perm | NA | Perm | Perm | NA | |
| Protected Phases | | 4 | | | 8 | | | 2 | | | 6 | |
| Permitted Phases | 4 | | | 8 | | 8 | 2 | | 2 | 6 | | |
| Actuated Green, G (s) | 8.5 | 8.5 | | 8.5 | 8.5 | 8.5 | 14.8 | 14.8 | 14.8 | 14.8 | 14.8 | |
| Effective Green, g (s) | 8.5 | 8.5 | | 8.5 | 8.5 | 8.5 | 14.8 | 14.8 | 14.8 | 14.8 | 14.8 | |
| Actuated g/C Ratio | 0.27 | 0.27 | | 0.27 | 0.27 | 0.27 | 0.47 | 0.47 | 0.47 | 0.47 | 0.47 | |
| Clearance Time (s) | 4.0 | 4.0 | | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | |
| Vehicle Extension (s) | 3.0 | 3.0 | | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | |
| Lane Grp Cap (vph) | 320 | 501 | | 320 | 505 | 420 | 541 | 880 | 732 | 628 | 866 | |
| v/s Ratio Prot | 0.04 | 0.10 | | 0.07 | c0.11 | 0.04 | 0.00 | 0.03 | 0.00 | 0.47 | 0.12 | |
| v/s Ratio Perm | 0.01 | 0.00 | | 0.06 | 0.00 | 0.04 | 0.02 | 0.07 | 0.03 | c0.17 | 0.07 | |
| v/c Ratio | 0.03 | 0.38 | | 0.24 | 0.39 | 0.15 | 0.04 | 0.07 | 0.07 | 0.36 | 0.26 | |
| Uniform Delay, d1 | 8.4 | 9.3 | | 8.9 | 9.3 | 8.7 | 4.4 | 4.5 | 4.5 | 5.3 | 4.9 | |
| Progression Factor | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | |
| Incremental Delay, d2 | 0.0 8.4 | 0.5 9.7 | | 0.4 9.3 | 0.5 9.8 | 0.2 8.8 | 0.0 4.5 | 0.0 4.5 | 0.0 4.5 | 0.4 5.6 | 0.2 5.1 | |
| Delay (s) Level of Service | 6.4 A | | | 9.3 A | 9.8 A | 8.8 A | 4.5 A | 4.5 A | 4.5 A | 5.0 A | | |
| | А | A 9.7 | | А | 9.3 | А | А | 4.5 | А | А | A 5.4 | |
| Approach LOS | | 9.7 A | | | 9.3 A | | | 4.5 A | | | | |
| Approach LOS | | А | | | А | | | А | | | А | |
| Intersection Summary | | | 7.0 | | | | | | | | | |
| HCM 2000 Control Delay | ', ', | | 7.3 | H | CM 2000 | Level of S | service | | А | | | |
| | HCM 2000 Volume to Capacity ratio 0.37 | | | | | Harris () | | | 2.2 | | | |
| Actuated Cycle Length (s) | _ L! | | 31.3 | | um of lost | | | | 8.0 | | | |
| Intersection Capacity Utiliz | auon | | 42.1% | IC | ICU Level of Service | | | | Α | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

| | ۶ | → | • | • | ← | 4 | 1 | † | <i>></i> | / | | √ |
|---|------|----------|-------|------|-------------|------------|------|----------|-------------|----------|--------------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | ₽ | | 7 | 1> | | ሻ | ₽ | | 7 | 1> | |
| Volume (veh/h) | 130 | 100 | 170 | 20 | 130 | 130 | 110 | 80 | 10 | 100 | 130 | 140 |
| Sign Control | | Free | | | Free | | | Stop | | | Stop | |
| Grade | | 0% | | | 0% | | | 0% | | | 0% | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 141 | 109 | 185 | 22 | 141 | 141 | 120 | 87 | 11 | 109 | 141 | 152 |
| Pedestrians | | | | | | | | | | | | |
| Lane Width (ft) | | | | | | | | | | | | |
| Walking Speed (ft/s) | | | | | | | | | | | | |
| Percent Blockage | | | | | | | | | | | | |
| Right turn flare (veh) | | | | | | | | | | | | |
| Median type | | None | | | None | | | | | | | |
| Median storage veh) | | | | | | | | | | | | |
| Upstream signal (ft) | | | | | | | | | | | | |
| pX, platoon unblocked | | | | | | | | | | | | |
| vC, conflicting volume | 283 | | | 293 | | | 891 | 810 | 201 | 701 | 832 | 212 |
| vC1, stage 1 conf vol | | | | | | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | | | | | | |
| vCu, unblocked vol | 283 | | | 293 | | | 891 | 810 | 201 | 701 | 832 | 212 |
| tC, single (s) | 4.1 | | | 4.1 | | | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| tC, 2 stage (s) | | | | | | | | | | | | |
| tF (s) | 2.2 | | | 2.2 | | | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| p0 queue free % | 89 | | | 98 | | | 0 | 68 | 99 | 55 | 47 | 82 |
| cM capacity (veh/h) | 1280 | | | 1268 | | | 114 | 275 | 840 | 239 | 267 | 828 |
| • | | EB 2 | WD 1 | WB 2 | ND 1 | ND 2 | | SB 2 | 0.10 | 207 | 207 | 020 |
| Direction, Lane # | EB 1 | | WB 1 | | NB 1 | NB 2 | SB 1 | | | | | |
| Volume Total | 141 | 293 | 22 | 283 | 120 | 98 | 109 | 293 | | | | |
| Volume Left | 141 | 105 | 22 | 0 | 120 | 0 | 109 | 0 | | | | |
| Volume Right | 1200 | 185 | 0 | 141 | 0 | 11 | 0 | 152 | | | | |
| cSH | 1280 | 1700 | 1268 | 1700 | 114 | 297 | 239 | 411 | | | | |
| Volume to Capacity | 0.11 | 0.17 | 0.02 | 0.17 | 1.05 | 0.33 | 0.45 | 0.71 | | | | |
| Queue Length 95th (ft) | 9 | 0 | 1 | 0 | 176 | 35 | 55 | 136 | | | | |
| Control Delay (s) | 8.2 | 0.0 | 7.9 | 0.0 | 169.9 | 23.0 | 32.0 | 32.8 | | | | |
| Lane LOS | A | | A | | F | С | D | D | | | | |
| Approach Delay (s) | 2.7 | | 0.6 | | 103.8 | | 32.6 | | | | | |
| Approach LOS | | | | | F | | D | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Average Delay | | | 27.2 | | | | | | | | | |
| Intersection Capacity Utilizat | ion | | 56.8% | IC | CU Level of | of Service | | | В | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| | | | | | | | | | | | | |

| | • | • | • | † | ↓ | 1 |
|-------------------------------|-------------|------|-------|----------|-----------|-------------|
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | ¥ | | ሻ | ^ | ^ | 7 |
| Volume (vph) | 190 | 90 | 130 | 610 | 650 | 340 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 6.8 | | 5.0 | 6.3 | 6.3 | 6.3 |
| Lane Util. Factor | 1.00 | | 1.00 | 0.95 | 0.95 | 1.00 |
| Frt | 0.96 | | 1.00 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.97 | | 0.95 | 1.00 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1723 | | 1770 | 3539 | 3539 | 1583 |
| Flt Permitted | 0.97 | | 0.95 | 1.00 | 1.00 | 1.00 |
| Satd. Flow (perm) | 1723 | | 1770 | 3539 | 3539 | 1583 |
| Peak-hour factor, PHF | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Adj. Flow (vph) | 209 | 99 | 143 | 670 | 714 | 374 |
| RTOR Reduction (vph) | 13 | 0 | 0 | 0 | 0 | 242 |
| Lane Group Flow (vph) | 295 | 0 | 143 | 670 | 714 | 132 |
| Turn Type | NA | | Prot | NA | NA | Perm |
| Protected Phases | 4 | | 5 | 2 | 6 | |
| Permitted Phases | | | | | | 6 |
| Actuated Green, G (s) | 18.5 | | 11.4 | 42.7 | 26.3 | 26.3 |
| Effective Green, g (s) | 18.5 | | 11.4 | 42.7 | 26.3 | 26.3 |
| Actuated g/C Ratio | 0.25 | | 0.15 | 0.57 | 0.35 | 0.35 |
| Clearance Time (s) | 6.8 | | 5.0 | 6.3 | 6.3 | 6.3 |
| Vehicle Extension (s) | 2.0 | | 2.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 429 | | 271 | 2033 | 1252 | 560 |
| v/s Ratio Prot | c0.17 | | c0.08 | 0.19 | c0.20 | |
| v/s Ratio Perm | | | | | | 0.08 |
| v/c Ratio | 0.69 | | 0.53 | 0.33 | 0.57 | 0.24 |
| Uniform Delay, d1 | 25.3 | | 29.0 | 8.3 | 19.4 | 16.9 |
| Progression Factor | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 3.6 | | 0.9 | 0.1 | 0.6 | 0.2 |
| Delay (s) | 28.9 | | 29.8 | 8.4 | 20.1 | 17.1 |
| Level of Service | С | | С | Α | С | В |
| Approach Delay (s) | 28.9 | | | 12.2 | 19.1 | |
| Approach LOS | С | | | В | В | |
| Intersection Summary | | | | | | |
| HCM 2000 Control Delay | | | 17.9 | Н | CM 2000 | Level of Se |
| HCM 2000 Volume to Capa | acity ratio | | 0.60 | | | |
| Actuated Cycle Length (s) | | | 74.3 | S | um of los | t time (s) |
| Intersection Capacity Utiliza | ation | | 56.3% | | | of Service |
| Analysis Period (min) | | | 15 | | | |
| c Critical Lane Group | | | | | | |

| | • | • | † | / | \ | ↓ | |
|--------------------------------|------------|--------|----------|------|------------|------------------|---|
| Movement | WBL | WBR | NBT | NBR | SBL | SBT | |
| Lane Configurations | ሻ | 7 | ^ | 7 | ሻ | † | |
| Volume (vph) | 270 | 0 | 900 | 100 | 0 | 680 | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | |
| Total Lost time (s) | 4.0 | | 4.0 | 4.0 | | 4.0 | |
| Lane Util. Factor | 1.00 | | 1.00 | 1.00 | | 1.00 | |
| Frt | 1.00 | | 1.00 | 0.85 | | 1.00 | |
| Flt Protected | 0.95 | | 1.00 | 1.00 | | 1.00 | |
| Satd. Flow (prot) | 1770 | | 1863 | 1583 | | 1863 | |
| Flt Permitted | 0.95 | | 1.00 | 1.00 | | 1.00 | |
| Satd. Flow (perm) | 1770 | | 1863 | 1583 | | 1863 | |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | |
| Adj. Flow (vph) | 293 | 0 | 978 | 109 | 0 | 739 | |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 0 | 0 | |
| Lane Group Flow (vph) | 293 | 0 | 978 | 109 | 0 | 739 | |
| Turn Type | NA | custom | NA | Free | Perm | NA | |
| Protected Phases | | | 2 | | | 6 | |
| Permitted Phases | 8 | 8 | | Free | 6 | | |
| Actuated Green, G (s) | 13.4 | | 34.8 | 56.2 | | 34.8 | |
| Effective Green, g (s) | 13.4 | | 34.8 | 56.2 | | 34.8 | |
| Actuated g/C Ratio | 0.24 | | 0.62 | 1.00 | | 0.62 | |
| Clearance Time (s) | 4.0 | | 4.0 | | | 4.0 | |
| Vehicle Extension (s) | 3.0 | | 3.0 | | | 3.0 | |
| Lane Grp Cap (vph) | 422 | | 1153 | 1583 | | 1153 | |
| v/s Ratio Prot | | | c0.53 | | | 0.40 | |
| v/s Ratio Perm | c0.17 | | | 0.07 | | | |
| v/c Ratio | 0.69 | | 0.85 | 0.07 | | 0.64 | |
| Uniform Delay, d1 | 19.5 | | 8.6 | 0.0 | | 6.8 | |
| Progression Factor | 1.00 | | 1.00 | 1.00 | | 1.00 | |
| Incremental Delay, d2 | 4.9 | | 6.0 | 0.1 | | 1.2 | |
| Delay (s) | 24.4 | | 14.6 | 0.1 | | 8.0 | |
| Level of Service | С | | В | А | | А | |
| Approach Delay (s) | 24.4 | | 13.1 | | | 8.0 | |
| Approach LOS | С | | В | | | А | |
| Intersection Summary | | | | | | | |
| HCM 2000 Control Delay | | | 12.9 | Н | CM 2000 | Level of Service | ; |
| HCM 2000 Volume to Capac | city ratio | | 0.81 | | | | |
| Actuated Cycle Length (s) | | | 56.2 | | um of lost | | |
| Intersection Capacity Utilizat | tion | | 69.0% | IC | CU Level c | of Service | |
| Analysis Period (min) | | | 15 | | | | |
| c Critical Lane Group | | | | | | | |

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|-----------------------------------|----------|-----------|-----------|-------------|------------|------------|-----------|-----------|----------|-----------|-------------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | ર્ન | 7 | ¥ | 4 | 7 | J. | ^ | 7 | ¥ | ^ | 7 |
| Volume (vph) | 10 | 10 | 10 | 720 | 10 | 10 | 10 | 740 | 730 | 10 | 860 | 10 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 5.0 | 5.0 | 5.0 | 5.0 | 4.0 | 4.0 | 5.0 | 4.0 | 4.0 | 5.0 | 5.0 |
| Lane Util. Factor | | 1.00 | 1.00 | 0.95 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frt | | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | | 0.98 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | | 1817 | 1583 | 1681 | 1688 | 1583 | 1770 | 3539 | 1583 | 1770 | 3539 | 1583 |
| Flt Permitted | | 0.98 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (perm) | | 1817 | 1583 | 1681 | 1688 | 1583 | 1770 | 3539 | 1583 | 1770 | 3539 | 1583 |
| Peak-hour factor, PHF | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Adj. Flow (vph) | 11 | 11 | 11 | 766 | 11 | 11 | 11 | 787 | 777 | 11 | 915 | 11 |
| RTOR Reduction (vph) | 0 | 0 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 |
| Lane Group Flow (vph) | 0 | 22 | 0 | 391 | 386 | 11 | 11 | 787 | 777 | 11 | 915 | 4 |
| Turn Type | Split | NA | Perm | Split | NA | Free | Prot | NA | Free | Prot | NA | Perm |
| Protected Phases | 4 | 4 | _ | 3 | 3 | _ | 5 | 2 | _ | 1 | 6 | |
| Permitted Phases | | | 4 | | | Free | | | Free | | | 6 |
| Actuated Green, G (s) | | 3.9 | 3.9 | 33.7 | 33.7 | 96.6 | 1.8 | 38.2 | 96.6 | 1.8 | 38.2 | 38.2 |
| Effective Green, g (s) | | 3.9 | 3.9 | 33.7 | 33.7 | 96.6 | 1.8 | 38.2 | 96.6 | 1.8 | 38.2 | 38.2 |
| Actuated g/C Ratio | | 0.04 | 0.04 | 0.35 | 0.35 | 1.00 | 0.02 | 0.40 | 1.00 | 0.02 | 0.40 | 0.40 |
| Clearance Time (s) | | 5.0 | 5.0 | 5.0 | 5.0 | | 4.0 | 5.0 | | 4.0 | 5.0 | 5.0 |
| Vehicle Extension (s) | | 3.0 | 3.0 | 3.0 | 3.0 | 1500 | 2.0 | 4.0 | 4500 | 2.0 | 4.0 | 4.0 |
| Lane Grp Cap (vph) | | 73 | 63 | 586 | 588 | 1583 | 32 | 1399 | 1583 | 32 | 1399 | 625 |
| v/s Ratio Prot | | 0.01 | 0.00 | c0.23 | 0.23 | 0.04 | 0.01 | 0.22 | 0.40 | 0.01 | c0.26 | 0.00 |
| v/s Ratio Perm | | 0.00 | 0.00 | 0 / 7 | 0.77 | 0.01 | 0.04 | 0.57 | c0.49 | 0.24 | 0.75 | 0.00 |
| v/c Ratio | | 0.30 | 0.01 | 0.67 | 0.66 | 0.01 | 0.34 | 0.56 | 0.49 | 0.34 | 0.65 | 0.01 |
| Uniform Delay, d1 | | 45.0 | 44.5 | 26.7 | 26.6 | 0.0 | 46.8 | 22.7 | 0.0 | 46.8 | 23.8 | 17.7 |
| Progression Factor | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | | 2.3 | 0.0 | 2.9 29.6 | 2.6 | 0.0 | 2.3 | 0.6 | 1.1 | 2.3 | 1.2 25.0 | 0.0 |
| Delay (s) Level of Service | | 47.3 D | 44.5 D | 29.0 C | 29.2 C | 0.0 A | 49.2 D | 23.3 C | 1.1 A | 49.2 D | 25.0 C | 17.7 |
| Approach Delay (s) | | 46.4 | U | C | 29.0 | А | U | 12.5 | А | U | 25.2 | В |
| Approach LOS | | 40.4 D | | | 29.0 C | | | 12.5 B | | | 23.2 C | |
| | | U | | | C | | | ь | | | C | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 20.3 | H | CM 2000 | Level of S | service | | С | | | |
| HCM 2000 Volume to Capaci | ty ratio | | 0.70 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 96.6 | | um of lost | | | | 19.0 | | | |
| Intersection Capacity Utilization | on | | 60.6% | IC | U Level (| of Service | | | В | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

LOS Worksheets – Year 2022 with Partial Development Conditions

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|-------------------------------|------------|----------|--------|------|------------|------------|---------|----------|-------------|----------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | र्स | 7 | | र्स | 7 | ¥ | † | 7 | J. | † | 7 |
| Volume (vph) | 30 | 170 | 71 | 330 | 80 | 280 | 31 | 561 | 454 | 440 | 556 | 10 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | | 5.0 | 5.0 | | 5.0 | 5.0 | 4.0 | 5.0 | 5.0 | 4.0 | 5.0 | 5.0 |
| Lane Util. Factor | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frpb, ped/bikes | | 1.00 | 0.98 | | 1.00 | 1.00 | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 1.00 |
| Flpb, ped/bikes | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | | 1.00 | 0.85 | | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | | 0.99 | 1.00 | | 0.96 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | | 1849 | 1550 | | 1788 | 1583 | 1770 | 1863 | 1547 | 1770 | 1863 | 1583 |
| Flt Permitted | | 0.73 | 1.00 | | 0.55 | 1.00 | 0.28 | 1.00 | 1.00 | 0.09 | 1.00 | 1.00 |
| Satd. Flow (perm) | | 1358 | 1550 | | 1018 | 1583 | 521 | 1863 | 1547 | 165 | 1863 | 1583 |
| Peak-hour factor, PHF | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Adj. Flow (vph) | 34 | 191 | 80 | 371 | 90 | 315 | 35 | 630 | 510 | 494 | 625 | 11 |
| RTOR Reduction (vph) | 0 | 0 | 51 | 0 | 0 | 159 | 0 | 0 | 257 | 0 | 0 | 6 |
| Lane Group Flow (vph) | 0 | 225 | 29 | 0 | 461 | 156 | 35 | 630 | 253 | 494 | 625 | 5 |
| Confl. Peds. (#/hr) | | | 1 | 1 | | | | | 1 | | | |
| Turn Type | Perm | NA | Perm | Perm | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases | | 4 | | | 8 | | 5 | 2 | | 1 | 6 | |
| Permitted Phases | 4 | | 4 | 8 | | 8 | 2 | | 2 | 6 | | 6 |
| Actuated Green, G (s) | | 40.0 | 40.0 | | 40.0 | 40.0 | 44.8 | 41.2 | 41.2 | 60.2 | 52.6 | 52.6 |
| Effective Green, g (s) | | 40.0 | 40.0 | | 40.0 | 40.0 | 44.8 | 41.2 | 41.2 | 60.2 | 52.6 | 52.6 |
| Actuated g/C Ratio | | 0.36 | 0.36 | | 0.36 | 0.36 | 0.41 | 0.37 | 0.37 | 0.55 | 0.48 | 0.48 |
| Clearance Time (s) | | 5.0 | 5.0 | | 5.0 | 5.0 | 4.0 | 5.0 | 5.0 | 4.0 | 5.0 | 5.0 |
| Vehicle Extension (s) | | 2.5 | 2.5 | | 2.5 | 2.5 | 2.0 | 5.0 | 5.0 | 2.0 | 5.0 | 5.0 |
| Lane Grp Cap (vph) | | 492 | 562 | | 369 | 574 | 252 | 696 | 578 | 308 | 889 | 755 |
| v/s Ratio Prot | | | | | | | 0.00 | 0.34 | | c0.22 | 0.34 | |
| v/s Ratio Perm | | 0.17 | 0.02 | | c0.45 | 0.10 | 0.05 | | 0.16 | c0.66 | | 0.00 |
| v/c Ratio | | 0.46 | 0.05 | | 1.25 | 0.27 | 0.14 | 0.91 | 0.44 | 1.60 | 0.70 | 0.01 |
| Uniform Delay, d1 | | 26.8 | 22.8 | | 35.1 | 24.8 | 20.8 | 32.7 | 25.8 | 34.0 | 22.7 | 15.1 |
| Progression Factor | | 1.00 | 1.00 | | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | | 0.5 | 0.0 | | 132.8 | 0.2 | 0.1 | 16.1 | 1.1 | 286.5 | 3.2 | 0.0 |
| Delay (s) | | 27.3 | 22.8 | | 167.9 | 25.0 | 20.9 | 48.8 | 26.9 | 320.4 | 25.8 | 15.1 |
| Level of Service | | С | С | | F | С | С | D | С | F | С | В |
| Approach Delay (s) | | 26.1 | | | 109.9 | | | 38.5 | | | 154.5 | |
| Approach LOS | | С | | | F | | | D | | | F | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 92.5 | H | CM 2000 | Level of | Service | | F | | | |
| HCM 2000 Volume to Capac | city ratio | | 1.50 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 110.2 | | um of lost | | | | 14.0 | | | |
| Intersection Capacity Utiliza | tion | | 102.8% | IC | U Level | of Service | е | | G | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lang Group | | | | | | | | | | | | |